## A RAY TRACING

# DIGITAL COMPUTER PROGRAM

# OR THE STUDY OF MAGNETOSPHERIC

# DUCT PROPAGATION

RAMASASTRY and WALSH

CASE FILE COPY



NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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JAYARAM RAMASASTRY and EDWARD J. WALSH

Prepared by
NASA Electronics Research Center



### **FOREWORD**

This NASA Special Publication is a documentation and discussion of a digital computer program used to conduct ray-tracing of electromagnetic waves in the magnetosphere. The publication consists of three sections. Section I contains a general description of the program and its capabilities. Section II assumes that the reader is aware of the scope of the program and provides all the information necessary for a non-programmer to run the program. Section III is a programming manual containing extensive information on the program structure. The program is designed to operate in the IBM 7094 IBSYS environment. It is written in Fortran IV but utilizes a MAP assembler subroutine to integrate the differential equations.

Ray-Tracing techniques are used extensively in the study and understanding of propagation of electromagnetic waves in any media (neutral, magneto-ionic, etc.). Combined with experimental data, the ray-tracing technique has served as a powerful tool in communications research. Data from NASA satellites (ISIS, Explorer, RAE, and the like) are better evaluated with the help of digital ray-tracing techniques. The present documented program has been used by the authors in studying the data from the ISIS topside sounder experiments. However, the program is applicable to any medium with suitable choice of models.

Jayaram Ramasastry Edward J. Walsh April 1969

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### INTRODUCTION

This report consists of three sections. Each section is intended to be an independent treatment of a specified aspect of reader interest.

Section I contains a general description of the program so that the reader can gain a general idea of the program's capability.

Section II assumes that the reader is aware of the scope of the program and that he intends to use this program in ray tracing analyses. Section II contains all the detailed information necessary for a non-programmer to run the program.

Section III is a programming manual containing detailed information on the program structure.

This program is designed to operate in the IBM 7094 IBSYS environment. The basic program is written in FORTRAN IV but utilizes a MAP assembler subroutine to integrate the differential equations.

The program can be considered to consist of five major parts:

- (1) An executive routine which governs program flow
- (2) An input section to assess the initial data necessary to operate the program.
- (3) An output which prints a history of the path of the ray and under option governs the generation of a plotting tape
- (4) Three mathematical models which characterize the electromagnetic properties of the magnetosphere
- (5) An integration routine which evaluates the differential equations

The ray-tracing technique has been used by many people in ionospheric and magnetospheric propagation research. Actual ray-paths and signal characteristics (like attenuation, path-loss, doppler shift, and refraction) in model atmospheres and ionospheres are computed using the ray-tracing program. Because of the high accuracy obtainable, the use of a high-speed digital computer is preferred to an analog machine for the integration of the ray equations.

The ray-tracing program used in our study is based on the Hamilton system of equations as derived in spherical polar coordinates by Haselgrove and extended by Grossi and Langworthy for the investigation of HF and VHF ionospheric propagation. The particular problem concerning our study is the guided propagation of high frequency radiowaves along the magnetic field lines of the Earth. Some of the echo traces appearing at virtual ranges greater than those of the normal vertical incidence echo traces on the topside-sounder ionograms have been explained in terms of guided propagation of radiowaves along the field-lines. The guided propagation along the field-line is made possible by field-aligned ionization irregularities (e.g., ducts and shells) of suitable scale sizes and enhancements or depletions. The irregularities are assumed to have thickness greater than the radio wavelength and hence act as waveguides or "ducts" to trap HF energy and produce the long-range echo traces. The guiding of rays along field-lines requires irregularities with a certain minimum transverse ionization gradient. Propagation between magnetic conjugate points or "conjugate ducting" occurs when the transverse ionization gradient exceeds the minimum required for quidance at the apex of the magnetic line of force. Conjugate echoes are recorded by the topside sounder receivers when the signal traverses to and from the conjugate reflection points along the magnetic field-line passing through the satellite. Knowing the satellite orbital parameters and the transmitted signal parameters, one could conduct ray-tracing utilizing realistic models for the magnetosphere. The ray-tracing program yields such useful information as the criteria for guidance, the groupdelays of the trapped signals of various frequencies, and total path length traversed. Ray-tracing method is a powerful tool when used alongside experimental observations since it gives a better insight into the observed results.

### I. GENERAL PROGRAM DESCRIPTION

### Introduction

This section provides a general description of the capabilities of the program. Major emphasis is placed on the program input and output and the basic formulation of the differential equations.

The integration technique is discussed only briefly but reference is made to Appendix A where the integration package is described in detail.

The three models characterizing the electromagnetic properties of the magnetosphere (electron density, collision frequency and magnetic field) are discussed briefly in this section and their detailed descriptions are presented in Section III.

### Main Program

The following equations form the basis of the ray tracing program. The first six equations are the Hamilton electromagnetic wave equations in spherical coordinates. The remaining five equations are additional functions of phase path length. All derivatives indicated with a dot are with respect to phase path length in km.

The ray is described in terms of position in spherical polar coordinates with origin at the center of the Earth and in terms of the components of the wave normal  $y_1$ ,  $y_2$ ,  $y_3$  in the r,  $\theta$ ,  $\phi$  directions, respectively. Figure 1 describes the ray position geometry in spherical coordinates.

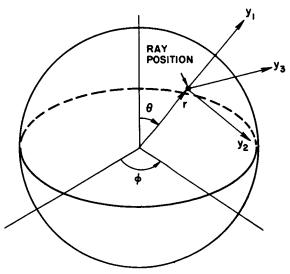


Figure 1. Ray Position in Spherical Coordinates.

Equation #

Initial Condition

1 
$$\dot{\mathbf{r}} = \frac{1}{\mu^2} \left( \mathbf{y}_1 - \mu \frac{\partial \mu}{\partial \mathbf{y}_1} \right)$$

$$r(o) = r_{o}$$

$$2 \qquad \dot{\theta} = \frac{1}{\mu^2 \mathbf{r}} \left( \mathbf{y}_2 - \mu \frac{\partial \mu}{\partial \mathbf{y}_2} \right)$$

$$\theta(0) = \theta_0$$

3 
$$\dot{\phi} = \frac{1}{\mu^2 r \sin \theta} \left( y_3 - \mu \frac{\partial \mu}{\partial y_3} \right)$$

$$\phi$$
(o) =  $\phi$ <sub>o</sub>

4 
$$\dot{y}_1 = \frac{1}{\mu} \frac{\partial \mu}{\partial r} + \dot{\theta} y_2 + \dot{\phi} y_3 \sin \theta$$

$$y_1(0) = y_1$$

5 
$$\dot{y}_2 = \frac{1}{r} \left( \frac{1}{\mu} \frac{\partial \mu}{\partial \theta} - \dot{r}y_2 + \phi y_3 r \cos \theta \right)$$

$$y_2(0) = y_2$$

$$6 \qquad \dot{y}_3 = \frac{1}{r\sin\theta} \left( \frac{1}{\mu} \frac{\partial \mu}{\partial \phi} - \dot{r} y_3 \sin\theta - \dot{\phi} y_3 r \cos\theta \right)$$

$$y_3(0) = y_3$$

$$\dot{\mathbf{G}} = \mathbf{1} + \frac{\mathbf{f}}{\mu} \quad \frac{\partial \mu}{\partial \mathbf{f}}$$

$$G(o) = 0.0$$

8 
$$\dot{S} = \frac{1}{\mu c \phi s \alpha}$$

$$S(0) = 0.0$$

9 
$$\dot{D} = -\frac{2K}{\mu} D$$

$$D(o) = 1.0$$

10 
$$\dot{\mathbf{E}} = \frac{1}{\mu} \frac{\partial \mu}{\partial \phi}$$
 and  $\dot{\Delta} \mathbf{f} = -\frac{\mathbf{f}}{\mathbf{c}} \dot{\mathbf{E}}$ 

$$E(o) = 0.0$$
  
 $\Delta f(o) = 0.0$ 

11 
$$\dot{P}_{F} = \frac{\nabla^{2} \tau}{\frac{2}{\mu} c \phi s \alpha}$$

$$P_{\mathbf{F}}(0) = 0.0$$

### where:

- $\mu$   $\Xi$  phase refractive index
- r = geocentric radius of the wave front
- $\theta \equiv colatitude$  of the wave front
- $\phi \equiv$  longitude of the wave front
- $(y_1, y_2, y_3) =$ components of the wave normal in the  $\theta$ ,  $\theta$ , and  $\phi$  directions
  - G ≡ group path length
  - S = ray path length
  - D = powerloss due to absorption
  - E = coefficient used to compute the doppler shift, see Section III
  - P<sub>F</sub> = coefficient used to compute the doppler shift, see Section III
    - $\tau$  = eikonal function that has the property that the surface  $\tau$  = constant, is the geometrical wave front
    - $\alpha$  = angle between the wave normal and the wave front

The powerloss calculation, Eq. (11), is optional and may be suppressed if this data is of no interest to the user.

A complete description of all calculations can be found in section III.

### Input Section

The input routine is written with the aim of providing maximum control over the operation of the program and at the same time minimize the size of the input deck. The NAMELIST feature of FORTRAN IV is used because it gives the user maximum flexibility and also tends to minimize the careless errors usually associated with fixed format input statements.

The input data is divided into three major parts:

(1) The data required to describe the initial position, direction and characteristics of the ray

- (2) Optional integration parameters
- (3) Optional limits for the axes of the calcomp plots

The required program inputs are:

- (1) Starting position and direction of the electromagnetic wave, which is referred to as a "ray"
- (2) Integration stops or triggers which either temporarily or permanently halt the integration procedure
- (3) Propagation frequency, and ray mode (ordinary or extraordinary)
- (4) Output controls, print and plotting intervals
- (5) Option indicators
- (6) Optional input indicators

All optional parameters are preset in the program. If, however, any or all of these parameters must be changed, the program allows for easy modification of these nominal values.

For a complete description of all required and optional inputs, see section II.

### Output Section

All output, with the exception of a list of the case inputs, is performed by subroutine OUTPUT. This subroutine not only prints a history of the path of the ray, but under option control governs the plotting of the data.

<u>Printed output.</u> - Results are printed whenever one of the following situations occur:

- (1) A print time is reached. Print time is a function of phase path length. A print time occurs at  $n \cdot \Delta hp$  where n = 0, 1, 2, 3... and  $\Delta hp$  is some increment in phase path length, measured in kilometers.
- (2) The rate of change of the geocentric radius, r, is approximately equal to zero.

- (3) A stopping condition has been reached.
- (4) A reflection has occurred.

The printed output consists of a sequence of 3 x 7 matrices grouped thirteen per page. The first matrix in the sequence, printed at the top of the page, is a heading matrix which identifies each data element of the data arrays. The heading definitions are listed below according to row and column.

Row	Column	<u>Title</u>	Description
1	1	PHASE PATH	Phase path length, hp, from $(r_0, \theta_0, \phi_0)$ in kilometers.
1	2	RADIUS	Geocentric radius, r, of the ray position in kilometers.
1	3	COLATITUDE	Colatitude, $\theta$ , of the ray position, in degrees.
1	4	LONGITUDE	Longitude, $\phi$ , of the ray position, in degrees.
1	5	ABSORPTION	Absorption loss, D.
1	6	DOPPLER, SP	Doppler shift
1	7	POWER LOSS	Power loss, $\frac{P_{RO}}{P_{T}}$ , exclusive of absorption
2	1	GROUP PATH	Group path length, G, in kilometers
2	2	Y <sub>1</sub>	Vertical component, Y <sub>1</sub> , of the wave normal
2	3	Y <sub>2</sub>	Southerly component, Y <sub>2</sub> , of the wave normal
2	4	Y <sub>3</sub>	Easterly component, Y <sub>3</sub> , of the wave normal
2	5	MU**2	Square of the Index of refraction $(\mu^2)$
2	6	Y**2	$Y_1^2 + Y_2^2 + Y_3^2$
2	7	EPSTEIN CD	Epstein condition

Row	Column	Title	Description
3	1	RAY PATH	Ray path length, s, in kilometers
3	2	POLARIZATION -MOD AND ARG	Modulus and argument of the wave polarization term, R.
3	4	DEL MU	Validity criterion
3	5	N	Electron density, N, in electrons/cc
3	6	NU	Collision frequency, $\nu$ , in collisions/sec.
3	7	GROUP DELAY (Gd)	Group delay in milliseconds. (Group path length divided by the velocity of light in free space.)

An example of the printed output can be found in Table I. Whenever results are printed because of any one of the stopping conditions, an appropriate message is printed below the data to which the message refers.

Plotted output. - Each output plot consists of two plots. The rectangular plot shows the distance of the ray normal to the field line from the near end. The polar plot shows the actual ray path with reference to the surface of the Earth. The polar plot gives a clear indication of the positions of the conjugate reflection points as well as the L value of the field line guiding the rays. A complete description of the plotting routine can be found in section III.

Some examples of the plotted output are described in the following paragraphs.

### Examples

Figures 2 through 4 show a few results of the ray tracing. They are chosen so as to demonstrate the capabilities of the program. Figure 2 is a single plot which simulates a conjugate echo path observed in an Alouette 2 ionogram. Figure 3 is an overlayed plot of two rays launched from the same point but with different launch angles, DELAO. Figure 4 is an overlayed plot of four rays launched from the same point with identical launch angles but at different frequencies.

Parameters shown in the figures are defined as follows:

# EXAMPLE OF PRINTED OUTPUT

DOCUMENTATION  LONGITUDE ARSORPTION DOPPLFR SP POWER LOSS  YA MU**2 Y**2 EPSTEIN CD  YA MU**2 NU GROUP DELAY	01 8,9999947E 01 9,9999999E=01 0.000000E=39 0.000000E=39 01 -0.0000000E=39 8.589997E=01 8.5899995E=01 3.2884926E=13 01 2.1791243E=05 1.2074153E 03 8.6929314E=06 8.0105249E=02	01 8.9999987E 01 9.999999E-01 _0.000000E-39	01 8,999987E 01 9,999999E-01 -0.000000E-39 0.00000E-39 01 0.000000E-39 8,6975418E-01 8,6975416E-01 1.0242290E-13 01 7,7818205E-06 1.148685E 01 3,0565067E-06 1.5872814E 00	01 8.9999987E 01 9.999999E-01 -0.0000000E-39 0.000000E-39 01 0.000000E-39 8.7415765E-01 8.7415764E-01 6.0527487E-14 01 1.612134E-05 1.1217326E 01 1.9024320E-06 2.3712085E 00	01 8.9999987E 01 9.999999E-01 -0.000000E-39 0.000000E-39 01 0.000unuE-39 A.7781720E-01 A.7781718E-01 3.8245256E-14 01 2.1914030E-05 1.1025245E 01 1.2563415E-06 3.1502037E 00	01 8.9999987E 01 9.999999E-01 -0.000000E-39 0.000000E-39 01 0.000000E-39 8.8080%30E-01 8.8080%28E-01 2.8948592E-14 01 9.8592200E-06 1.0848494E 0* 8.8431544E-07 3.9251668E 00	01 8.9999947E 01 9.9999999E-01 -0.000000E-39 0.000000E-39 01 0.000000E-39 R.R324545E-01 R.R324544E-01 1.R751383E-14 01 1.n791444E-05 1.0700884E 01 A.5878622E-07 4.A968806E 00	01 8.9999987E 01 9.9999999E=01 =0.000000RE=39 0.000000E=39 01 0.0000000E=39 8.8518248E=01 8.8518245E=01 1.4453184E=14 01 2.1180092E=05 1.0580794E 01 5.2030317E=07 5.4660469E 00	U1 8.999987E 01 9.9999999E=U1 -0.000000E=39 0.000000E=39 U1 0.000000E=39 8.8660226E=01 8.8660225E=01 1.2002435E=14 U1 1.*447359E=U5 1.0490262E 01 4.3987898E=07 6.2332779E 00	U1 8.9999987E 01 9.9999999E=01 -n.NQNQNNDE=39 N.NDNDNOE=39 U1 0.NQNQNUNE=39 R.R75610NE=01 R.R756102E=01 1.N6R6431E-14 U1 9.N264119E=U6 1.N426152E 01 1.9635N41E=07 6.9991287E 00	01 8.9999987E 01 9.9999999E=01 -0.0000000E=39 0.000000E=39 01 0.0000000E=39 8.8811187E=01 8.8811182E=01 1.0141845E=14 01 1.7753554E=05 1.0385536E 01 3.7861936E=07 7.7641417E 00	
GENEPAT <sub>E</sub> N FOR DUCUM COLATTUDE 12 1 MUD AMD ARG	7.756m658E 01 8.494u216E-01 -09.000u00E 01 2	7.8563367E 01 8.8.60490.5E-01 0	7.9885571E 01 8.7869874E-01 09.000gwnE 01 7.	8.1110704E 01 8. 8.9420238E-01 0. -9.000000E 01 1.	8.234U946E 01 8. 9.0372155E-01 0. -9.000u00E 01 2.	8.3575100E 01 8.9.145786E-01 09.00000NE 01 9	8.4814052E 01 8. 9.2559346E-01 0. -9.00000NE 01 1.	œ c N	8.7296759E U1 8.9.3677850E-U1 09.000000E U1 1.	9.4092793E-01 9.4092793E-01 9.	8.979.206E 01 8.9.4235470E-01 09.000.00E 01 1.	8.9805684E 01 8.
SAMPLE CASE GENAUIUS Y1 POLAKIZATION -	0.3041084£ U3 3.7083140E-U1 1.0000023E U0 -	9.379u591E_u3 3.5227335E-01 1.0u00086E_00	0.4549106E U3 7.1247831E-U1 1.0000001E U0	0.5233201E 03 2.7305632E-01 1.000071E 00	9.5431912E U3 2.4719298E-U1 1.0000027E U0 -	0.632651E 03 2.1059714E-01 1.0000034E 00 -	0.6/63511E U3 1.6285645E-U1 1.0U0U041E U0 -	0.7104039E U3 1.2611563E-U1 1.0000010E U0	0.7346377E U3 0.5122551E-U2 1.0000070E_U0	0.7496772E U3 . u.7U7U662E-U2 1.0U0U0U1E U0 -	0.7562792E 03 6.3855051E-04 1.0000062E 00	0.7562800E U3
PHASE PATH GROUP PATH RAY PATH	2.00000000 ul 2.4u31575E ul 2.1583306E ul	2.0000000 u2 2.3919784E u2 2.1547645E u2	4.00000000 U2 4.7618443E U2 4.3024053E U2	6.0000000 u2 7.1136256 u2 6.4441360E u2	8.0000000 U2 9.4506111E U2 8.5809700E U2	1.0000000 U3 1.1775500E U3 1.0713754E U3	1.2000000	1.40000000 03 1.6398141E 03 1.4970117E 03	1.6000000 u3 1.8699834E u3 1.7094989E u3	1.80000000 03 2.0997386E 03 1.9216413E 03	2.000u0u0e u3 2.3292425E u3 2.134u939E u3	2.0026441E U3

PKFRAC = the peak fractional ionization enhancement

LAMBDA = the colatitude of the field line

AO = the initial angle the ray makes with the local vertical

BO = the initial angle the ray makes with the south vector

PHI

& THETA = the magnetic longitude and colatitude of the initial signal position

HO = the scale size of the duct at the base of the field line

FREQ = the frequency of the initial signal

The ray mode (ordinary or extraordinary) is also indicated.

Each figure consists of two plots. The rectangular plot shows the distance of the ray normal to the field line versus the distance along the field line from the near end. The polar plot shows the actual ray path with reference to the surface of the Earth. The polar plot gives a clear indication of the positions of the conjugate reflection points as well as the L value of the field line guiding the rays.

All cases are for the L=1.53 field line using a peak electron density enhancement of 5.0 percent at the point the ray is launched. The rays are all of the extraordinary mode.

In Figure 2 the ray has an initial geocentric radius of 9295.40 km. This corresponds to a distance of about 2.75 km from the field line at a colatitude of 77.445 degrees. The ray starts at about 4,500 km along the field line from its base in the northern hemisphere. It passes from north to south and is reflected in the southern hemisphere. After reflection it travels back into the northern hemisphere where it is again reflected. The program was deliberately stopped after the second reflection.

The slight bowing observed in the path of the ray near the equator is caused by the larger scale size near the equator. The larger scale size causes the enhancement structure to be wider. Thus, the ray rides further out from the field line.

S 00

= 10024.00

2

THETR = 109.050

-2.00

-55.371

8

= 1.200

FREG

00.0

90.000

Ę

LAMBOR = 48.920

	90.00
	40.00 50.00 60.00 70.00 80.00 DIS ALONG FLO LN IN KM *10
	30.00
	20.00
	10.00
18.00 -16.00 -14.00 -12.00 -9.00 -6.00 -4.00	.0 .0 .00
BG : 0.000 HPRIME : 1.839 PKFRAC : 0.070 HD : 1.000 IN KM DIS FROM FLD LN IN KM	•

Single Plot Simulating a Conjugate Echo Path Observed in Alouette 2 ı Figure 2A.

100.00 110.00

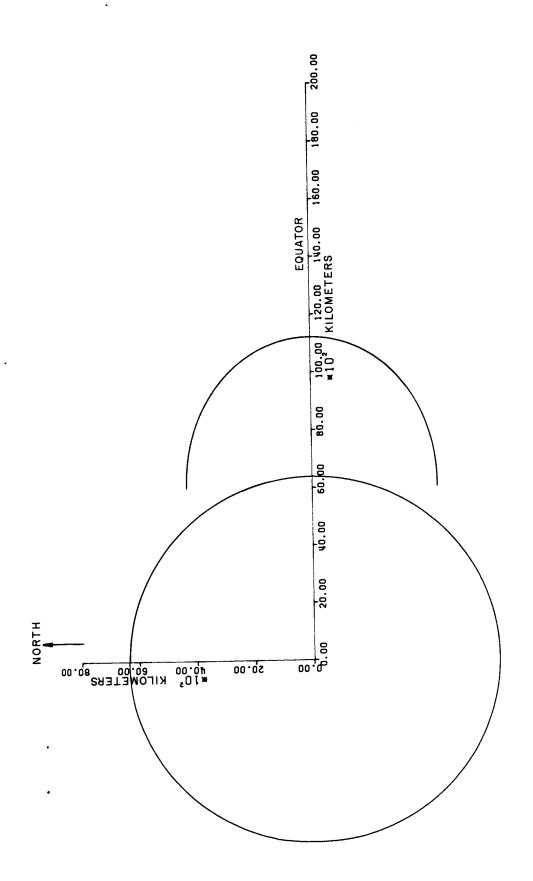


Figure 2B. - Single Plot Simulating a Conjugate Echo Path Observed in Alouette 2.

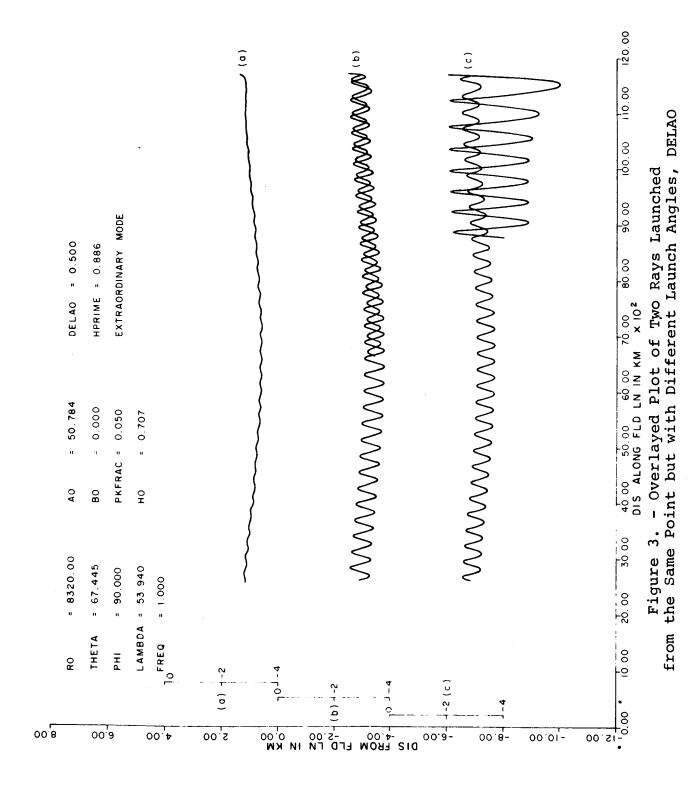
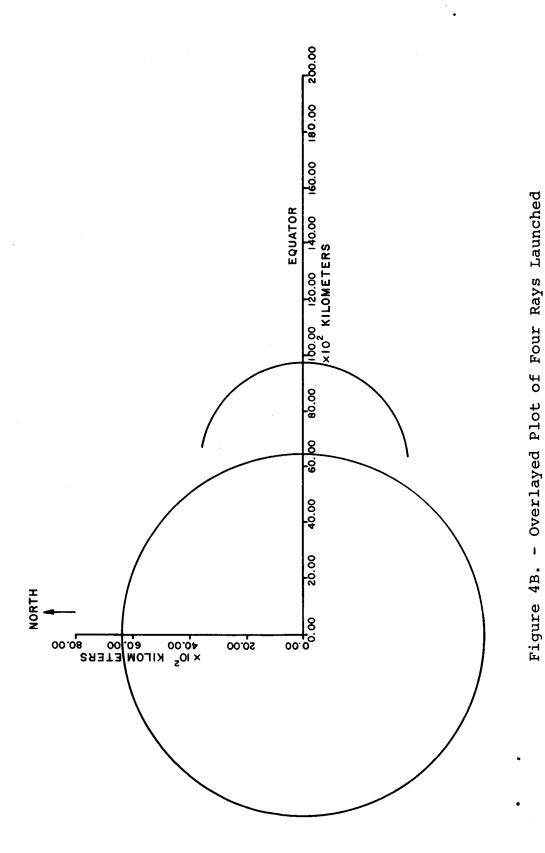


Figure 4A. - Overlayed Plot of Four Rays Launched



The oscillatory nature of the ray path seen in the rectangular plot is caused by the ray being launched at a point where the electron density gradient is greater than necessary for guidance. The ray tends to oscillate about a point where the electron density gradient is just sufficient to guide the ray parallel to the field line. A careful launching of the signal can minimize these initial oscillations. In this figure the oscillations were somewhat damped upon reflection. However, this is not always the case. For example, in Figure 4 the amplitude of the oscillations after reflection was actually increased.

Figure 3 shows three rays launched from the same point but with different launch angles, DELAO. The launch angles corresponding to plots (a), (b) and (c) are 0 degrees, - 0.5 degrees and + 0.5 degrees, respectively. The oscillatory nature of the ray paths in plots (b) and (c) once again demonstrates that the rays were launched off the equilibrium position. The rays started in the northern hemisphere about 2500 km along the field line and propagated along the field line to the southern hemisphere down to the reflection level. After reflection, they retraced their path and returned to the reflection level in the northern hemisphere and were again reflected. The program was stopped at this point because two reflections were counted.

In Figure 4, one can observe the behavior of waves at different frequencies. Three rays are launched from the same point with identical launch angles. The enhancement model is the same but the three rays differed in their frequencies. The three frequencies are 0.95, 1.15, and 1.25 MHz. The ray with a frequency of 0.95 MHz has the greatest amplitude of oscillation and the ray with the frequency of 1.25 MHz has the minimum initial oscillations. The rays were launched in the southern hemisphere at a colatitude of 77.445 degrees. The rays passed from south to north. Only one ray was reflected back into the duct at the conjugate reflection point. The other two escaped upon reflection. The inverse proportionality of the oscillation amplitude to frequency indicates that higher electron density gradients are required to guide the rays of higher frequencies.

Figures 5A, B; 5C, D, and 5E, F correspond to cases where a frequency of 1.2 MHz is trapped in enhancement ducts of different peak fractional enhancements. The ray launching position and the launch angle is the same for all the three cases. However, the peak fractional enhancements are 5, 6 and 7 percent for Figures 5A, 5C, and 5E, respectively. It may be noticed that in Figure 5A, the peak fractional enhancement of 5 percent is not sufficient to contain the ray on its way back from the reflection point in the northern hemisphere. Peak fractional enhancements of 6 and 7 percent as shown in Figures 5C and 5E seem sufficient to trap the rays and when the program was terminated after two reflections, the rays were still well trapped.

### Magnetospheric Models

The following characterizes properties of the magnetosphere:

- (1) The electron density distribution
- (2) The magnetic field distribution
- (3) The electron collision frequency distribution

The mathematical models for these quantities have been implemented in the form of subroutines and can be independently modified as necessary.

Magnetic field model.- A dipole model is used for the magnetic field of the Earth. The magnetic field equation which defines gyrofrequency,  $f_{\rm u}$ , is given by:

$$f_{H}(r, \theta) = C_{11} \left(\frac{a}{r}\right)^{3} \left[1 + 3\cos^{2}\theta\right]^{1/2}$$

where a = 6378.0, the radius of the earth in km, and r and  $\theta$  are the geocentric distance and colatitude of any point on the field line.

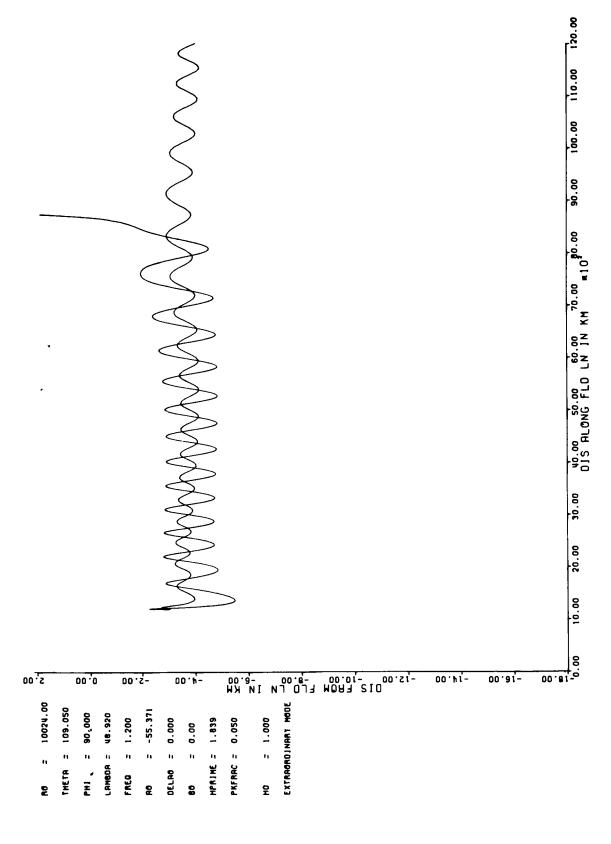
$$C_{11} = \frac{e}{2\pi m} B_0 * 1.0E-6 = 0.9$$

where  $B_O$  is the magnetic field on the surface of the Earth at the equator, and e and m are the charge and mass of an electron. A value of 0.3142 Gauss is used for  $B_O$ .

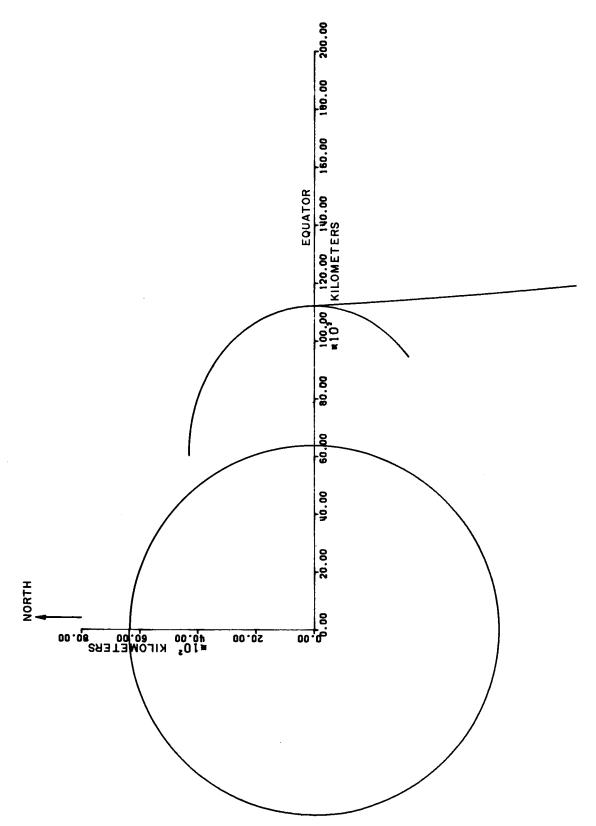
The angle between the magnetic field direction and the wave normal is given by

$$\cos \psi = \frac{2Y_1 \cos \theta + Y_2 \sin \theta}{\left[\left(\sum_{i=1}^{3} Y_i^2\right) \left(1 + 3\cos^2 \theta\right)\right]^{1/2}}$$

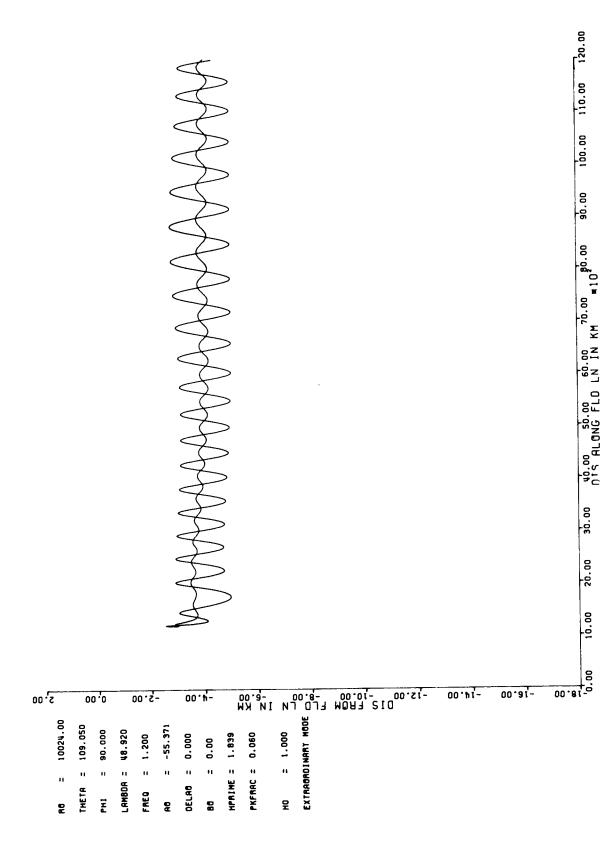
$$\sin \psi = \frac{2Y_2 \cos \theta = Y_1 \sin \theta}{\left| 2Y_2 \cos \theta - Y_1 \sin \theta \right|} \quad \left( 1 - \cos^2 \psi \right)^{\frac{1}{2}}$$



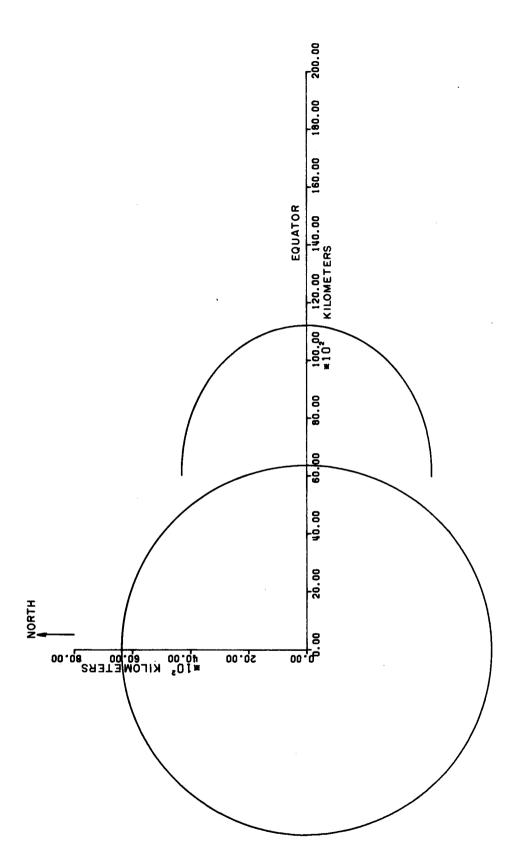
- Ray Path of 1.2 MHz Signal Trapped in an Enhancement Duct. Peak Fractional Enhancement in the Duct at the Initial Ray Position is Equal to 5 Percent Figure 5A.



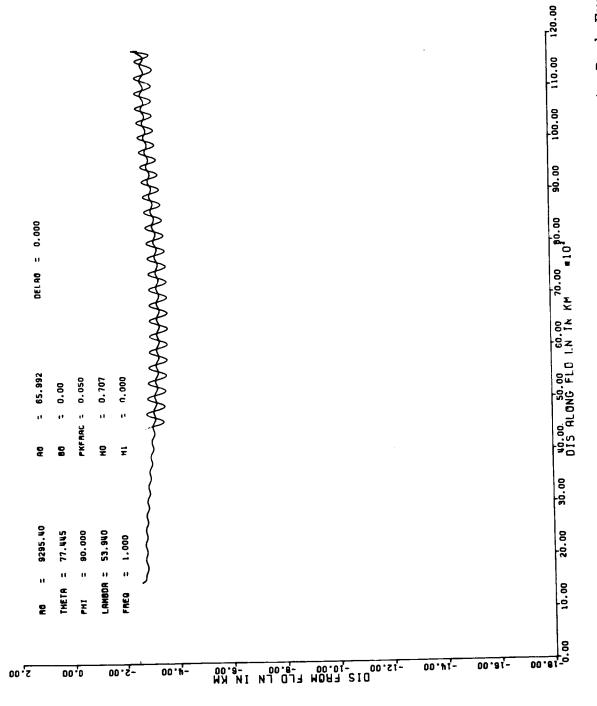
- Ray Path of 1.2 MHz Signal Trapped in an Enhancement Duct. Peak Fractional Enhancement in the Duct at the Initial Ray Position is Equal to 5 Percent Figure 5B.



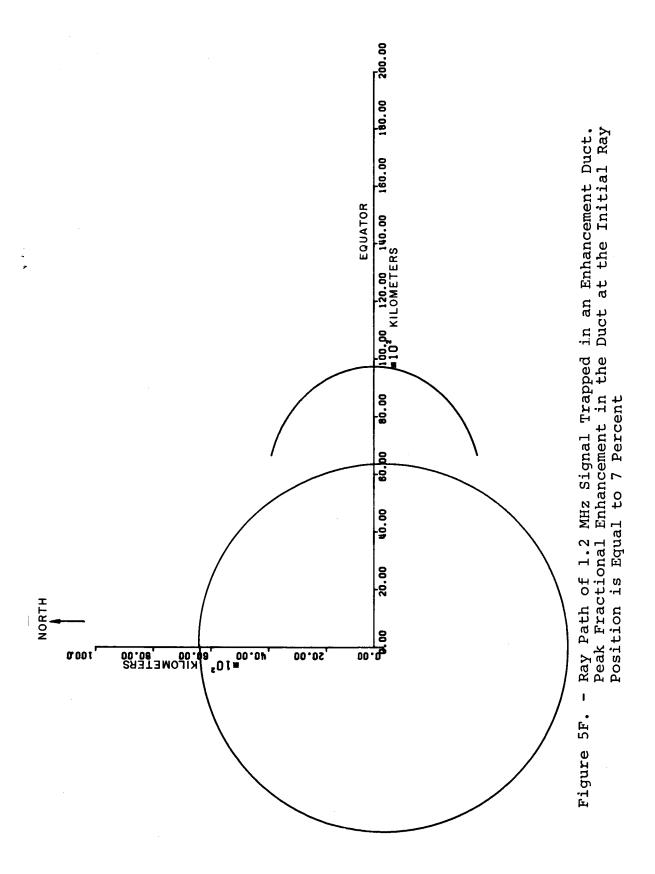
Ray Path of 1.2 MHz Signal Trapped in an Enhancement Duct. Peak Fractional Enhancement in the Duct at the Initial Ray Position is Equal to 5 Percent - Ray Path of Figure 5C.



Ray Path of 1.2 MHz Signal Trapped in an Enhancement Duct. Peak Fractional Enhancement in the Duct at the Initial Ray Position is Equal to 6 Percent ı Figure 5D.



1.2 MHz Signal Trapped in an Enhancement Duct. Peak Fractional in the Duct at the Initial Ray Position is Equal to 7 Percent Enhancement in the Duct at - Ray Path of Figure 5E.



But, the dipole model is highly idealized and lacks such features as local variations in the magnetic field strength. Its advantage lies in the fact that it saves a lot of computer time and for the ray-tracing problem under study, the microscopic features of the magnetic field are not necessary.\*

Collision frequency model. - The collision frequency model has the following functional form:

$$v = 10^{v'}$$

where  $\nu'$  is computed as shown below. The collision frequency profile as a function of altitude consists of three parts that are smoothly joined with the aid of a curve fitting program.

for  $6378 \leqslant r \leqslant 6478 \text{ km}$ :

$$\nu' = 12.03527 - 0.07392 x$$

where

$$x = (r-6378) \text{km}$$
.

for  $6478 \le r \le 6853$  km:

$$\nu' = \sum_{i=1}^{6} \left[ a_i + C(\theta, \phi) b_i \right] f_i(x)$$

where

$$f_1(x) = 1$$
 ;  $x = (r-6478)km$   
 $f_2(x) = x$   
 $f_3(x) = x^2$   
 $f_4(x) = x^3$   
 $f_5(x) = \cos(0.0157x)$ 

<sup>\*</sup>Those who are interested in using a better magnetic field model should refer to Langworthy (Smith) (1966) for a description of the Gaussian spherical harmonic magnetic field model.

$$f_{6}(x) = \sin(0.0157x)$$

$$a_{1} = 5.0562$$

$$a_{2} = -3.7482x10^{-2}$$

$$a_{3} = 1.3864x10^{-4}$$

$$a_{4} = 1.4777x10^{-7}$$

$$a_{5} = -0.48192$$

$$a_{6} = -0.27021$$

$$; b_{1} = 0.032512$$

$$; b_{2} = -0.8847x10^{-2}$$

$$; b_{3} = 0.8541x10^{-4}$$

$$; b_{4} = -1.5422x10^{-7}$$

$$; b_{5} = 0.01470$$

$$; b_{6} = 0.65037$$

 $C(\theta, \phi) = C_1 \theta^2 + C_2 \theta + C_3 + (d_1 \theta^2 + d_2 \theta + d_3) \cos \phi$ 

where

$$C_1 = -0.35818$$
 ;  $d_1 = -0.17828$ 

$$C_2 = 1.1250$$
 ;  $d_2 = 0.55997$ 

$$C_3 = -0.88344$$
 ;  $d_3 = 0.56028$ 

 $\theta$  is the colatitude and  $\varphi$  is the longitude in degrees. Symbol  $\varphi$  = 0 corresponds to local noon.

For 
$$r \ge 6853$$
 km,  
 $\nu' = 2.3653-0.0030266x + (0.3195-0.0000536x) C(\theta, \phi)$ 

where

$$x = (r-6853)$$

Electron density model.— The model for the electron density distribution incorporates those features that have a bearing on the high-frequency ducting problem. Thus, an ionization irregularity (duct) model is superimposed on the normal radial distribution of electron density. The duct structure is aligned along the magnetic field.

A complete description of the electron density model can be found in section III.

### Integration Package

Because of the high accuracy obtainable, the use of a digital computer is preferred to an analog machine for the integration of the ray equations. The method used solves the first n of a set, N, of first-order differential equations simultaneously. The Adams-Moulton open and/or open and closed formulas are used. A Runge-Kutta fourth-order integrator is used as a starting routine to generate the necessary differences. Provision is made for interrupting the integration process at specific values of either the independent or dependent variables. The order of differences used in the Adams-Moulton mode is less than or equal to nine.

A complete description of the integration package is found in Appendix A.

### II. USER'S MANUAL

### Introduction

This User's Manual is intended to supply all the information and guidelines necessary for a non-programmer to operate the ray-tracing program.

### Inputs

In order to facilitate using this program, the NAMELIST feature of FORTRAN IV is used. This input mode has two distinct advantages over a fixed format statement:

- (1) It minimizes keypunching errors
- (2) When stacking cases, it minimizes the size of the input deck

NAMELIST allows for a free format input stream; the data can be placed anywhere on the card and spaced in any convenient manner. The basic rules the user must keep in mind when constructing an input deck are outlined in section III. For a detailed description of the NAMELIST feature see IBM form C28-6390.

IBM 7090-7094 IBSYS operating system, version 13, FORTRAN IV language.— It has been found that when stacking data sets for running as many cases as possible, there is usually some similarity among successive sets. NAMELIST allows the user to take maximum advantage of any similarity.

The first data set in the stack must contain all data required by the program for normal operation. Each successive data set, however, must specify only those parameters whose values differ from immediately preceding case.

We consider the input data to be of three distinct types:

- (1) Data which is required for the normal operation of the program and must be supplied by the user
- (2) Optional integration control parameters
- (3) Optional plotting limits

Detailed descriptions of these three data types can be found in the following paragraphs.

Input dictionaries. The input is under control of three dictionaries. The first dictionary, XNAME1, refers to the required program inputs. The remaining dictionaries, XNAME3 and XNAME5, refer to the optional integration and plot parameters, respectively.

Required input - XNAME1. - Figure 6 shows a sample input deck for the required inputs. The dictionary for these inputs consists of five names: D, LAST, NTITLE, NCONST, and LIMITS. The first name, D, is a 28-word array containing all the data about the initial position of the ray, direction and ray characteristics. The four remaining names are single word indicators. An explanation of each of the required inputs follows.

Darray. Table II contains an item by item description of each of the parameters in the Darray. The subscript shown in the left-hand column indicates the position in the array. The subscript of the first item must be punched and then the remaining items will be stored sequentially. Figure 7 is a graphical illustration of the initial ray-position input parameters specified by D(1) through D(6).

### TABLE II

### D ARRAY

D	DESCRIPTION
1	Initial geocentric radius, ro, in kilometers
2	Initial colatitude, $\theta_{O}$ , in degrees. (0 $\leq$ 0 $\leq$ 180)
3	Initial longitude, $\phi_0$ , in degrees. (0 $\leq$ $\phi$ $\leq$ 360)
4	Initial ray angle, A , with respect to the local vertical, in degrees. (000 $\leq$ A $_{\odot}$ $\leq$ 1800)
	NOTE
	A is no longer a program input.
	${f A_O}$ is calculated from ${f \Delta A_O}$ . How-
	ever, the location D(4) is still
	reserved for A <sub>o</sub> .
5	Initial ray angle, B , with respect to the south vector, in degrees. (0° $\leq$ B o $\leq$ 360°)
6	Initial ray angle, $\Delta A$ , with respect to the tangent of the field line in degrees: $(0 \le \Delta A_{\odot} \le 180^{\circ})$
7	Maximum allowable geocentric radius, R <sub>max</sub> , in kilometers

### TABLE II.- Continued

### D ARRAY

D	Description
8	Minimum allowable geocentric radius, R in kilometers
9	Maximum allowable colatitude, $\theta_{\text{max}}$ , in degrees. (0° $\leq$ $\theta_{\text{max}}$ $\leq$ 180°)
10	Minimum allowable coatitude, $\theta_{\min}$ , in degrees. $(0^{\circ} \leq \theta_{\min} \leq 180^{\circ})$
11	Maximum allowable longitude, $\phi_{\text{max}}$ , in degrees. (0° $<$ $\phi_{\text{max}}$ $<$ 360°)
12	Minimum allowable longitude, $\phi_{\min}$ , in degrees. (0° $\leq \phi_{\min} \leq 360^{\circ}$ )
13	Print interval in kilometers. Printed output is keyed to phase path length
14	Plot interval in kilometers. Plotted output is keyed to phase path length. It has nothing to do with the Print Interval. It is only a control of the spacing of the points to be plotted.
15	Nominal integration step size, in kilometers. Integrations are with respect to phase path length
16	Wave frequency, F, in megacycles per second
17	Ray type indicator:
	Set equal to 1 for ordinary type, or Set equal to -1 for extraordinary type
18	Reflection indicator:
	Set equal to 2 if reflection is desired, 0 otherwise. Ordinarily, reflection occurs whenever the rate of change of geocentric radius goes to zero
19	Powerloss calculation indicator:
	Set equal to 1 if computation is desired, 0 otherwise

### TABLE II.- Concluded

### D ARRAY

D	Description
20	Plot option indicator:
	Set equal to 1 if plotting is desired, 0 otherwise
21	Plot overlay option indicator:
	Set equal to 1 if overlaying of successive plots is desired, 0 otherwise. Ignored if NPLOT = 0
22	Automatic positioning of ray at point of maximum electron density gradient indicator:
	Set equal to 1 if automatic positioning is desired, 0 otherwise
23	Scale size of the ionization irregularity at the base of the field line $\rm^{H}_{O}$
24	Peak fractional enhancement at $(r_0, \theta_0, \phi_0)$ where $r_0$ is the initial geocentric radius, $\theta_0$ is the initial colatitude and $\phi_0$ is the initial longitude
25	Colatitude, $\lambda\text{,}$ in degrees of the field-line passing through the initial ray position.
26,2	7,28 Not used

Figure 6. - Sample Deck Setup

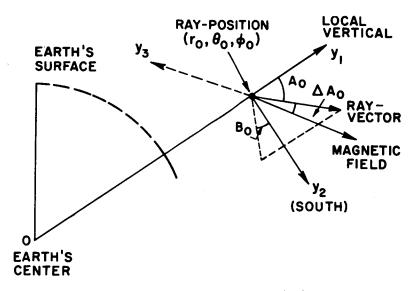


Figure 7. - Initial Ray - Position Inputs

Required indicators. - The remaining inputs under control of XNAMEl are four indicators described in Table III.

TABLE III
REQUIRED INPUT INDICATORS

Name	Description
LAST	Last Case Indicator:
	The program assumes LAST = 0, so the last case to be executed must explicitly set this parameter to 1
NTITLE	Optional Title Information:
	NTITLE preset to 0. If some identifi- cation is to be printed, set NTITLE = 1
NCONST	Optional Input Indicator, Integration Para- meters:
	The program assumes NCONST = 0. If the integration parameters are to be changed, set NCONST = 1
LIMITS	Optional Input Indicator, Plotting Limits:
	The program assumes LIMITS = 0. If the plotting limits are to be changed set LIMITS = 1

Optional input. The parameters described here are preset by the program. However, the user can replace any subset of these parameters by setting the values of NCONST and/or LIMITS equal to 1 and then punching a set of data cards using the dictionary XNAME3 and/or XNAME5. These cards must follow the statement card if NTITLE = 1 or immediately following the required inputs if NTITLE = 0.

Integration parameters - XNAME3. - The optional integration parameters are under control of the dictionary XNAME3. The dictionary contains seven names representing seven data items. Table IV defines each parameter and gives its nominal value. Appendix A contains a description of the integration routine.

TABLE IV (XNAME3)

# Integration Parameters

Name	Nominal Value	Descri <b>pt</b> ion
ORDER	1.0	Precision option. When set to 0 the integration is carried out in partial double precision, set to 1.0 integration is performed in full double precision
EUBAR	1.0E-5	Maximum integration error. When the integration error is greater or equal to this value the integration interval is halved
ELBAR	1.0E-7	Minimum integration error. When the integration error is less than or equal to this parameter the integration step is doubled
YCLOW	1.0E.7	Minimum value of the dependent variable. If the dependent variable is less than or equal to this parameter no halving will take place
НМАХТ	1.0E+4	Maximum integration step. The integration step is not permitted to exceed this value
HMINT	1.0E-7	Minimum integration step. The integra- tion step is not allowed to be smaller than this input
KD	4	Type of integration (must always equal 4)

Plot limits (XNAME5). - The optional plot limits are under the control of dictionary XNAME5. This dictionary contains eight names. Table V defines each limit and its nominal value.

#### TABLE V (XNAME5)

PLOT LIMITS

Name	Nominal Value	Description
XMINO	0.0	Minimum value of the X-axis for the rectangular plot.
OXAMX	1.20E4	Maximum value of the X-axis for the rectangular plot.
YMINO	-18.0	Minimum value of the Y-axis for the rectangular plot.
OXAMY	+2.0	Maximum value of the Y-axis for the rectangular plot.
XMIN1	0.0	Minimum value of the X-axis for the Polar Plot.
XMAX1	2.0E4	Maximum value of the X-axis for the Polar Plot.
YMIN1	0.0	Minimum value of the Y-axis for the Polar Plot.
YMAX1	1.0E4	Maximum value of the Y-axis for the Polar Plot.

Input conventions. - The following is a listing of a few simple rules the user must keep in mind when constructing an input deck:

- 1. Column 1 of each input card is not to be used. Any information punched in this column will be ignored.
- 2. The first character encountered by the input system must be a dollar sign (\$) punched in column 2 of the first card of each group of inputs.
- 3. All data must be separated by commas. The input system assumes that any single input quantity must lie between an equal sign and a comma, or between two commas.
- 4. All numerical data can be entered in either a fixed decimal or exponential format. Whenever a decimal point does not appear within a number, in the case of the fixed decimal format, the system assumes that it is in front of the separator and all trailing blanks (i.e., no punches) will be

converted to zeroes. In the case of the exponential format the decimal point is assumed to lie to the right of the least significant digit. As an illustration, the following list of numbers will have identical binary representations in core storage:

2500.0 25bb fixed decimal (b-blank, no punch) 25E+2 2.5E+3 exponential format

Note that in the above illustration the exponent is separated from the significant part of the number by the letter E.

5. The NAME LIST system allows for continuation cards. If continuation cards are used then the user must be careful in placing the input cards in proper order. When using continuation cards the name of the table, (array) need not be repeated. The only limitations are that column 1 is not to be used and each card must end with a comma.

This program allows the user to execute several cases within a single run. This is done by first setting the indicator, NA, equal to zero within the first set of input and then for each of the following cases simply punch the dictionary name with the proper system symbols and then specify only those inputs which are to differ from the immediately preceding case. The inputs for each case are then placed behind each other, no separator cards are required, and the resulting input deck is placed behind the binary deck as described earlier.

6. The end of an input string is indicated by a dollar sign (\$). The input system will continue reading until the second dollar sign is encountered.

# Operating Instructions

Deck setup.- The following is a list of the control cards
necessary to compile and execute the program in source form:

CC CC CC 1 8 16

\$JOB D3121A 1 ERC J. Ramasastry - TRACE \$EXECUTE IBJOB \$IBJOB FIOCS

\$IBFTC M	AIN				
		MAIN	PROGRA	ΔM	(SOURCE)
\$IBFTC I		SUBRC	UTINE	INPUT	(SOURCE)
\$IBFTC O	UTPU				
\$IBFTC F		SUBRC	UTINE	OUTPUT	(SOURCE)
		SUBRO	UTINE	FIELD	(SOURCE)
\$IBFTC D	ENS	SUBRO	UTINE	DENSE	(SOURCE)
\$IBFTC C	OL				
\$IBFTC C.	AT CO	SUBRO	UTINE	COLL	(SOURCE)
VIDITE C.	ADCO	SUBRO	OUTINE	CALCO4	(SOURCE)
\$IBFTC S	CA	CIIDDO	NIM T NIE	DDAM	(COUDCE)
\$IBFTC F	ORC	SUBRC	DUTINE	PRAM	(SOURCE)
		SUBRO	DUTINE	FORCE	(SOURCE)
\$IBFTC P	OLA	SUBRO	OUTINE	POLAR	(SOURCE)
\$IBFTC P	OWER				
\$IBFTC M	LARS	SUBRO	DUTINE	POWERL	(SOURCE)
		SUBRO	OUTINE	MARK	(SOURCE)
\$IBFTC S	SMK2	SUBRO	OUTINE	SMARK	(SOURCE)

SIBFTC CST

SUBROUTINE CSINT (SOURCE)

\$IBFTC MIN

SUBROUTINE MINV

(SOURCE)

\$IBFTC TO

SUBROUTINE TOR

(SOURCE)

\$DATA

DATA DECK

END OF FILE CARD

I/O assignments. - The program uses the standard ERC-IBM 7094-II assignments. The FORTRAN IV logical units are 5 and 6, respectively. If a plot is to be generated a tape must be mounted on SYSUT7.

Abnormal termination. - The program recognizes three types of abnormal terminations:

- (1) An error in the integration routine. The message, ERROR RETURN FROM MARK is printed. The program will continue on to the next case.
- (2)  $\mu^2 \leq 0$

The message, THE VALUE OF EMUS IS NEGATIVE is printed. The program will continue on to the next case.

(3)  $1 - x \le 0$ 

The message, THE VALUE OF TERM IS NEGATIVE is printed. The program will continue on to the next case.

#### III. PROGRAMMER'S MANUAL

#### Introduction

This Programmer's Manual contains all the technical information required by a programmer whose task it may be to modify the program.

Each subroutine is described separately. Each description generally consists of:

- (1) The mathematical formulation of the computations
- (2) A flow chart of the routine
- (3) A dictionary of the FORTRAN variables calculated in the routine

Following the subroutine descriptions the labeled COMMON statements are correlated with the subroutines in which they are used.

Source statement lists of all the subroutines are provided in Appendix B.

# Main Program

<u>Description</u>. - The main program, MAIN, serves as an executive routine. (See flow chart in Figures 8A to 8H.) The functions of MAIN are:

- (1) Initialization of the integration routine
- (2) Computation of the derivative box
- (3) Handling of trigger stops

The integration routine has a return indicator, NRTN, which, when tested, determines the order of calculations.

Upon return from the integration routine, the variable NRTN is set to an integer value from 1 to 5. NRTN is used to control program flow. Table VI indicates the action taken when NRTN assumes a particular value.

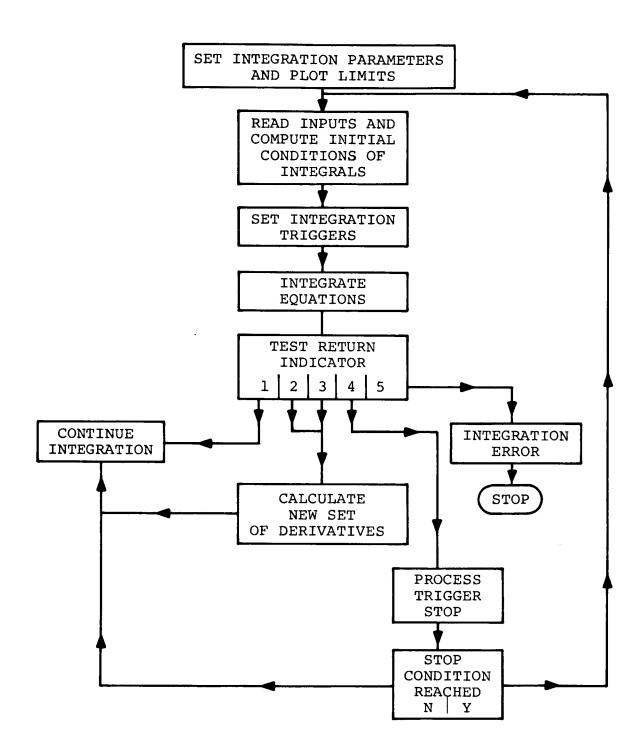


Figure 8A. - Flow Chart of Main Program

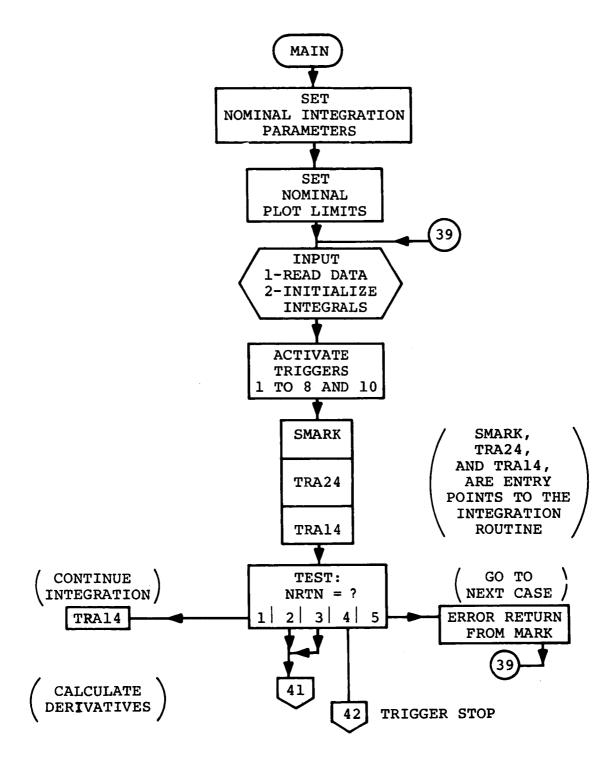


Figure 8B. - Flow Chart of Main Program

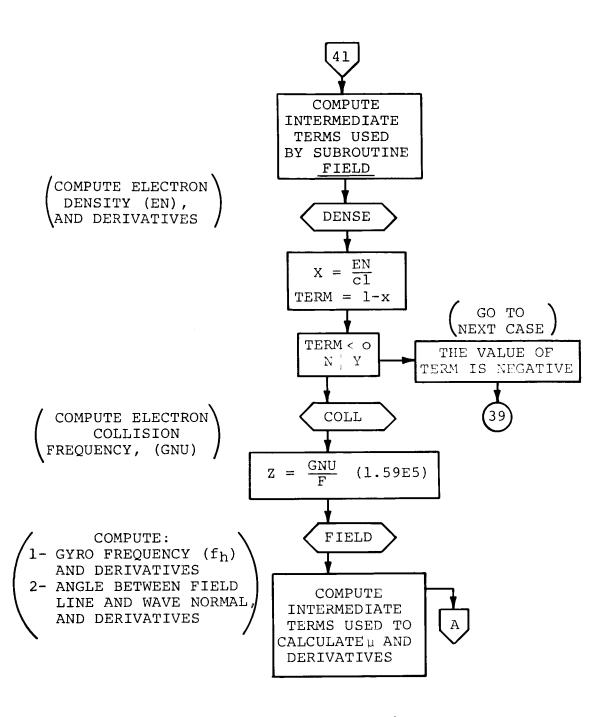


Figure 8C. - Flow Chart of Main Program

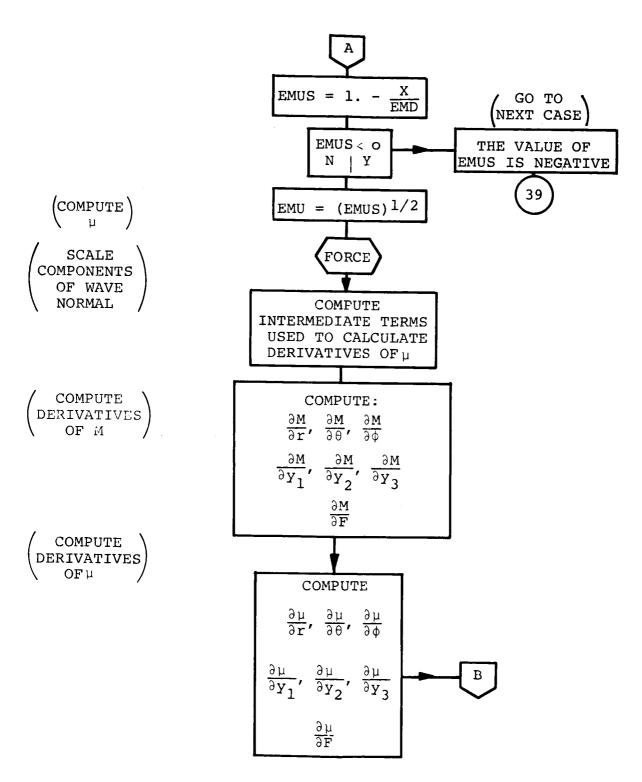


Figure 8D. - Flow Chart of Main Program

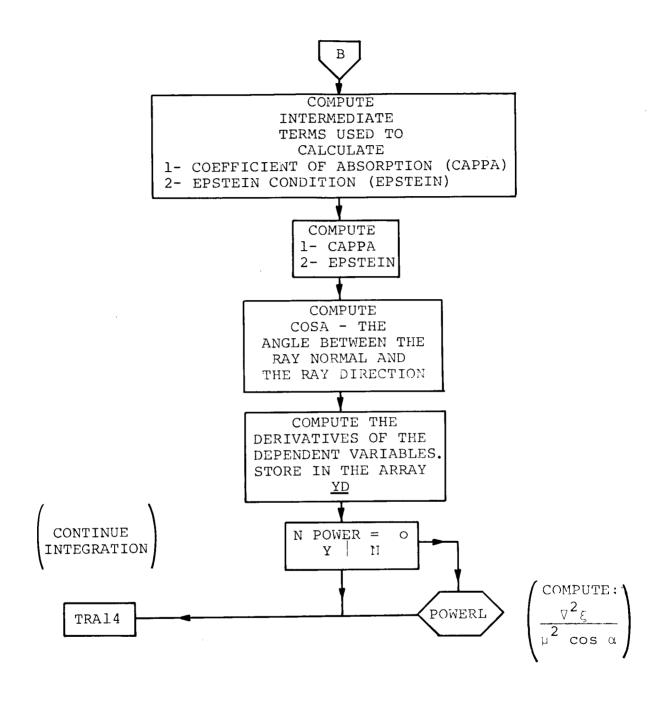


Figure 8E. - Flow Chart of Main Program

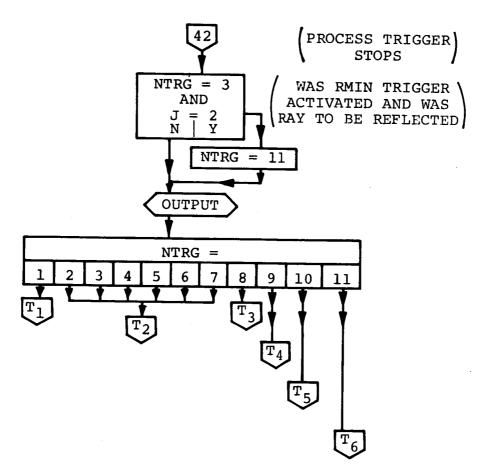
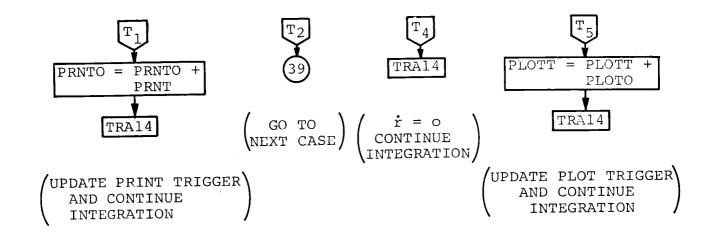


Figure 8F. - Flow Chart of Main Program



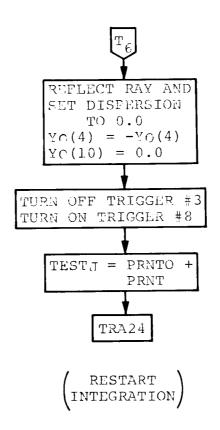


Figure 8G. - Flow Chart of Main Program

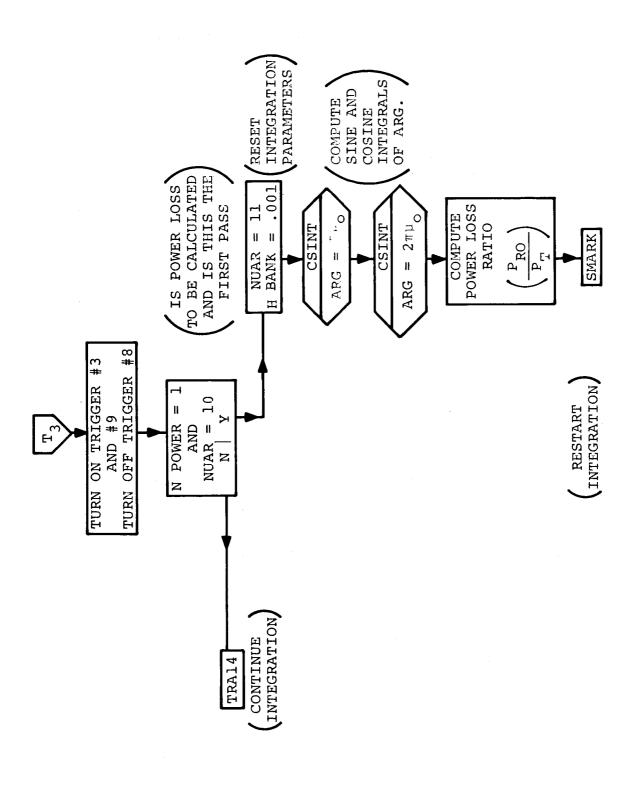


Figure 8H. - Flow Chart of Main Program

TABLE VI

ACTION TAKEN WITH REFERENCE TO RETURN INDICATOR

NRTN	
1	Return control to the integration routine.
2	Transfer control to DER1, the derivative box inclusive of any calculations which involve the independent variable.
3	Transfer control to DER2, the derivative box exclusive of any calculations which involve the independent variable.
	NOTE
	In this application, the independent variable is never used explicitly so for NRTN = 2 and NRTN = 3, control is transferred to DER2.
4	A trigger stop has occurred, process trigger stop.
5	An error has occurred during integration. The message ERROR RETURN FROM MARK will be printed and the program will stop.

Trigger stops are used to interrupt the integration routine at predetermined points. This program uses ten triggers. If a trigger stop occurs (i.e., NRTN = 4), the trigger indicator, NTRG, is set to an integer value from 1 to 10. The value assumed by NTRG corresponds to the trigger activated by the integration routine, MARK.

Table VII correlates the value of NTRG, the trigger activated and the sequence of actions taken.

# SEQUENCE OF ACTIONS TAKEN WITH REFERENCE TO TRIGGER INDICATOR

TABLE VII

NTRG	
1	Print interval: call OUTPUT to print data, update trigger, return control to MARK.
2	The geocentric radius, r, has reached $R_{\text{max}}$ : call OUTPUT to print data, if NPLOT $\geqslant$ 0 plot data, print end of case message, call INPUT to process next case.
3	The geocentric radius, r, has reached $R_{min}$ : if reflection indicator, JTEST, does not equal two, the procedure is the same as for NTRG = 2, if JTEST = 2, the ray is reflected from a plane perpendicular to $\vec{r}$ and control is returned to the integration routine.
4	$\theta > \theta_{\text{max}}$ : the procedure is the same as for NTRG = 2.
5	$\theta \leqslant \theta_{\text{min}}$ : the procedure is the same as for NTRG = 2.
6	$\varphi \geqslant \varphi_{\mbox{\scriptsize max}} \colon$ the procedure is the same as for NTRG = 2.
7	$\varphi \leqslant \varphi_{\mbox{min}} \colon$ the procedure is the same as for NTRG = 2.
8	Phase path, h <sub>p</sub> , has reached a value indicated by TESTJ: the stop on TESTJ has two functions. The first is to delay the start of the power loss calculation until the ray has traveled enough to be considered in the far field. It also turns on the trigger for a reflection stop when the ray has gone a specified distance past the reflection.

### TABLE VII. - Concluded

# SEQUENCE OF ACTIONS TAKEN WITH REFERENCE TO TRIGGER INDICATOR

NTRG	
9	. r = 0: call OUTPUT to print data, and store current values of r, $\theta$ , and $\phi$ in plotting arrays, print value of r, return control to MARK.
10	Plot interval: store current values of r, $\theta$ , and $\phi$ in plotting arrays, update trigger, return control to MARK.

Differential equations evaluated in the MAIN PROGRAM.— The following equations form a closed system for tracing the rays. The ray is described in terms of position in spherical coordinates with the origin at the center of the Earth and in terms of the components of the wave normal,  $Y_1$ ,  $Y_2$ ,  $Y_3$  in the r,  $\theta$ ,  $\phi$  directions, respectively.

#1 
$$\dot{\mathbf{r}} = \frac{1}{\mu^2} \left( \mathbf{Y}_{1N} - \mu \frac{\partial \mu}{\partial \mathbf{Y}_1} \right)$$
 ;  $\mathbf{r}(0) = \mathbf{r}_0$ 

#2 
$$\dot{\theta} = \frac{1}{r\mu^2} \left( Y_{2N} - \mu \frac{\partial \mu}{\partial Y_2} \right)$$
 ;  $\theta(0) = \theta_0$ 

#3 
$$\dot{\phi} = \frac{1}{r_{\mu}^2 \sin \theta} \left( Y_{3N} - \mu \frac{\partial \mu}{\partial Y_3} \right)$$
 ;  $\phi(o) = \phi_o$ 

#4 
$$\dot{Y}_1 = \frac{1}{\mu} \frac{\partial \mu}{\partial r} + \dot{\theta} Y_2 + \dot{\phi} Y_3 \sin \theta$$
 ;  $Y_1(0) = Y_{10}$ 

#5 
$$\dot{\mathbf{Y}}_{2} = \frac{1}{\mathbf{r}} \left[ \frac{1}{\mu} \frac{\partial \mu}{\partial \theta} - \dot{\mathbf{r}} \mathbf{Y}_{2} + \dot{\phi} \mathbf{Y}_{3} \mathbf{r} \cos \theta \right] \qquad ; \quad \mathbf{Y}_{2}(0) = \mathbf{Y}_{20}$$

#6 
$$\dot{\mathbf{Y}}_{3} = \frac{1}{\mathrm{rsin}\theta} \left[ \frac{1}{\mu} \frac{\partial \mu}{\partial \phi} - \dot{\mathbf{r}} \mathbf{Y}_{3} \sin \theta - \dot{\theta} \mathbf{Y}_{3} \cos \theta \right] ; \mathbf{Y}_{3}(0) = \mathbf{Y}_{30}$$

where Y in are components of the normalized Y-vector, i.e.,

$$\sum_{i=1}^{3} Y_{in}^2 = \mu^2$$

 $\vec{Y}$  is normalized by subroutine FORCE. The symbols r,  $\theta$ ,  $\phi$ ,  $Y_1$ ,  $Y_2$ ,  $Y_3$  are derivatives with respect to phase path length,  $h_p$  (the independent variable), in kilometers. The symbol  $\mu$  is the phase refractive index.

The simplified Appleton-Hartree expression for the phase refractive index is used. It is given by

$$\mu^{2} = 1 - \frac{X}{1 - M + \sqrt{M^{2} + Y_{L}^{2}}}$$

and the collisions are neglected.

The appropriate algebraic sign (+) in the denominator is chosen according to the indicator supplied by the user via the required input D(17). The plus (+) sign refers to ordinary rays and the minus (-) sign refers to extra-ordinary rays.

$$X = \frac{e^2 N}{\epsilon_0 m (2\pi f)^2} = \frac{N}{12400. f^2} = \frac{N}{C_1}$$

N = electron density in electrons per cc

f = frequency of propagation in megacycles
 per second

e = charge of an electron

m = mass of an electron

 $\varepsilon_{\circ}$  = permittivity of free space

$$C_1 = \frac{\epsilon_0 m(2\pi f)^2}{e^2} = 12400.f^2$$

$$\mathbf{M} = \frac{\frac{1}{2} \mathbf{Y}_{\mathbf{T}}^2}{1 - \mathbf{X}}$$

$$Y_{\dot{T}} = \frac{f_H \sin \psi}{f}$$

$$Y_{L} = \frac{f_{H} \cos \psi}{f}$$

 $f_{H}$  = gyrofrequency in megacycles per sec

 $\psi$  = angle between the magnetic field and the wave normal

The problem is now reduced to one of finding N,  $f_H$  and  $\psi$  and their derivatives with respect to r,  $\theta$ ,  $\phi$ ,  $Y_1$ ,  $Y_2$  and  $Y_3$ . The initial coordinates of the ray-position  $(r_0$ ,  $\theta_0$ ,  $\phi_0)$  and the initial ray direction  $(Y_{10},\,Y_{20},\,Y_{30})$  and the wave-frequency, f, should be known. Thus, for a given electron density (N) and magnetic field  $(f_H$  and  $\psi)$ , one can trace rays of any frequency from any point. This is subject to the constraint that  $\mu^2 \geqslant 0$ . The local values of electron density,  $N(r,\,\theta,\,\phi)$ , and the magnetic field,  $f_H(r,\,\theta,\,\phi)$  and  $\mu(r,\,\theta,\,\phi,\,Y_1,\,Y_2,\,Y_3)$  are derived from the respective models.

For Hamilton's equations, one must evaluate  $\partial \mu/\partial r$ ,  $\partial \mu/\partial \theta$ ,  $\partial \mu/\partial \Psi_1$ ,  $\partial \mu/\partial \Psi_2$  and  $\partial \mu/\partial \Psi_3$ .

$$\frac{\partial \mu}{\partial r} = \frac{1}{2\mu M_{R}} \cdot \left\{ -\frac{1}{C_{1}} \frac{\partial N}{\partial r} + \frac{N}{C_{1} M_{R}} \left[ -\frac{\partial M}{\partial r} + \frac{1}{C_{1} M_{R}} \left( -\frac{\partial M}{\partial r} + \frac{1}{C_{1} M_{R}} + \frac{1}{C_{1} M_{R}} \left[ -\frac{\partial M}{\partial r} + \frac{1}{C_{1} M_{R}} \left[ -\frac{\partial M}{\partial r} + \frac{1}{C_{1} M_{R}} + \frac{1}{C_{1} M_{R}} + \frac{1}{C_{1} M_{R}} + \frac{1}{C_{1} M_{R}} \left[ -\frac{\partial M}{\partial r} + \frac{1}{C_{1} M_{R}} + \frac{1}{C_{1} M_{R$$

$$\begin{split} \frac{\partial \mu}{\partial \theta} &= \frac{1}{2\mu M_{R}} \cdot \left\{ -\frac{1}{C_{1}} \quad \frac{\partial N}{\partial \theta} \, + \, \frac{N}{C_{1} M_{R}} \left[ -\frac{\partial M}{\partial \theta} \, \pm \, \frac{1}{R} \left( M \, \frac{\partial M}{\partial \theta} \, + \, \frac{Y_{L}^{2}}{f_{H}} \, \frac{\partial f_{H}}{\partial \theta} \right. \right. \\ & \left. + \cos \psi \, \frac{f_{H}^{2}}{f^{2}} \, \frac{\partial \cos \psi}{\partial \theta} \, \right) \right] \right\} \end{split}$$

$$\frac{\partial \mu}{\partial \phi} = \frac{1}{2\mu M_{R}} \cdot \left\{ -\frac{1}{C_{1}} \frac{\partial N}{\partial \phi} + \frac{N}{C_{1}M_{R}} \left[ -\frac{\partial M}{\partial \phi} \pm \frac{1}{R} \left( M \frac{\partial M}{\partial \phi} + \frac{Y_{L}^{2}}{f_{H}} \frac{\partial f_{H}}{\partial \phi} + \cos \psi \frac{f_{H}^{2}}{f^{2}} \frac{\partial \cos \psi}{\partial \phi} \right) \right] \right\}$$

$$\frac{\partial \mu}{\partial y_1} = \frac{1}{2\mu M_R^2} \left\{ \frac{N}{C_1} \left[ -\frac{\partial M}{\partial y_1} \pm \frac{1}{R} \left( M \frac{\partial M}{\partial y_1} + \cos \psi \frac{f_H^2}{f_1^2} - \frac{\partial \cos \psi}{\partial Y_1} \right) \right] \right\}$$

$$\frac{\partial \mu}{\partial \mathbf{y}_2} = \frac{1}{2\mu \mathbf{M}_{\mathbf{R}}^2} \left\{ \frac{\mathbf{N}}{\mathbf{C}_1} \left[ \frac{\partial \mathbf{M}}{\partial \mathbf{y}_2} \pm \frac{1}{\mathbf{R}} \left( \mathbf{M} \frac{\partial \mathbf{M}}{\partial \mathbf{y}_2} + \cos \psi \frac{\mathbf{f}_{\mathbf{H}}^2}{\mathbf{f}^2} - \frac{\partial \cos \psi}{\partial \mathbf{y}_2} \right) \right] \right\}$$

$$\frac{\partial \mu}{\partial y_3} \ = \ \frac{1}{2\mu M_R^2} \left\{ \frac{N}{C_1} \left[ - \ \frac{\partial M}{\partial y_3} \ \pm \ \frac{1}{R} \left( \ M \ \frac{\partial M}{\partial y_3} + \cos \psi \ \frac{f_H^2}{f^2} \ \frac{\partial \cos \psi}{\partial y_3} \right) \right] \right\}$$

$$\frac{\partial \mathbf{M}}{\partial \mathbf{r}} = \frac{1}{2\mathbf{f}^{2}(1-\mathbf{x})} \left\{ 2\mathbf{f}_{\mathbf{H}} \sin^{2} \psi \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \mathbf{r}} + \mathbf{f}_{\mathbf{H}}^{2} \sin \psi \frac{\partial \sin \psi}{\partial \mathbf{r}} + \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}_{\mathbf{L}}^{2}} \sin^{2} \psi \frac{\partial \mathbf{N}}{\partial \mathbf{r}} + \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}_{\mathbf{L}}^{2}} \sin^{2} \psi \frac{\partial \mathbf{N}}{\partial \mathbf{r}} \right\}$$

$$\frac{\partial M}{\partial \theta} \; = \; \frac{1}{2f^2(1-X)} \; \left\{ 2f_H \sin^2 \psi \;\; \frac{\partial f_H}{\partial \theta} \; + \; f_H^2 \sin \psi \; \frac{\partial \sin \psi}{\partial \theta} \; + \; \frac{\frac{f_H^2}{C_1} \; \sin^2 \psi \; \frac{\partial N}{\partial \theta}}{1 \; - \; X} \right\}$$

$$\frac{\partial M}{\partial \phi} = \frac{1}{2f^2(1-X)} \left\{ 2f_H \sin^2 \! \psi \, \frac{\partial f_H}{\partial \phi} \, + \, f_H^2 \sin \! \psi \, \frac{\partial \sin \! \psi}{\partial \phi} \, + \, \frac{\frac{f_H^2}{C_1} \, \sin^2 \! \psi \, \frac{\partial N}{\partial \phi}}{1-X} \right\}$$

$$\frac{\partial M}{\partial Y_1} = \frac{1}{(1-X)} \frac{f_H^2}{f^2} \sin \psi \frac{\partial \sin \psi}{\partial Y_1}$$

$$\frac{\partial M}{\partial Y_2} = \frac{1}{1-X} \frac{f^2_H}{f^2} \sin \psi \frac{\partial \sin \psi}{\partial Y_2}$$

$$\frac{\partial M}{\partial Y_3} = \frac{1}{1-X} \frac{f_H^2}{f^2} \sin \psi \frac{\partial \sin \psi}{\partial Y_3}$$

$$\frac{\partial \mu}{\partial f} = \frac{X}{2\mu M_{\mathbf{p}}^2} \left\{ -\frac{Y_{\mathbf{T}}Y_{\mathbf{L}}}{1-X} + \frac{1}{R} \left( M \frac{Y_{\mathbf{T}}Y_{\mathbf{L}}}{1-X} - Y_{\mathbf{T}}Y_{\mathbf{L}} \right) \right\}$$

where

$$R = \sqrt{M^2 + Y_L^2}$$

$$M_{R} = 1 - M + R$$

The derivatives of N are calculated in DENSE (subroutine).

The derivatives of  $\,\psi\,\,$  and  $\,f_{\mbox{\scriptsize H}}^{}\,\,$  are calculated in FIELD (subroutine).

Other differential equations evaluated. - Group path length, ray path length, power loss due to absorption, doppler shift, and power loss along the ray's path are the other differential equations evaluated and are discussed as follows:

(1) Group Path Length

$$\dot{G}_{L} = 1 + \frac{f}{\mu} \frac{\partial \mu}{\partial f}$$

$$G_{T_{i}}(o) = 0$$

 $\mathbf{G}_{\mathbf{T}_{\mathbf{L}}}$  is measured in km

Group delay is determined by

$$G_D = \frac{1}{c} G_L$$

where

 $c = 3.0 \times 10^5 \text{ km/sec} \equiv \text{velocity of light}$ 

(2) Ray Path Length

$$\dot{s} = \frac{1}{\mu \cos \alpha}$$

$$S(0) = 0$$

S is measured in km

- $\alpha$  is the angle between the wave normal and and the ray direction
- (3) Power Loss Due To Absorption

$$\dot{D} = - 2 \frac{K}{\mu} D$$

$$D(0) = 1.0$$

$$K = \frac{2\pi fk}{C}$$

where

D = power loss due to absorption

k = index of absorption

K = coefficient of absorption

$$k = \frac{BX}{2\mu(A^2 + B^2)} \qquad X = \frac{Ne^2}{\epsilon_0 m(2\pi f)^2}$$

$$A = 1 - \frac{\frac{1}{2} \frac{f_{H}^{2}}{f^{2}} \sin^{2} \psi(1-X)}{(1-X)^{2} + Z^{2}} + \left\{ \frac{1}{2} \left[ U + (U^{2} + V^{2})^{1/2} \right] \right\}^{1/2}$$

$$B = Z + \frac{\frac{1}{2} Z \frac{f_{H}^{2}}{f^{2}} \sin^{2} \psi}{(1-X)^{2} + Z^{2}} + \frac{V}{2 \left\{ \frac{1}{2} \left[ U + (U^{2} + V^{2})^{1/2} \right] \right\}^{1/2}}$$

$$U = \left[\frac{\frac{1}{2}y^2 \sin^2 \psi (1-X)}{(1-X)^2 + z^2}\right]^2 - \left[\frac{\frac{1}{2}zy^2 \sin^2 \psi}{(1-X)^2 + z^2}\right]^2 + y^2 \cos \psi$$

$$V = 2 \frac{\frac{1}{2} y^2 \sin^2 \psi (1-X)}{(1-X)^2 + Z^2} \cdot \frac{\frac{1}{2} y^2 \sin^2 \psi Z}{(1-X)^2 + Z^2}$$

where

$$y = \frac{f_H}{f}$$
 
$$Z = \frac{v}{2\pi f} \qquad v = \text{collision frequency in collisions per sec}$$

 $\nu$  is given by the collision frequency model. The collision frequency model is described in subroutine COLL.

(4) Doppler Shift 
$$\Delta f = -\frac{f}{c} \int_{r_0}^{r} \mu \cos \alpha \, ds \; ; \qquad \Delta f(o) = 0$$

Δf is the Doppler-Shift in MHz

c is the velocity of light

f is the wave frequency om MHz

 $\boldsymbol{\mu}$  is the phase refractive index

(5) Power Loss Along the Path of the Ray
The total power loss in dB is:

$$10 \log_{10} \left\{ \frac{c^2}{4\pi f^2} \times \frac{P_r}{P_T} \times \frac{\mu_{Final}}{\mu_o} \text{ EXP(E}_1) \times \text{EXP(E}_2) \right\}$$

$$E_1 = -\int_{s_t}^{s_L} \frac{\nabla^2 \xi}{\mu} ds$$

$$E_2 = -2 \int_{s_0}^{s_1} \alpha_{ABS} ds$$

where

$$ds = \frac{dh_p}{\mu \cos \alpha}$$

s = ray path length

 $h_{p}$  = phase path length

$$\frac{c^2}{4\pi f^2}$$
 = isotropic radiator aperture loss

$$\frac{P_{ro}}{P_{T}}$$
 = near field loss due to refraction and inverse square law spreading

$$\text{EXP} \left[ - \int_{s_0}^{s_t} \alpha_{ABS} \, ds \right] = \text{power loss due to absorption}$$

 $\alpha_{\mbox{\scriptsize ABS}}$  is related to the absorption coefficient, K, of the wave by the expression

$$\alpha_{ABS} = K \cos \alpha$$
.

Then the term

EXP 
$$\left[ \begin{array}{cc} -2 & \int_{\mathbf{s}_{\mathbf{0}}}^{\mathbf{s}_{\mathbf{t}}} & \alpha_{\mathbf{ABS}} \, \mathrm{ds} \\ \end{array} \right]$$

is equivalent to D, the power loss due to absorption.

Power loss in the near field. The power losses in the near field is calculated in MAIN. It is evaluated only once, when the ray has traveled far enough to be considered in the far field.

 $\rm ^{p}_{RO}/\rm ^{p}_{T}$  gives the power loss in the near field from  $\rm s_{O}$  to  $\rm s_{t}$  due to refraction and inverse square law spreading. The equation given below is for a dipole antenna.

r' and  $\gamma$  are shown in the following Figure 9.

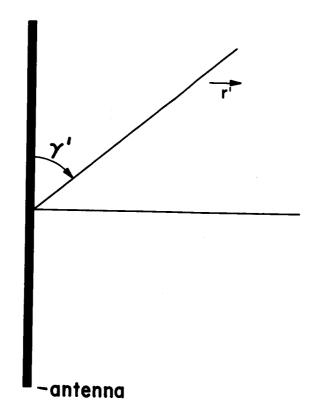


Figure 9.- Dipole antenna defined.

Let

$$C_{i}(P) = - \int_{P}^{\infty} \frac{\cos(x)}{x} dx$$

$$C_{i}(P) = \int_{0}^{P} \frac{\sin(x)}{x} dx$$

then

$$\frac{P_{RO}}{P_{T}} = \frac{\left[\frac{\cos (T \cos \gamma') - \cos \left(\frac{1}{2}T\right)}{\sin \gamma'}\right]^{2}}{2\pi (r')^{2}A_{1}}$$

$$T = \pi \mu_{o}$$

$$(\mathbf{r})^2 = \mathbf{r}_0^2 + \mathbf{r}^2 - 2\mathbf{r}_0\mathbf{r}\cos\gamma$$

 $\cos \gamma = \sin(\theta_0)\sin(\theta)\cos(\phi_0 - \phi) - \cos(\theta_0)\cos(\theta)$ 

$$\gamma' = \pi - \cos^{-1} \left[ \frac{(r')^2 + (r_0^2) - r^2}{2r'r_0} \right]$$

$$A_1 = .5772 + ln(T) - C_i(T)$$

$$+ \frac{1}{2} \sin(T) \left[ S_i(2T) - 2S_i(T) \right]$$

$$+\frac{1}{2}\cos(T)\left[C_{i}(2T)-2C_{i}(T)\right]$$

$$+\frac{1}{2}\cos(T)\left[.5772 + \ln(\frac{1}{2}T)\right]$$

Program Notes .- The program variable PROPT is actually

$$\frac{c^2}{4\pi f \mu_0 \times 10^{12}} \qquad x \quad \frac{P_{ro}}{P_{T}}$$

where

$$c = the velocity of light in km/sec$$
  
=  $3 \times 10^5 km/sec$ 

Power loss in the far field. - The term

$$\frac{\mu_{\text{Final}}}{\mu_{\text{o}}} \quad \int_{\mathbf{s}_{\text{t}}}^{\mathbf{s}_{\text{r}}} \frac{\mathbf{z}^{2} \boldsymbol{\xi}}{\mu} \, d\mathbf{s}$$

where  $\xi$  is the eikonal function which has the property that the surface  $\xi=$  constant is the geometrical wave-front and gives the power loss in the far field due to refraction and inverse square spreading. These are field losses calculated in POWERL routine but integrated under control of the main program.

Polarization Term. - The expression  $R = E_{\overline{X}}/E_{\overline{Y}}$ , a complex number, is the polarization term.  $E_{\overline{X}}$  and  $E_{\overline{Y}}$  are the components of the electric vector of the wave along axes  $(\overline{x},\overline{y})$  in the wave front,  $\overline{y}$  being in and  $\overline{x}$  perpendicular to the plane containing the magnetic field of the Earth.

$$|R| = \text{modulus of } R = \frac{1}{Y_L} \left[ \frac{\frac{1}{4}Y_T^4 + A + Y_T^2 A^{1/2} \cos(\frac{\theta}{2})}{d} \right]^{1/2}$$

$$\Phi = \text{ argument of R} = \tan^{-1} \left\{ \frac{-\frac{1}{2} (1-X) Y_{T}^{2} + A^{1/2} \left[ \cos \frac{\theta}{2} (1-X) - Z \sin \frac{\theta}{2} \right]}{\frac{1}{2} Z Y_{T}^{2} + A^{1/2} \left[ \sin \frac{\theta}{2} (1-X) + Z \cos \frac{\theta}{2} \right]} \right\}$$

$$d = (1-X)^2 + Z^2$$

$$A = \left\{ \left[ \frac{1}{4} Y_{T}^{4} + Y_{L}^{2} d \right]^{2} + \left[ 2 Z Y_{L}^{2} (1-X) \right]^{2} \right\}^{1/2}$$

where

$$\theta = \tan^{-1} \left\{ \frac{-2(1-X)ZY_L^2}{\frac{1}{4}Y_T^4 + Y_L^2 d} \right\}$$

Evaluation of the polarization term is described under sub-routine POLAR.

Dictionary of Major FORTRAN Names. - Table VIII contains a dictionary of major FORTRAN names for the MAIN program.

TABLE VIII

FORTRAN NAME	DEFINITION
PRNTO	Value of PRINT trigger
PLOTT	Value of PLOT trigger
MORDGR	Order of differences carried in integration routine
MUFLAG	Pass indicator subroutine POWERL. Equals zero for the first pass and 1 for the rest of the run
DMDR	<u>9 m</u>
DMDT	<u>∂ M</u>
DMDP	<u>θ Μ</u>
DMDYl	$\frac{9 \text{ A}}{9 \text{ W}}$
DMDY2	$\frac{\partial M}{\partial Y_2}$
DMDY3	$\frac{9A}{9W}$
DMDF	$\frac{\partial M}{\partial F}$
DMUDR	<u>θμ</u>
DMUDT	<u>θμ</u> θθ
DMUDP	<u>θμ</u> θφ
DMUDY1	$\frac{\partial \mu}{\partial \mathbf{Y_1}}$
DMUDY2	<u>θν</u> θ <b>Υ</b> 2
DMUDY3	9 <b>Χ</b> 3

TABLE VIII. - Concluded

FORTRAN NAME	DEFINITION
DMUDF	<u>θμ</u> θ <b>f</b>
CAPPA	K, absorption coefficient
EPSTIN	Epstein condition
DMDSI	<u>9 Μ</u>
DMUDSI	<u>9ψ</u>
ΥD	Array of values of differ- ential equations
DENØM	A <sub>1</sub>
CØSPSI	cøs Y
RP	r' see near field power losses
PSI	γ' (
PRØPT	$\frac{P_{TO}}{P_{T}}$

## Subroutine POWERL

Description. - POWERL computes the power loss in the far field due to refraction and inverse square law spreading.

POWERL evaluates

$$\dot{\mathbf{P}}_{\mathbf{F}} = \frac{\sqrt{2}\xi}{\mu^2 \cos\alpha}$$

where  $\zeta$  is the eikonal function which has the property that the surface  $\zeta$  = constant is the geometrical wave front.

Derivation of 
$$\nabla^2_{\zeta}$$

$$\nabla \xi = \mathbf{n} \frac{d\mathbf{r}'}{d\mathbf{s}} = \mu \left( \frac{\partial \mathbf{r}'}{\partial \mathbf{s}} \ \hat{\mathbf{r}}' \right)$$

$$= \mu \left( \frac{\partial \mathbf{r}'}{\partial \mathbf{r}} \dot{\mathbf{r}} + \frac{\partial \mathbf{r}'}{\partial \theta} \dot{\theta} + \frac{\partial \mathbf{r}'}{\partial \phi} \dot{\phi} \right) \frac{\partial \mathbf{h}}{\partial \mathbf{s}} \hat{\mathbf{r}}' = \mu \dot{\mathbf{r}}' \hat{\mathbf{r}}'$$

where

$$\dot{\mathbf{r}}' = \frac{1}{\sqrt{\mu^2 + \left(\frac{\partial \mu}{\partial \psi}\right)^2}} \quad \left\{ \frac{\partial \mathbf{r}'}{\partial \mathbf{r}} \left( \mathbf{y}_1 - \mu \frac{\partial \mu}{\partial \mathbf{y}_1} \right) + \frac{\partial \mathbf{r}'}{\partial \theta} \frac{1}{\mathbf{r}} \left( \mathbf{y}_2 - \mu \frac{\partial \mu}{\partial \mathbf{y}_2} \right) \right\}$$

$$+ \frac{\partial \mathbf{r}}{\partial \phi} \frac{1}{\mathbf{r} \sin \theta} \left( \mathbf{y}_3 - \mu \frac{\partial \mu}{\partial \mathbf{y}_3} \right) \right\}$$

$$\nabla^2 \xi = \operatorname{div} \left( \mu \frac{\partial \bar{\mathbf{r}}}{\partial \mathbf{s}} \right) = \frac{1}{(r!)^2} \frac{\partial}{\partial \mathbf{r}} (\mu(\mathbf{r})^2 \dot{\mathbf{r}})$$

where

$$\frac{1}{(\mathbf{r}^{\,\prime})^2} \frac{\partial}{\partial \mathbf{r}^{\,\prime}} (\mu(\mathbf{r}^{\,\prime})^2 \dot{\mathbf{r}}^{\,\prime}) = \left(\frac{2\mu}{\mathbf{r}^{\,\prime}} + \frac{\partial\mu}{\partial \mathbf{r}^{\,\prime}}\right) \dot{\mathbf{r}}^{\,\prime} - \frac{\mu \dot{\mathbf{r}}^{\,\prime} \left(\mu \frac{\partial\mu}{\partial \mathbf{r}^{\,\prime}} + \frac{\partial\mu}{\partial \psi} \frac{\partial^2\mu}{\partial \mathbf{r}^{\,\prime} \partial \psi}\right)}{\left(\mu^2 + \left(\frac{\partial\mu}{\partial \psi}\right)^2\right)}$$

$$-\frac{\mu}{\left(\mu^2 + \left(\frac{\partial \mu}{\partial \psi}\right)^2\right)^{1/2}} \quad \left\{ \frac{\partial \mathbf{r}}{\partial \mathbf{r}} \left( \frac{\partial \mu}{\partial \mathbf{r}}, \frac{\partial \mu}{\partial \mathbf{y}} + \mu \frac{\partial^2 \mu}{\partial \mathbf{r} \partial \mathbf{y}_1} \right) \right.$$

$$+ \frac{1}{\mathbf{r}} \frac{\partial \mathbf{r}}{\partial \theta} \left[ \frac{1}{\mathbf{r}} \frac{\partial \mathbf{r}}{\partial \mathbf{r}} \left( \mathbf{y}_2 - \mu \frac{\partial \mu}{\partial \mathbf{y}_2} \right) + \left( \frac{\partial \mu}{\partial \mathbf{r}}, \frac{\partial \mu}{\partial \mathbf{y}_2} + \mu \frac{\partial^2 \mu}{\partial \mathbf{r} \partial \mathbf{y}_2} \right) \right]$$

$$+ \frac{1}{r \sin \theta} \frac{\partial r!}{\partial \phi} \left[ \left( \frac{1}{r} \frac{\partial r}{\partial r!} + \frac{\cos \theta}{\sin \theta} \frac{\partial \theta}{\partial r!} \right) \left( y_3 - \mu \frac{\partial \mu}{\partial y_3} \right) \right]$$

$$+ \frac{\partial \mu}{\partial \mathbf{r}'} \frac{\partial \mu}{\partial \mathbf{y}_3} + \mu \frac{\partial^2 \mu}{\partial \mathbf{r}' \partial \mathbf{y}_3}$$

The derivatives of r' with respect to r,  $\theta$ ,  $\phi$  are:

$$\frac{\partial \mathbf{r}'}{\partial \mathbf{r}} = \frac{1}{\mathbf{r}'} \left[ \mathbf{r} - \mathbf{r}_{0} \left( \sin\theta \sin\theta_{0} \cos(\phi - \phi_{0}) + \cos\theta \cos\theta_{0} \right) \right]$$

$$\frac{\partial \mathbf{r}'}{\partial \theta} = \frac{\mathbf{r}_{0}}{\mathbf{r}'} \left[ \cos \theta_{0} \sin \theta - \sin \theta_{0} \cos \theta \cos (\phi - \phi_{0}) \right]$$

$$\frac{\partial \mathbf{r}'}{\partial \phi} = \frac{\mathbf{r}'}{\mathbf{r}'} \sin\theta \sin\theta_0 \sin(\phi - \phi_0)$$

To find the derivatives of r,  $\theta$ ,  $\phi$  with respect to r', we differentiate the equations defining r',  $\theta$ ',  $\phi$ ' with respect to r'. In general, we have

$$\frac{1}{2} \frac{\partial}{\partial \mathbf{r}'} (\mathbf{r}')^2 = \mathbf{r} \frac{\partial \mathbf{r}}{\partial \mathbf{r}'} - \mathbf{r}_0 \frac{\partial \mathbf{r}}{\partial \mathbf{r}'} \left( \sin\theta \sin\theta_0 \cos(\phi - \phi_0) \right)$$

$$+\cos\theta\cos\theta_{o}$$
 -  $rr_{o}$   $(\cos\theta\sin\theta_{o}\cos(\phi-\phi_{o})\frac{\partial\theta}{\partial r})$ 

$$-\sin\theta\cos\theta_{0}\frac{\partial\theta}{\partial \mathbf{r}^{\dagger}}-\sin\theta\sin\theta_{0}\sin(\phi-\phi_{0})\frac{\partial\phi}{\partial \mathbf{r}^{\dagger}}$$

$$\frac{\partial}{\partial \mathbf{r}^{\dagger}} (\mathbf{r}^{\dagger} \cos \theta^{\dagger}) = \cos \theta \frac{\partial \mathbf{r}}{\partial \mathbf{r}^{\dagger}} - \mathbf{r} \sin \theta \frac{\partial \theta}{\partial \mathbf{r}^{\dagger}}$$

$$\frac{\partial}{\partial \mathbf{r'}} \left( \mathbf{r'} \sin \theta \cdot \cos \phi \cdot \right) = \sin \theta \cos \phi \cdot \frac{\partial \mathbf{r}}{\partial \mathbf{r'}} + \mathbf{r} \cos \theta \cdot \cos \phi \cdot \frac{\partial \theta}{\partial \mathbf{r'}}$$

$$-\mathbf{r} \sin\theta \sin\phi \frac{\partial\phi}{\partial\mathbf{r}}$$

We then solve these three simultaneous equations for

$$\frac{\partial \mathbf{r}}{\partial \mathbf{r}'}$$
 ,  $\frac{\partial \theta}{\partial \mathbf{r}'}$  , and  $\frac{\partial \phi}{\partial \mathbf{r}'}$ 

Now we must find the derivatives of  $\mu$  with respect to the r,  $\theta$ ,  $\phi$  system. The first derivatives of  $\mu$  are given in MAIN PROGRAM. It remains to find the second derivatives.

$$\begin{split} \frac{\partial^{2}\mu}{\partial\psi\partial\mathbf{r}} &= -\frac{1}{\mu} \frac{\partial\mu}{\partial\psi} \frac{\partial\mu}{\partial\mathbf{r}} - \frac{1}{\mathbf{A}} \frac{\partial\mu}{\partial\mathbf{r}} \frac{\partial\mathbf{A}}{\partial\psi} + \frac{\mathbf{N}}{2\mu\mathbf{C}_{1}}\mathbf{A}^{2} \left[ -\frac{\partial^{2}\mathbf{M}}{\partial\psi\partial\mathbf{r}} \right] \\ &- \frac{1}{\mathbf{B}} \frac{\partial\mathbf{B}}{\partial\psi} \frac{\partial\mathbf{B}}{\partial\mathbf{r}} + \frac{1}{\mathbf{B}} \left( \frac{\partial\mathbf{M}}{\partial\mathbf{r}} \frac{\partial\mathbf{M}}{\partial\psi} + \mathbf{M} \frac{\partial^{2}\mathbf{M}}{\partial\psi\partial\mathbf{r}} \right) \\ &- 2\frac{\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^{2}} \cos\psi \sin\psi \frac{\partial\mathbf{f}_{\mathbf{H}}}{\partial\mathbf{r}} - \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}^{2}} \sin\psi \frac{\partial\cos\psi}{\partial\mathbf{r}} \\ &+ \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}^{2}} \frac{\cos^{2}\psi}{\sin\psi} \frac{\partial\cos\psi}{\partial\mathbf{r}} \right] - \frac{\mathbf{N}}{2\mu\mathbf{C}_{1}}\mathbf{A}^{3} \frac{\partial\mathbf{A}}{\partial\mathbf{r}} \frac{\partial\mathbf{A}}{\partial\psi} \\ &- \frac{\partial\mathbf{A}}{\partial\psi\partial\theta} = -\frac{1}{\mu} \frac{\partial\mu}{\partial\psi} \frac{\partial\mu}{\partial\theta} - \frac{1}{\mathbf{A}} \frac{\partial\mu}{\partial\theta} \frac{\partial\mathbf{A}}{\partial\theta} + \frac{\mathbf{N}}{2\mu\mathbf{C}_{1}}\mathbf{A}^{2} \left[ -\frac{\partial^{2}\mathbf{M}}{\partial\psi\partial\theta} \right] \\ &- \frac{1}{\mathbf{B}} \frac{\partial\mathbf{B}}{\partial\theta} \frac{\partial\mathbf{B}}{\partial\psi} + \frac{1}{\mathbf{B}} \left( \frac{\partial\mathbf{M}}{\partial\psi} \frac{\partial\mathbf{M}}{\partial\theta} + \mathbf{M} \frac{\partial^{2}\mathbf{M}}{\partial\psi\partial\theta} \right) \\ &- 2\frac{\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^{2}} \cos\psi \sin\psi \frac{\partial\mathbf{f}_{\mathbf{H}}}{\partial\theta} - \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}^{2}} \sin\psi \frac{\partial\cos\psi}{\partial\theta} \\ &+ \frac{\mathbf{f}_{\mathbf{H}}^{2}}{\mathbf{f}^{2}} \frac{\cos^{2}\psi}{\sin\psi} \frac{\partial\cos\psi}{\partial\theta} \right] \\ &- \frac{\mathbf{N}}{2\mu\mathbf{C}_{1}}\mathbf{A}^{3} \frac{\partial\mathbf{A}}{\partial\theta} \frac{\partial\mathbf{A}}{\partial\psi} \frac{\partial\mathbf{A}}{\partial\theta} \end{aligned}$$

$$\begin{split} \frac{\partial^{2}\mu}{\partial\psi\partial\phi} &= -\frac{1}{\mu} \frac{\partial\mu}{\partial\psi} \frac{\partial\mu}{\partial\phi} - \frac{1}{A} \frac{\partial\mu}{\partial\phi} \frac{\partial A}{\partial\psi} + \frac{N}{2\mu C_{1}A^{2}} \left[ -\frac{\partial^{2}M}{\partial\psi\partial\phi} \right. \\ &- \frac{1}{B} \frac{\partial B}{\partial\phi} \frac{\partial B}{\partial\psi} + \frac{1}{B} \left( \frac{\partial M}{\partial\psi} \frac{\partial M}{\partial\phi} + M \frac{\partial^{2}M}{\partial\psi\partial\phi} \right. \\ &- 2 \frac{f}{H^{2}} \cos\psi \sin\psi \frac{\partial f}{\partial\phi} - \frac{f}{H^{2}} \sin\psi \frac{\partial\cos\psi}{\partial\phi} \\ &+ \frac{f^{2}_{H^{2}}}{f^{2}} \frac{\cos^{2}\psi}{\sin\psi} \frac{\partial\cos\psi}{\partial\phi} \right) \right] - \frac{N}{2\mu C_{1}A^{3}} \frac{\partial A}{\partial\phi} \frac{\partial A}{\partial\psi} \\ &+ \frac{\partial^{2}\mu}{f^{2}} \frac{\partial^{2}\mu}{\sin\psi} \frac{\partial^{2}\mu}{\partial\phi} \right) - \frac{N}{2\mu C_{1}A^{3}} \frac{\partial A}{\partial\phi} \frac{\partial A}{\partial\psi} \\ &+ \frac{\partial^{2}\mu}{f^{2}} \frac{\partial^{2}\mu}{\sin\psi} \frac{\partial^{2}\mu}{\partial\phi} \right) - \frac{N}{2\mu C_{1}A^{3}} \frac{\partial^{2}\mu}{\partial\phi} \frac{\partial^{2}\mu}{\partial\phi} \\ &- 2 \frac{\partial\mu}{\partial\phi} \frac{\partial\mu}{\partial\psi_{1}} \right] \\ &\frac{\partial^{2}\mu}{\partial\gamma_{2}\partial\theta} = \frac{1}{2\mu} \left[ \frac{1}{A^{2}C_{1}} \frac{\partial A}{\partial\gamma_{2}} \left( \frac{\partial N}{\partial\phi} - \frac{2N}{A} \frac{\partial A}{\partial\phi} \right) + \frac{N}{A^{2}C_{1}} \frac{\partial^{2}A}{\partial\gamma_{2}\partial\theta} \right. \\ &- 2 \frac{\partial\mu}{\partial\theta} \frac{\partial\mu}{\partial\psi_{2}} \right] \\ &\frac{\partial^{2}\mu}{\partial\gamma_{3}\partial\phi} = \frac{1}{2\mu} \left[ \frac{1}{A^{2}C_{1}} \frac{\partial A}{\partial\gamma_{3}} \left( \frac{\partial N}{\partial\phi} - \frac{2N}{A} \frac{\partial A}{\partial\phi} \right) + \frac{N}{A^{2}C_{1}} \frac{\partial^{2}A}{\partial\gamma_{3}\partial\phi} \right. \\ &- 2 \frac{\partial\mu}{\partial\phi} \frac{\partial\mu}{\partial\psi_{3}} \right] \end{split}$$

$$A = 1 - M + \frac{1}{4} M^2 + \frac{f_H^2}{f^2} \cos^2 \psi$$

$$B = \sqrt{M^2 + \frac{f_H^2}{f^2} \cos^2 \psi}$$

$$M = \frac{1}{2} \quad \frac{f_H^2}{f^2} \quad \frac{\sin^2 \psi}{C}$$

and

$$C = 1 - \frac{N}{C_1}$$

$$. \quad \frac{\partial^2 \mathbf{M}}{\partial \psi \partial \mathbf{r}} = \frac{1}{2\mathbf{f}^2} \quad \frac{1}{\left(1 - \frac{\mathbf{N}}{\mathbf{C}_1}\right)} \left\{ \begin{array}{l} 4 \, \mathbf{f}_{\mathbf{H}} \, \sin\!\psi \, \cos\!\psi \, \, \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \mathbf{r}} \, + \, 2 \, \, \mathbf{f}_{\mathbf{H}}^2 \, \cos\!\psi \, \, \frac{\partial \sin\!\psi}{\partial \mathbf{r}} \end{array} \right.$$

$$+ 2 f_{H}^{2} \sin \psi \frac{\partial \cos \psi}{\partial r} + \frac{2 f_{H}^{2} \sin \psi \cos \psi \frac{\partial N}{\partial r}}{\left(C_{1} \left[1 - \frac{N}{C_{1}}\right]\right)}$$

$$\frac{\partial^2 \mathbf{M}}{\partial \psi \partial \theta} = \frac{1}{2\mathbf{f}^2} \frac{1}{\left(1 - \frac{\mathbf{N}}{\mathbf{C}_1}\right)} \left\{ 4\mathbf{f}_{\mathbf{H}} \sin \psi \cos \psi \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \theta} + 2\mathbf{f}_{\mathbf{H}}^2 \cos \psi \frac{\partial \sin \psi}{\partial \theta} \right.$$

$$+ 2 f_{H}^{2} \sin \psi \frac{\partial \cos \psi}{\partial \theta} + \frac{2 f_{H}^{2} \sin \psi \cos \psi \frac{\partial N}{\partial \theta}}{\left(C_{1} \left[1 - \frac{N}{C_{1}}\right]\right)} \right\}$$

$$\begin{split} \frac{\partial^2 \mathbf{M}}{\partial \psi \partial \phi} &= \frac{1}{2\mathbf{f}^2} \left( 1 - \frac{\mathbf{N}}{\mathbf{C}_1} \right) \left\{ \begin{array}{l} 4 \, f_{\mathbf{H}} \sin \psi \cos \psi \, \frac{\partial \mathbf{f}}{\partial \phi} \, + \, 2 \, f_{\mathbf{H}}^2 \, \cos \psi \, \frac{\partial \sin \psi}{\partial \phi} \\ \\ &+ \, 2 \, f_{\mathbf{H}}^2 \, \sin \psi \, \frac{\partial \cos \psi}{\partial \phi} \, + \, \frac{2 \, f_{\mathbf{H}}^2 \, \sin \psi \, \cos \psi \, \frac{\partial \mathbf{N}}{\partial \phi}}{\left( \mathbf{C}_1 \left[ 1 - \frac{\mathbf{N}}{\mathbf{C}_1} \right] \right)} \right\} \\ \\ \frac{\partial^2 \mathbf{M}}{\partial \mathbf{r} \, \partial \mathbf{y}_1} &= \, \frac{1}{f^2 \mathbf{C}} \, \left\{ \, 2 \, f_{\mathbf{H}} \, \sin \psi \, \frac{\partial \sin \psi}{\partial \mathbf{y}_1} \, \, \frac{\partial \mathbf{f}}{\partial \mathbf{H}} \, + \, f_{\mathbf{H}}^2 \, \, \frac{\partial \sin \psi}{\partial \mathbf{r}} \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_1} \\ \\ &+ \, f_{\mathbf{H}}^2 \, \sin \psi \, \frac{\partial^2 \, \sin \psi}{\partial \mathbf{r} \, \partial \mathbf{y}_1} \, + \, \frac{f_{\mathbf{H}}^2}{\mathbf{C} \mathbf{C}_1} \, \sin \psi \, \frac{\partial \sin \psi}{\partial \mathbf{y}_1} \, \, \frac{\partial \mathbf{N}}{\partial \mathbf{r}} \right\} \\ \\ \frac{\partial^2 \mathbf{M}}{\partial \theta \, \partial \mathbf{y}_2} &= \, \frac{1}{f^2 \mathbf{C}} \, \left\{ \, 2 \, f_{\mathbf{H}} \, \sin \psi \, \frac{\partial \sin \psi}{\partial \mathbf{y}_2} \, \, \frac{\partial \mathbf{f}}{\partial \theta} \, + \, f_{\mathbf{H}}^2 \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_2} \, \, \frac{\partial \sin \psi}{\partial \theta} \, \right. \\ \\ &+ \, f_{\mathbf{H}}^2 \, \sin \psi \, \, \frac{\partial^2 \, \sin \psi}{\partial \theta \, \partial \mathbf{y}_2} \, + \, \frac{f_{\mathbf{H}}^2}{\mathbf{C} \mathbf{C}_1} \, \, \sin \psi \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_2} \, \, \frac{\partial \mathbf{N}}{\partial \theta} \, \right\} \\ \\ \frac{\partial^2 \mathbf{M}}{\partial \phi \, \partial \mathbf{y}_3} &= \, \frac{1}{f^2 \mathbf{C}} \, \left\{ \, 2 \, f_{\mathbf{H}} \, \sin \psi \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_3} \, \, \frac{\partial \mathbf{f}}{\partial \mathbf{H}} \, + \, f_{\mathbf{H}}^2 \, \, \frac{\partial \sin \psi}{\partial \phi} \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_3} \, \, \frac{\partial \sin \psi}{\partial \phi} \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_3} \, \, \frac{\partial \sin \psi}{\partial \phi} \, \, \frac{\partial \sin \psi}{\partial \mathbf{y}_3} \, \, \frac{\partial \sin \psi}{\partial \phi} \, \, \frac{\partial \sin \psi}{\partial \phi$$

$$\begin{split} \frac{\partial^2 \mathbf{A}}{\partial \mathbf{r} \partial \mathbf{y}_1} &= -\frac{\partial^2 \mathbf{M}}{\partial \mathbf{r} \partial \mathbf{y}_1} \quad \mp \quad \frac{1}{\mathbf{B}^3} \left( \ \mathbf{M} \ \frac{\partial \mathbf{M}}{\partial \mathbf{r}} + \frac{\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^2} \cos \psi \left[ \cos \psi \ \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \mathbf{r}} \right] \right. \\ &+ \left. \mathbf{f}_{\mathbf{H}} \ \frac{\partial \cos \psi}{\partial \mathbf{r}} \right] \right) \left( \mathbf{M} \ \frac{\partial \mathbf{M}}{\partial \mathbf{y}_1} + \frac{\mathbf{f}_{\mathbf{H}}^2}{\mathbf{f}^2} \cos \psi \ \frac{\partial \cos \psi}{\partial \mathbf{y}_1} \right) \\ & \quad \pm \quad \frac{1}{\mathbf{B}} \left\{ \frac{\partial \mathbf{M}}{\partial \mathbf{r}} \quad \frac{\partial \mathbf{M}}{\partial \mathbf{y}_1} + \mathbf{M} \ \frac{\partial^2 \mathbf{M}}{\partial \mathbf{r} \partial \mathbf{y}_1} + \frac{2\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^2} \cos \psi \ \frac{\partial \cos \psi}{\partial \mathbf{y}_1} \quad \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \mathbf{r}} \right. \\ &+ \left. \frac{\mathbf{f}_{\mathbf{H}}^2}{\mathbf{f}^2} \left( \frac{\partial \cos \psi}{\partial \mathbf{r}} \quad \frac{\partial \cos \psi}{\partial \mathbf{y}_1} + \cos \psi \ \frac{\partial^2 \cos \psi}{\partial \mathbf{r} \partial \mathbf{y}_1} \right) \right\} \\ & \quad \frac{\partial^2 \mathbf{A}}{\partial \theta \partial \mathbf{y}_2} = - \frac{\partial^2 \mathbf{M}}{\partial \theta \partial \mathbf{y}_2} \quad \mp \quad \frac{1}{\mathbf{B}^3} \left( \mathbf{M} \ \frac{\partial \mathbf{M}}{\partial \theta} + \frac{\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^2} \cos \psi \left[ \cos \psi \ \frac{\partial \mathbf{f}_{\mathbf{H}}}{\partial \theta} \right. \right. \\ &+ \left. \mathbf{f}_{\mathbf{H}} \ \frac{\partial \cos \psi}{\partial \theta} \right] \right) \left( \mathbf{M} \ \frac{\partial \mathbf{M}}{\partial \mathbf{y}_2} + \frac{\mathbf{f}_{\mathbf{H}}^2}{\mathbf{f}^2} \cos \psi \ \frac{\partial \cos \psi}{\partial \mathbf{y}_2} \right) \\ & \quad \pm \quad \frac{1}{\mathbf{B}} \left\{ \frac{\partial \mathbf{M}}{\partial \theta} \quad \frac{\partial \mathbf{M}}{\partial \mathbf{y}_2} + \mathbf{M} \ \frac{\partial^2 \mathbf{M}}{\partial \theta \partial \mathbf{y}_2} + \frac{2\mathbf{f}_{\mathbf{H}}}{\mathbf{f}^2} \cos \psi \ \frac{\partial \cos \psi}{\partial \mathbf{y}_2} \right. \\ &+ \left. \frac{\mathbf{f}_{\mathbf{H}}^2}}{\mathbf{f}^2} \left( \frac{\partial \cos \psi}{\partial \theta} \quad \frac{\partial \cos \psi}{\partial \mathbf{y}_2} + \cos \psi \ \frac{\partial^2 \cos \psi}{\partial \theta \partial \mathbf{y}_2} \right) \right\} \end{aligned}$$

$$\begin{split} \frac{\partial^{2} A}{\partial \phi \partial y_{3}} &= -\frac{\partial^{2} M}{\partial \phi \partial y_{3}} \stackrel{-}{+} \frac{1}{B^{3}} \left( M \frac{\partial M}{\partial \phi} + \frac{f_{H}}{f^{2}} \cos \psi \left[ \cos \psi \frac{\partial f_{H}}{\partial \phi} \right] \right) \\ &+ f_{H} \frac{\partial \cos \psi}{\partial \phi} \right] \right) \left( M \frac{\partial M}{\partial y_{3}} + \frac{f_{H}^{2}}{f^{2}} \cos \psi \frac{\partial \cos \psi}{\partial y_{3}} \right) \\ & \stackrel{+}{+} \frac{1}{B} \left\{ \frac{\partial M}{\partial \phi} \frac{\partial M}{\partial y_{3}} + M \frac{\partial^{2} M}{\partial \phi \partial y_{3}} + \frac{2f_{H}}{f^{2}} \cos \psi \frac{\partial \cos \psi}{\partial y_{3}} \right. \\ &+ \frac{f_{H}^{2}}{f^{2}} \left( \frac{\partial \cos \psi}{\partial \phi} \frac{\partial \cos \psi}{\partial y_{3}} + \cos \psi \frac{\partial^{2} \cos \psi}{\partial \phi \partial y_{3}} \right) \right\} \end{split}$$

The derivatives of  $\,f_H^{},\,\cos\,\psi^{},\,$  and sin  $\psi^{}$  depend on the particular magnetic field model used.

The power loss as computed above (and ray-tracing in general) is valid only when the following conditions are fulfilled:

$$\frac{1}{k\mu}$$
  $\frac{\nabla \mu}{\mu}$  << 1 where  $k = \frac{2\pi}{\lambda}$ 

and

$$\frac{1}{k\mu}$$
  $\frac{\nabla PL}{PL}$  << 1

These conditions are violated in rapidly varying media or when a caustic is encountered. Figure 10 is a flow chart of the subroutine POWERL.

Dictionary of major FORTRAN names.-Table IX contains a dictionary of major FORTRAN names, subroutine POWERL.

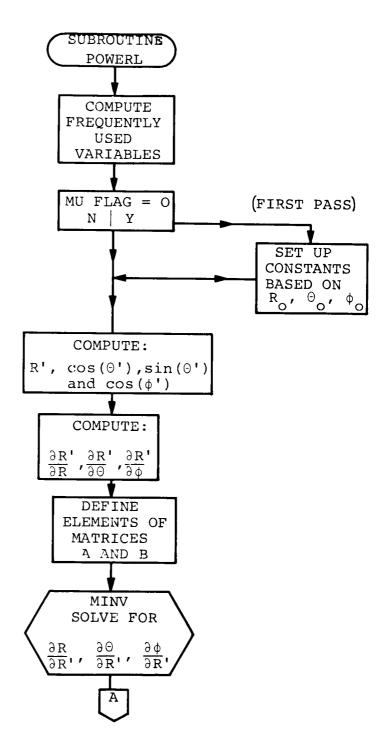


Figure 10A. - Flow Chart of Subroutine POWERL

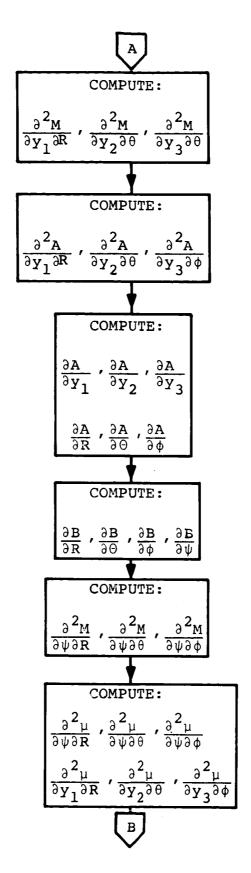


Figure 10B. - Flow Chart of Subroutine POWERL

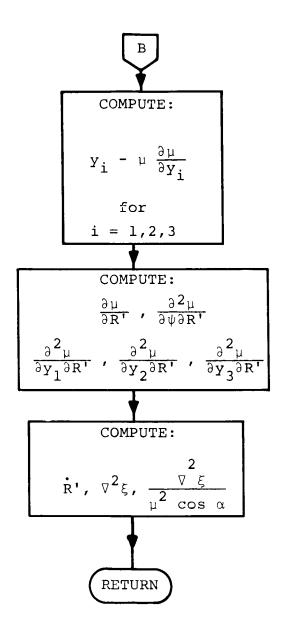


Figure 10C. - Flow Chart of Subroutine POWERL

TABLE IX

FORTRAN Name	Definition
DRPDR	∂r' ∂r
DRPDT	$\frac{\partial \mathbf{r}}{\partial \theta}$
DRPDP	∂r' ∂ø
DSITP	cos(φ')
COTP	cos(θ ')
COPP	$\sin( heta)$
DRDRP	∂r ∂r'
DTDRP	$\frac{\partial \theta}{\partial \mathbf{r}}$
DPDRP	$\frac{\partial \phi}{\partial \mathbf{r}}$
D2MY1R	$\frac{\partial^2 \mathbf{M}}{\partial \mathbf{y_1} \partial \mathbf{r}}$ $\frac{\partial^2 \mathbf{M}}{\partial \mathbf{y_2} \partial \theta}$
D2MY2T	$\frac{\partial^2 \mathbf{M}}{\partial \mathbf{y_2} \partial \theta}$
D2MY3P	$rac{\partial^2 \mathbf{M}}{\partial \mathbf{y_3} \partial \boldsymbol{\phi}}$

TABLE IX.- Continued

FORTRAN Name	Definition
D2AY1R	$\frac{\partial^2 \mathbf{A}}{\partial \mathbf{y_1} \partial \mathbf{r}}$
D2AY2T	$\frac{\partial^2 \mathbf{A}}{\partial \mathbf{y_2} \partial \theta}$
D2AY3P	$\frac{\partial^2 \mathbf{A}}{\partial \mathbf{y_3} \partial \phi}$
DADY1	$\frac{\partial \mathbf{A}}{\partial \mathbf{y}_{1}}$
DADY2	$\frac{\partial \mathbf{A}}{\partial \mathbf{y}_2}$
DADY3	$\frac{\partial A}{\partial y_3}$
DADR	$\frac{\partial \mathbf{A}}{\partial \mathbf{r}}$
DADT	$\frac{\partial \mathbf{A}}{\partial \theta}$
DADP	$rac{\partial \mathbf{A}}{\partial \phi}$
DBDR	$\frac{\partial \mathbf{B}}{\partial \mathbf{r}}$
DBDT	$\frac{\partial \mathbf{B}}{\partial \theta}$
DBDP	<u>θΒ</u> θφ

TABLE IX. - Continued

FORTRAN Name	Definition
DBDSI	$rac{\partial \mathbf{B}}{\partial \psi}$
D2MDSR	<u>∂<sup>2</sup>Μ</u> ∂ψ∂ <b>R</b>
D2MDST	<u>∂<sup>2</sup>Μ</u> ∂ψ∂θ
D2MDSP	$rac{\partial^2 \mathbf{M}}{\partial \psi \partial \phi}$
D2UDSR	$rac{\partial^2 \mu}{\partial \psi \partial \mathbf{r}}$
D2UDST	$\frac{\partial^2 \mu}{\partial \psi  \partial  \theta}$
D2UDSP	$rac{\partial^2 \mu}{\partial \psi \partial \phi}$
D2UY1R	$\frac{\partial^2 \mu}{\partial \mathbf{Y_1} \partial \mathbf{r}}$
D2UY2T	$rac{\partial^2 \mu}{\partial \mathbf{Y_2} \partial  heta}$
D2UY3P	$\frac{\partial^{2} \mu}{\partial Y_{3} \partial \phi}$ $Y_{1} - \mu \frac{\partial \mu}{\partial Y_{1}}$
YPEMDU	$Y_1 - \mu \frac{\partial \mu}{\partial Y_1}$

TABLE IX. - Concluded

FORTRAN Name	Definition
YP2MDU	$Y_2 - \mu \frac{\partial \mu}{\partial Y_2}$
YP3MDU	$\mathbf{Y}_{3} - \mu \frac{\partial \mu}{\partial \mathbf{Y}_{3}}$
DMUDRP	$\frac{\partial \mu}{\partial \mathbf{r}}$
DUDSRP	$\frac{\partial^2 \mu}{\partial \psi \partial \mathbf{r}}$ '
DUY1RP	$rac{\partial^2 \mu}{\partial { m Y}_1 \partial { m r}}$ '
DUY2RP	$rac{\partial^2 \mu}{\partial { m Y_2} \partial { m r}}$
DUY3RP	$rac{\partial^2 \mu}{\partial { m Y_3} \partial { m r}}$
RDØTP	rٔ۰
DEL2S	$\sqrt{2} \xi$
YD(11)	$\dot{P}_{F} = \frac{\nabla^{2} \xi}{\mu^{2} \cos \alpha}$

Subroutine INPUT

Description. The purpose of the INPUT routine is to bring into core the user's data and then convert it into a useable format. (See flow chart in Figure 11.) Most of the initialization

is performed here. Since all the information referring to the input section is already presented in Section II, it is sufficient to present only the flow chart and the listing of the subroutine.

Dictionary of major FORTRAN names. - Table X contains a dictionary of major FORTRAN names.

TABLE X

TABLE A		
FORTRAN Name	Data Type	Definition
V	Numeric array	Coefficients used to calculate $N_{\mathbf{x}}^{(r)}$
W	Numeric array	Coefficients used to calculate $N_{\mathbf{x}}^{(\mathbf{r})}$
D	Numeric array	Dummy input array
XNAME1	Name list	Description in Section II
XNAME3	Name list	Description in Section II
XNAME5	Name list	Description in Section II
Н		Scale size of electron density distribution
HPRIME		Point of maximum electron den- sity gradient
ZX		$\frac{r}{r}$ (r - r )
ENF		N <sub>F</sub> Electron density in F region
ENXR		N <sub>x</sub> (r)
ENX		N Electron density in exo- sphere
EN		Total electron density, $N_{x} + N_{F} = N$

TABLE X.- Concluded

FORTRAN Name	Data Type	Definitions
PKDELN		$\Delta N_0 = PKFRAC * N(PKFRAC is in percent)$
PLT		Array used to store plotting title information
YO	Array	Contains value of differen- tial equations evaluated
NUAR		Number of differential equa- tions evaluated

## Subroutine Output

 $\underline{\text{Description.}}\text{--}$  Final calculations are made in OUTPUT prior to printing results.

(1) DOPPLER SHIFT - DSHIFT

$$\Delta f = -(2.424067E-4).f \int_{0}^{h} p \frac{1}{\mu} \frac{\partial \mu}{\partial \phi} dh_{p}$$

(2) VALIDITY CRITERION - VALCRIT

$$\mathbf{v_c} = \mathbf{K} \left[ \left( \frac{\partial \mu}{\partial \mathbf{r}} \right)^2 + \frac{1}{\mathbf{r}^2} \left( \frac{\partial \mu}{\partial \theta} \right)^2 + \frac{1}{(\mathbf{rcos}\theta)^2} \left( \frac{\partial \mu}{\partial \phi} \right)^2 \right]^{1/2}$$

where

$$K = \frac{1}{K_1 f \mu^2 \cdot 10^6}$$

$$K_1 = \frac{2\pi}{c} = 2.0943933E-5$$

c = speed of light in km

f = signal frequency in megacycles/sec.

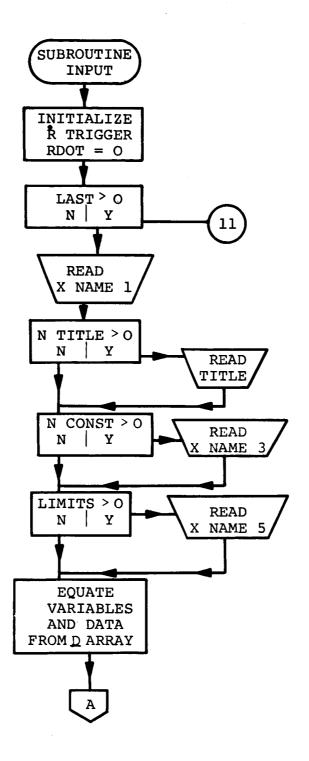


Figure 11A. - Flow Chart of Subroutine INPUT

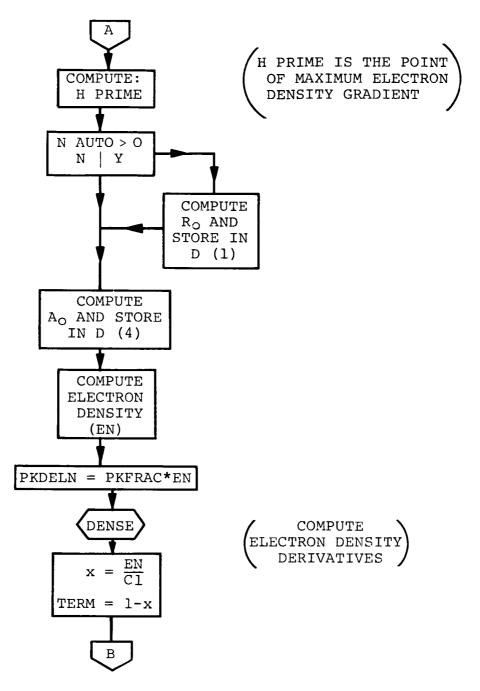


Figure 11B. - Flow Chart of Subroutine INPUT

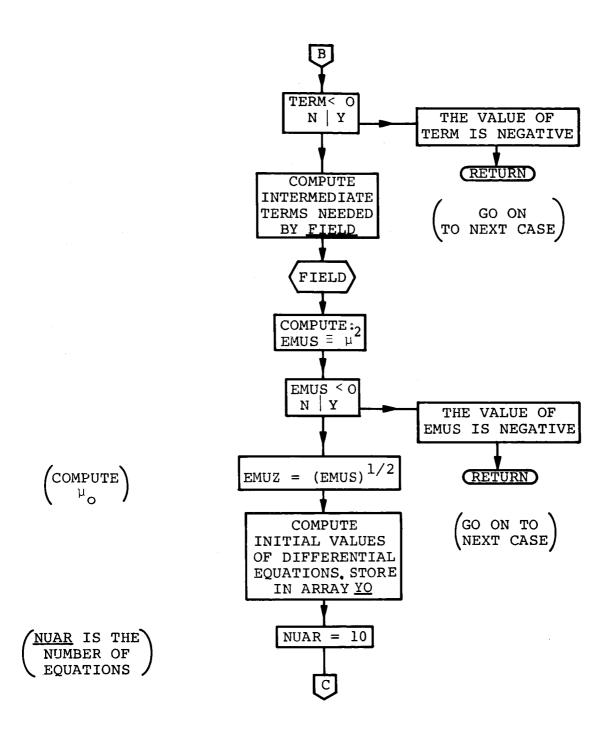


Figure 11C. - Flow Chart of Subroutine INPUT

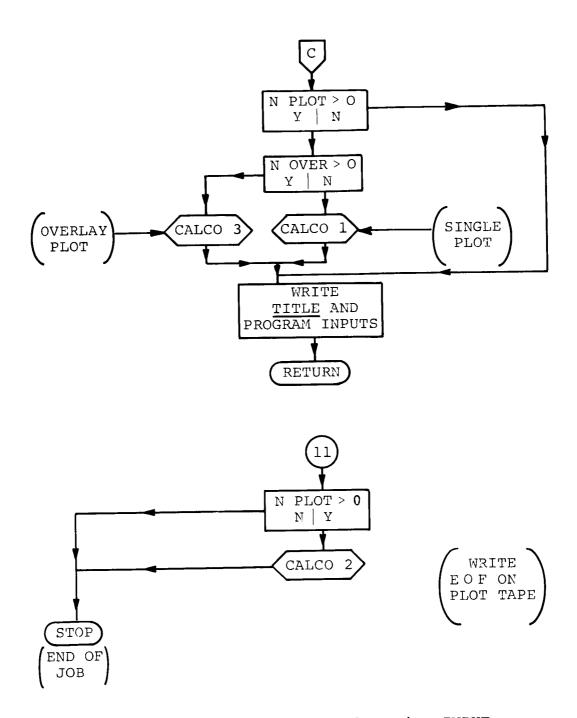


Figure 11D. - Flow Chart of Subroutine INPUT

In the flow chart convention:

$$DM\mu DR = \frac{\partial \mu}{\partial r}$$

$$VØ(1) = r$$

$$DMUDT = \frac{\partial \mu}{\partial \theta}$$

$$RCT = rcos\theta$$

$$DMUDP = \frac{\partial \mu}{\partial \phi}$$

$$EMUS = \mu^{2}$$

(3) TOTAL POWER LOSS IN DB - PL -

$$P_{L} = 10 \log_{10} \left( \mu \ PR \phi PT \ EXP \left[ - \int_{0}^{h} \frac{\sqrt{2} \xi}{\mu^{2} \cos \alpha} \ dh_{p} \right] \right)$$

where

$$YD(11) = \dot{P}_{F} = \frac{\sqrt{2} \zeta}{\mu^{2} \cos \alpha}$$

$$YØ(11) = \int_{0}^{h_{p}} \dot{P}_{F} dh_{p}$$

$$PRØPT = \frac{P_{ro}}{P_{T}} \times \frac{c^{2}}{4\pi f^{2} \mu_{o}} \times 10^{12}$$

(4) GROUP DELAY IN MILLISECONDS - GRODEL

GRØDEL = 
$$\frac{1}{c}$$
 
$$\int_{0}^{h} \left(1 + \frac{f \times 1.0E6}{\mu} \frac{\partial \mu}{\partial f}\right) dh_{p}$$

where f is the frequency in MHz and  $dh_p = \mu \cos \alpha ds$ .

In the flow chart convention:

$$YD(7) = G_L = 1 + \frac{f \bullet 1.0E6}{\mu} \frac{\partial \mu}{\partial f}$$

$$Y\emptyset(7) = \int_{0}^{h_{p}} \dot{G}_{L} dh_{p} = G_{L}$$

$$GRØDEL = \frac{G_L}{c}$$

where

 $G_{L}$  = group path length in km c = speed of light in km/sec = 3 x 10<sup>2</sup>

Also, see the flow chart, Figure 12.

Dictionary of major FORTRAN names. - Table XI contains a dictionary of major FORTRAN names, subroutine OUTPUT.

TABLE XI

FORTRAN Name	Data Type	Definition
THETA		Colatitude of wave front in degrees
PHI		Longitude of wave front in degrees
YØSQR		$[Y\emptyset(4)]^2 + [Y\emptyset(5)]^2 + [Y\emptyset(6)]^2$
DSHIFT		Doppler shift, $\Delta f$ .
C2		4.24737E-6/F, used to calcu- late dispersion

TABLE XI.- Concluded

FORTRAN Name	Data Type	Definition
VALCRIT		Validity criterion for $\mu^2$
PL		Total power loss in db, exclusive of absorption
GRØDEL		Group delay in milliseconds
XX	Array	Array used to store geocen- tric radius for plot of total ray path
YY	Array	Array used to store colati- tude for plot of total ray path, theta in degrees
LL		Number of points in the XX and YY arrays 500 points maximum
JFLAG		Program indicator, used to indicate reason OUTPUT was called
JUMP		Program indicator, used to indicate that an end of case condition exists
N		Program indicator, used as a line counter

## Subroutine COLL

Description.- The collision frequency model has the following
functional form:

$$v = 10^{v'}$$

where  $\nu^{\prime}$  is computed as shown below. (Also, see flow chart, Figure 13.) The collision frequency profile as a function of

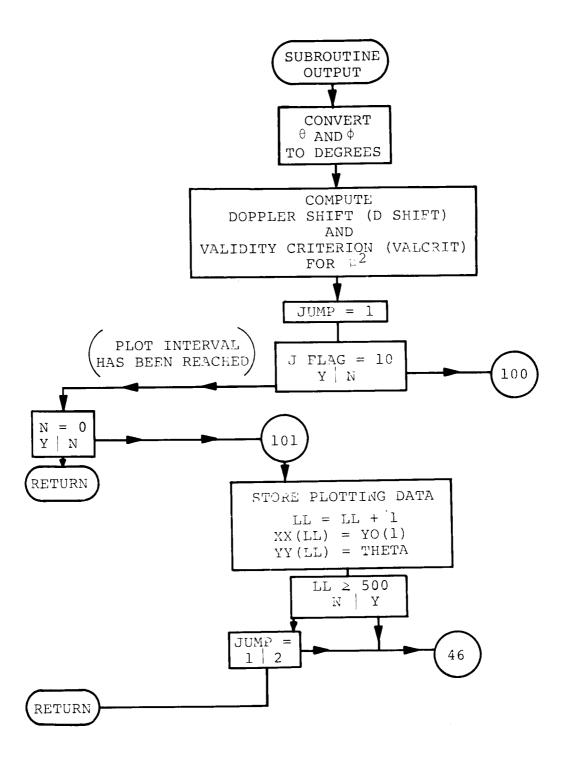


Figure 12A. - Flow Chart of Subroutine OUTPUT

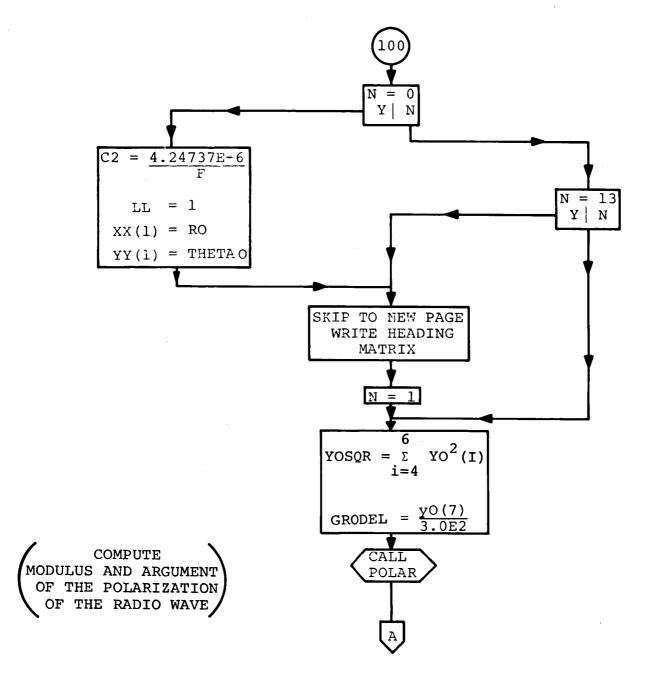


Figure 12B. - Flow Chart of Subroutine OUTPUT

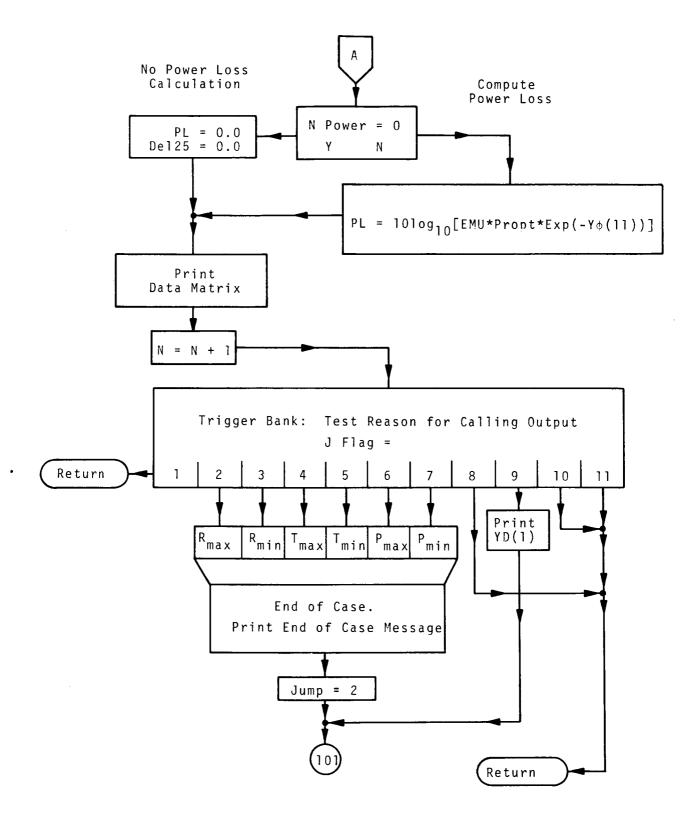
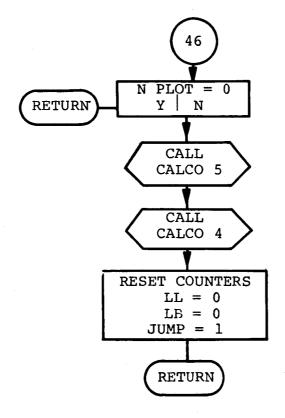


Figure 12C. - Flow Chart of Subroutine OUTPUT



TO GENERATE RECTANGULAR PLOT CALL CALCO 5
TO GENERATE POLAR PLOT CALL CALCO 4

BOTH PLOTS ARE DESCRIBED IN THE FOLLOWING SECTION

Figure 12D. - Flow Chart of Subroutine OUTPUT

altitude consists of three parts that are smoothly joined with the aid of a curve fitting program.

For  $6378 \le r \le 6478$  km:

$$v' = 12.03527 - 0.07392 x$$

where

$$x = (r - 6378) \text{ km}.$$

For  $6478 \le r \le 6853$  km:

$$\nu = \sum_{i=1}^{6} \left[ a_i + C(\theta, \phi) b_i \right] f_i(x)$$

where

$$f_1(x) = 1$$
 ;  $x = (r-6478)$ km  
 $f_2(x) = x$   
 $f_3(x) = x^2$   
 $f_4(x) = x^3$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_6(x) = \sin(0.0157 x)$   
 $f_1(x) = \sin(0.0157 x)$   
 $f_2(x) = \sin(0.0157 x)$   
 $f_3(x) = \cos(0.0157 x)$   
 $f_4(x) = \sin(0.0157 x)$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_1(x) = x^2$   
 $f_2(x) = x$   
 $f_3(x) = x^2$   
 $f_4(x) = x^3$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_1(x) = x^2$   
 $f_2(x) = x$   
 $f_3(x) = x^2$   
 $f_4(x) = x^3$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_1(x) = x^2$   
 $f_2(x) = x^2$   
 $f_3(x) = x^2$   
 $f_4(x) = x^3$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_5(x) = \cos(0.0157 x)$   
 $f_6(x) = \sin(0.0157 x)$   
 $f_1(x) = 0.032512$   
 $f_2(x) = 0.032512$   
 $f_3(x) = 0.032512$   
 $f_3(x) = 0.032512$   
 $f_4(x) = 0.032512$   
 $f_5(x) = 0.032512$   
 $f_5(x) = 0.032512$   
 $f_7(x) = 0.032512$   

$$c(\theta, \phi) = c_1^2 + c_2^2 + c_3^2 + (d_1^2 + d_2^2 + d_3^2) \cos \phi$$

where

$$c_1 = -0.35818$$
 ;  $d_1 = -0.17828$ 

$$c_2 = 1.1250$$
 ;  $d_2 = 0.55997$ 

$$c_3 = -0.88344$$
 ;  $d_3 = 0.56028$ 

 $\theta$  is the colatitude and  $\varphi$  is the longitude in degrees.  $\varphi$  = 0 corresponds to local noon. For r  $\geqslant$  6853 km,

$$\nu = 2.3653 - 0.0030266 \text{ x} \bullet (0.3195 - 0.0000536 \text{ x}) c(\theta, \phi)$$

where

$$x = (r - 6853)$$

Also, see flow chart of subroutine COLL, Figure 13.

## Subroutine FIELD

Description. An idealized dipole model is used for the magnetic field of the Earth. The magnetic field equations which define gyrofrequency,  $f_H$ , and the angle between the magnetic field and the wave normal,  $\psi$ , are

$$f_{H} = c_{11} \left(\frac{a}{r}\right)^{3} \left[1 + 3\cos\theta\right]^{1/2}$$

where a = 6378 km, the radius of the Earth and r and  $\theta$  are the geocentric radius and colatitude of the ray position

$$c_{11} = \frac{e}{2\pi m} B_0 \bullet 10^{-6} \doteq 0.9$$

where  $B_0$  = 0.3142 Gauss is the magnetic field on the surface of the Earth at the equator and e and m are the charge and mass of an electron.

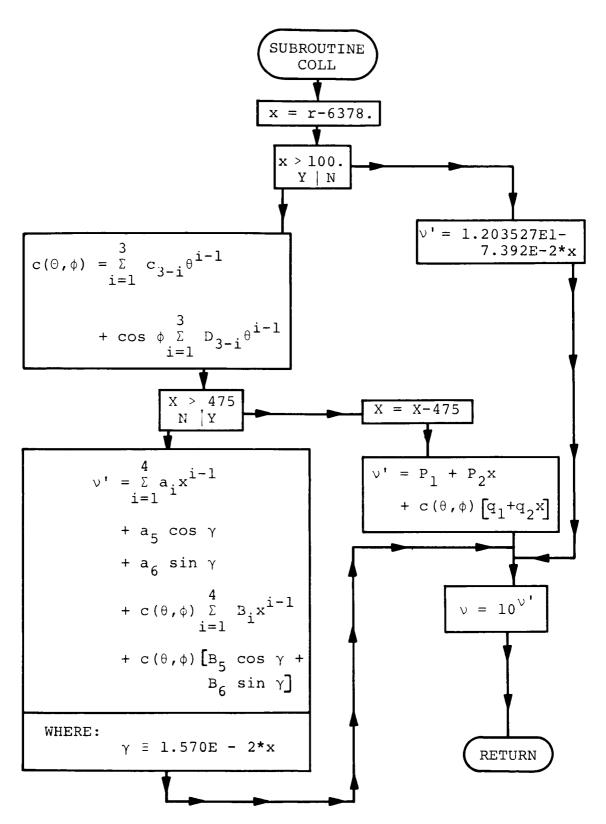


Figure 13. - Flow Chart of Subroutine COLL

$$\cos \psi = \frac{\cos\theta + Y_2 \sin\theta}{\sum_{i=1}^{3} Y_L^2 \cdot \left[1 + 3\cos\theta\right]^{1/2}}$$

$$\sin \psi = \frac{2Y_2 \cos\theta - Y_1 \sin\theta}{|2Y_2 \cos\theta - Y_1 \sin\theta|} \left[1 - \cos^2 \psi\right]^{1/2}$$

The derivatives of  $f_H$  and  $\psi$  are:

$$\frac{d(f_{H})}{dr} = -2.7 \left(\frac{a^3}{r^4}\right) \left[1 + \cos^2\theta\right]^{1/2}$$

$$\frac{d(f_{H})}{d\theta} = -2.7 \left(\frac{a^{3}}{r^{3}}\right) \frac{\sin\theta \cos\theta}{\left[1 + 3\cos^{2}\theta\right]^{1/2}}$$

$$\frac{d(f_{H})}{d\phi} = 0$$

Let

$$T_1 = \sum_{L=1}^3 Y_L^2$$

$$T_2 = Y_1 \cos\theta + \frac{1}{2} Y_2 \sin\theta$$

$$T_3 = \cos^2\theta + \frac{1}{4} \sin^2\theta$$

$$T_4 = -Y_1 \sin\theta + \frac{1}{2} Y_2 \cos\theta$$

Then

$$\frac{d(\cos\psi)}{dr} = 0$$

$$\frac{d(\cos \psi)}{d\theta} = \frac{T_4 + \frac{3}{4} \left[ \frac{T_2 \sin \theta \cos \theta}{T_3} \right]}{(T_1)^{1/2} \bullet (T_3)^{1/2}}$$

$$\frac{\mathrm{d}(\cos\psi)}{\mathrm{d}\;\phi} = 0$$

$$\frac{d(\cos \psi)}{dY_1} = \frac{\cos \theta - \left[\frac{Y_1 \cdot T_2}{T_1}\right]}{(T_1)^{1/2} (T_3)^{1/2}}$$

$$\frac{\frac{d(\cos \psi)}{dY_2} = \frac{\frac{1}{2}\sin \theta - \left[\frac{Y_2 \cdot T_2}{T_1}\right]}{(T_1)^{1/2} (T_3)^{1/2}}$$

$$\frac{d(\cos\psi)}{dY_3} = \frac{-Y_3\cos\psi}{T_1}$$

$$\frac{d^{2}(\cos\psi)}{dY_{2}d\theta} = -\frac{d(\cos\psi)}{d\theta} \frac{Y_{2}}{T_{1}} + \frac{4\cos\theta}{(T_{1})^{1/2}(T_{3})^{1/2}[1 + 3\cos^{2}\theta]^{2}}$$

$$\frac{d^{2}(\sin\psi)}{dY_{2}d\theta} = -\frac{1}{\sin\psi} \left[ \cos\psi \frac{d^{2}(\cos\psi)}{dY_{2}d\theta} + \frac{d(\cos\psi)}{d\theta} \frac{d(\cos\psi)}{dY_{2}} \cdot \frac{1}{\sin^{2}\psi} \right]$$

Also, see flow chart, Figure 14.

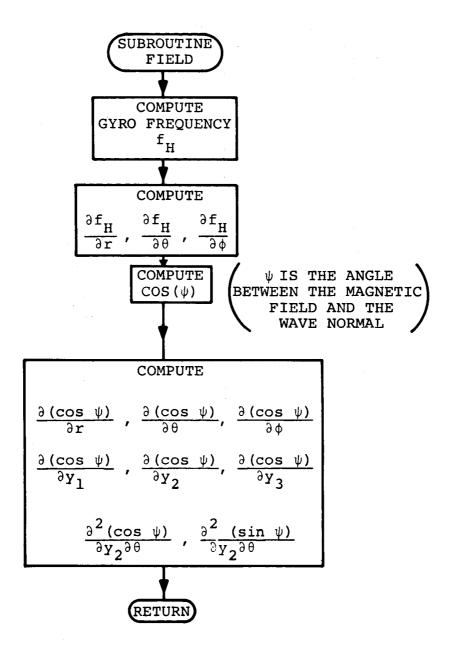


Figure 14. - Flow Chart of Subroutine FIELD

Dictionary of major FORTRAN names. - Table XII contains a dictionary of major FORTRAN names, subroutine FIELD.

TABLE XII

FORTRAN Name	Definition	
FH	f <sub>H</sub> , gyrofrequency in MHz	
DFHDR	$\frac{d(f_H)}{dr}$	
DFHDQ	$\frac{\mathrm{d}(\mathrm{f}_{\mathrm{H}})}{\mathrm{d} heta}$	
DFHDP	$rac{d(\mathrm{f}_{\mathrm{H}})}{d\phi}$	
COSPSI	$\mathbf{cos}(\psi)$	
SP2	$1 - \cos^2(\psi)$	
DCPDR	$\frac{\mathbf{d}(\mathbf{cos}\psi)}{\mathbf{dr}} = 0$	
DCPDT	d(cosψ) dθ	
DCPDP	$rac{\mathrm{d}(\mathbf{cos}\psi)}{\mathrm{d}\phi} \ = \ 0$	
DCPDY1	$rac{ ext{d}( ext{cos}\psi)}{ ext{dY}_1}$	

TABLE XII. - Concluded

FORTRAN Name	Definition
DCPDY2	$rac{ ext{d}(\cos\psi)}{ ext{dY}_2}$
DCPDY3	<u>d(cosψ)</u> dY <sub>3</sub>
D2CY2T	$\frac{\mathrm{d}(\mathtt{cos}\psi)}{\mathrm{d}(\mathrm{Y}_2)\mathrm{d}(\theta)}$
D2SY2T	$rac{ ext{d}( ext{sin}\psi)}{ ext{dY}_2 ext{d} heta}$

Subroutine DENSE

Description .- The electron density is given by

$$N(\mathbf{r},\theta,\phi)=N_1(\mathbf{r},\theta)\bullet N_2(\mathbf{r},\theta,\phi)$$

where r is the geocentric radius,  $\theta$  is the colatitude, and  $\varphi$  is the magnetic longitude.

 $N_1(r,\theta)$  represents the background density in the magnetic meridional plane and  $N_2(r,\theta,\phi)$  represents the ionization of the field-aligned irregularities in both the meridional and azimuthal planes.

The background ionization is assumed to have the form:

$$N_1(r,\theta) = N_F + N_X$$

where

 $N_F$  = electron density in the F-region

 $N_{_{\mathbf{X}}}$  = electron density in the exosphere

$$N_F = N_{max} * EXP[1/2 \{ 1-W-e^{-W} \}]$$

 $N_{\text{max}}$  is assumed to be 2.7E5

$$W = \frac{h - h_{max}}{H_F}$$

 $h_{max}$  = altitude of the peak electron density  $N_{max}$ 

 $H_{F} =$ the scale height

 $h_{max} = 350 \text{ km}$ 

 $H_F = 50 \text{ km}$ 

The electron density in the exosphere is given by:

$$N_{x} = N_{r} \times [1.659E3 \bullet \theta + 1.662E4]$$

where  $\theta$  is the colatitude in radians.

$$N_{r} = \left[\sum_{i=1}^{3} \beta_{i} \exp\left(-\frac{Z_{x}}{H_{i}}\right)\right]^{1/2}$$

where  $Z_{x}$  is the geopotential altitude given by:

$$Z_{x} = \frac{r_{o}}{r} (r-r_{o})$$

where  $r_0$  is the reference radial distance and is equal to 6878 in the model.

The symbol i refers to each ion present in the exosphere. H<sub>i</sub> and  $\beta_i$  refer to the scale height and the fractional density of the i-th ion at the reference level  $r_0$ .

A three-ion gas model consisting of oxygen  $(0^+)$ , helium  $(\mathrm{He}^+)$ , and hydrogen  $(\mathrm{H}^+)$  ions is assumed. The various parameters in the density equation have the following values:

ion <sub>i</sub>	$^{eta}$ i	$^{ ext{H}}$ i
0+	.9788	66.546
H+	.0016	1056.3
He <sup>+</sup>	.0196	265.98

The technique suggested by Swayze is used to join the exospheric profile smoothly with that of the F-layer between 350 and 1000 km. The expression  $\rm N_{\rm X}$  is modulated by a factor

$$EXP \left[ -\left(\frac{h-1000}{500}\right)^2 \right]$$

where h is the altitude in km.

The model for the field aligned ionization irregularities is given by:

$$N_{2}(\mathbf{r},\theta) = 1 + \frac{\Delta N_{0}}{\left(N \cdot \frac{t}{t_{0}}\right)} \cdot \text{EXP} \left[ -\left(\frac{\Delta z}{H_{0}\left(\frac{t}{t_{0}}\right)}\right)^{2} \right]$$

 $\rm N_{\rm O}$  is the peak ionization enhancement and  $\rm H_{\rm O}$  is the scale size of the irregularity at the base of the field line

$$\frac{t}{t_o} = \frac{\text{meridional width at } (r, \theta)}{\text{meridional width at } (r_o, \theta_o)}$$
$$= \frac{\sin^3 \theta (4 - 3\sin^2 \theta_o)^{1/2}}{\sin^3 \theta_o (4 - 3\sin^2 \theta)^{1/2}}$$

$$N_{F} = N_{max} \bullet exp \left[ \frac{1}{2} \left( 1 - W - e^{-W} \right) \right]$$

$$\frac{dN_F}{dr} = N_F \bullet \left(-\frac{1}{2H_F}\right) \left(1 - e^{-W}\right)$$

Since  $H_F = 50 \text{ km}$ 

$$\frac{dN_F}{dr} = N_F \times 10^{-2} (e^{-W}-1)$$

$$\frac{dN_F}{d\theta} = 0$$

$$N_X = N_F [K_1\theta + K_2]$$

where  $\kappa_1$  and  $\kappa_2$  are constants and  $\theta$  is the colatitude.

$$N_{r} = \left[\sum_{i=1}^{3} \beta_{i} \exp\left(-\frac{Z_{x}}{H_{i}}\right)\right]^{1/2}$$

where

$$Z_{x} = \frac{r_{o}}{r} (r-r_{o})$$

$$\frac{dN_{x}}{dr} = -\frac{(K_{1}\theta + K_{2})}{2N_{r}} \left[ \sum_{i=1}^{3} \frac{\beta_{i}}{H_{i}} \exp\left(-\frac{Z_{x}}{H_{i}}\right) \right] \frac{dZ_{x}}{dr}.$$

But,

$$\frac{dZ}{dr} = \frac{r^2}{\frac{o}{2}}$$

$$\frac{dN_{x}}{dr} = -\frac{(K_{1}\theta + K_{2})}{2N_{r}} \cdot \frac{r_{o}^{2}}{r} \begin{vmatrix} 3 & \beta_{i} \\ \sum_{i=1}^{3} & \frac{\beta_{i}}{H_{i}} & \exp\left(-\frac{Z_{x}}{H_{i}}\right) \end{vmatrix}$$

$$\frac{dN}{d\theta} = K_1 N_r.$$

If  $N_{\mathbf{x}}$  is modulated by the factor

$$\mathbf{F_r} = \exp \left[ - \left( \frac{\mathbf{r} - 7378}{500} \right)^2 \right]$$

for r < 7378 km.

$$\frac{dN_{x}'}{dr} = \frac{d(N_{x} \cdot F_{r})}{dr} = \frac{dN_{x}}{dr} \bullet F_{r} + N_{x} \frac{dF_{r}}{dr} .$$

$$\frac{\mathrm{dF}_{\mathbf{r}}}{\mathrm{dr}} = F_{\mathbf{r}} \bullet \left(\frac{7378 - \mathbf{r}}{125000}\right)$$

Similarly,

$$\frac{dN_{x}'}{d\theta} = \frac{d(N_{x} \cdot F_{r})}{d\theta} = F_{r} \cdot \frac{dN_{x}}{d\theta}$$
$$= K_{1}N_{r} \cdot F_{r}$$

DIS refers to the normal distance of the ray-position  $(r, \theta, \phi)$  from a field-line of colatitude  $\lambda$ .

DIS = 
$$\mathbf{r} \cdot \frac{\left(1 - \frac{\mathbf{a}}{\mathbf{r}} \frac{\sin^2 \theta}{2}\right)}{\left(1 + \frac{4}{\tan^2 \theta_1}\right)}$$

where

$$\theta_1 = \theta + \left\{ 1 - \frac{\mathbf{a}}{\mathbf{r}} \bullet \frac{\sin^2 \theta}{\sin^2 \lambda} \quad \frac{\frac{2}{\tan \theta}}{\left(1 + \frac{4}{\tan^2 \theta}\right)} \right\}$$

SOA refers to the geometrical path length in Earth radii of any arbitrary ray-position  $(r,\theta)$  from its initial position  $(r_0,\theta_0)$  along the same magnetic field line of the colatitude  $\lambda$ .

$$SOA = \frac{\sqrt{3}}{\sin^{2} \lambda} \begin{bmatrix} \left(\frac{4}{3} - \sin^{2} \theta\right)^{1/2} \cos \theta - \left(\frac{4}{3} - \sin^{2} \theta_{o}\right)^{1/2} \cos \theta_{o} \\ + \frac{1}{3} \log \left[\frac{\left(\frac{4}{3} - \sin^{2} \theta\right)^{1/2} + \cos \theta}{\left(\frac{4}{3} - \sin^{2} \theta_{o}\right)^{1/2} + \cos \theta_{o}} \right]$$

Also, see flow chart, Figure 15.

Dictionary of major FORTRAN names. - Table XIII contains a dictionary of major FORTRAN names, subroutine DENSE.

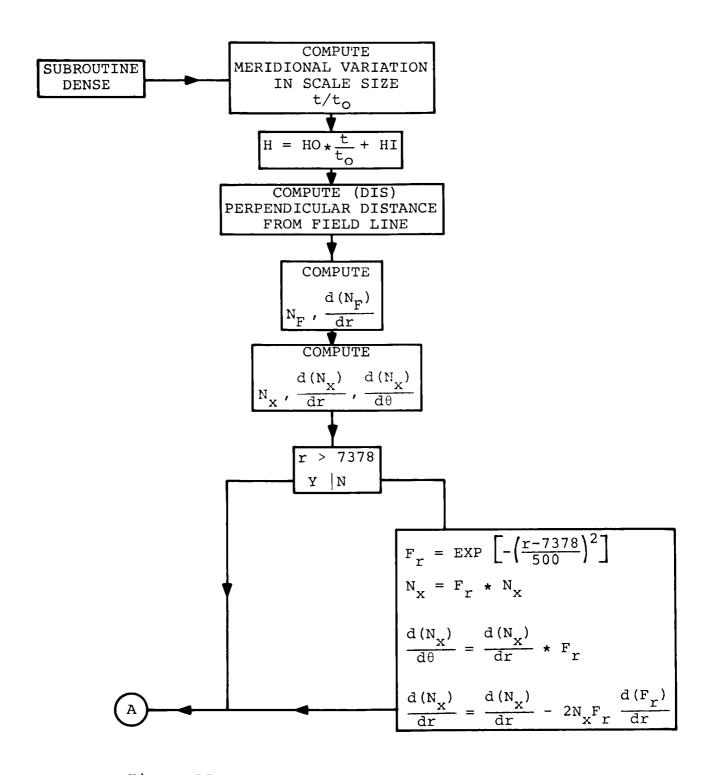


Figure 15A. - Flow Chart of Subroutine DENSE

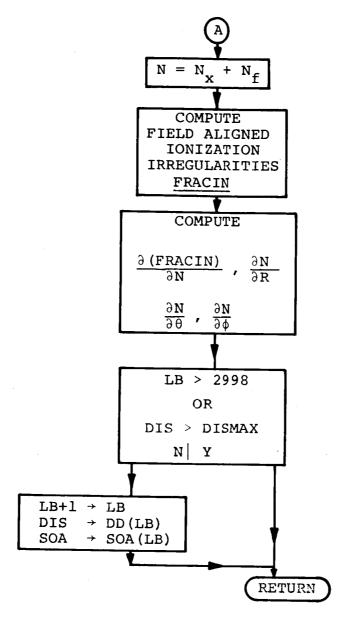


Figure 15B. - Flow Chart of Subroutine DENSE

TABLE XIII

FORTRAN Name	Data Type	Definition
ENF		N <sub>F</sub> - Electron density in the F-region
ENX		N <sub>X</sub> - Electron density in the exosphere
ZX		$\frac{r_0}{r}$ (r - $r_0$ ) - geopotential altitude
ENXR		$\Sigma \beta_{i} \bullet EXP \left(-\frac{Z_{x}}{H_{i}}\right)$
DZXDR		$\frac{d(Z_{X})}{dr}$
DENFDR		$\frac{d(N_{\overline{F}})}{dr}$
DENXDR		$\frac{d(N_{\chi})}{dr}$
DENXDT		$\frac{\mathrm{d(N_x)}}{\mathrm{d}\theta}$
R	r	Geocenter radius of wave front, in km
тн	θ	Colatitude of wave front, in radians
AMBDA	λ	Colatitude of point where the field line intersects the Earth's surface, in radians

TABLE XIII. - Concluded

FORTRAN Name	Data Type	Definition
ZM5	t <sub>o</sub>	$ \begin{array}{c} \text{meridional width} \\ \underline{\text{at } (r,\theta)} \\ \text{meridional width} \\ \text{at } (r_0,\theta_0) \end{array} \right) \begin{array}{c} \text{modula-} \\ \text{tion factor} \\ \text{if variable} \\ \text{width duct} \\ \text{is considered} \end{array} $
Н	t <sub>o</sub> H <sub>o</sub>	Scale size of the field line at $(r,\theta,\phi)$
DIS		Distance perpendicular from $(r,\theta,\phi)$ to field line
DD		Plotting array used to store distance from field line, DIS
SØA		Plotting array used to store distance along field line

## Subroutine CALCØ5

Description. - This subroutine does the plotting for the ray tracing program. All plotting operations are performed by this routine.

Two types of plot are generated by this program. The first is a rectangular plot of distance from the field line vs. distance along the field line from near end. The polar plot shows the total ray path with respect to the Earth. All distances are in kilometers.

Multiple entry points allow the user to obtain either one or both of the plots. The user also has the option of overlaying successive plots.

This subroutine has entry points CALCO4 and CALCO5 in subroutine OUTPUT. CALCO1, CALCO2 and CALCO3 are called by INPUT.

This subroutine in turn calls subroutine AXIS, SYMBOL, NUM-BER, LINE and PLOT. These are standard calcomp plotting subroutines and are described in Bulletin #170-C, Programming for Calcomp Digital Incremental Plotters, by California Computer Products, Inc.

The subroutine PRAM calculates the adjusted minimum and delta required by the line and axis subroutines.

## Restrictions of CALCO4

Titling - Because only one set of axes is drawn, when using the overlay option, titling information for the overlayed plots is not printed. The user should know beforehand the content of the plot.

Also, see flow chart, Figure 16.

Dictionary of major FORTRAN Names. - Table XIV contains a table of major FORTRAN names, subroutine CALCO5.

TABLE XIV

FORTRAN Name	Data Type	Definition
PLDAT	Numeric array	Working storage for plot subroutine
Х	Numeric array	X coordinates to be plotted
Y	Numeric array	Y coordinates to be plotted
LL	Scalar	Number of points in X and Y arrays
DATE	Alphanumeric array	20 characters reserved for data
PLT	Numeric array	Numeric values of labling information
XMAXO XMINO	Scalar	Maximum and minimum values of the X-axis for the rectangular plot of the distance from the field line vs. the distance along the field line
YMAXO YMINO	Scalar	Maximum and minimum values of the Y-axis for the rectangular plot of the distance from the field line vs. the distance along the field line
xmax1 xmin1	Scalar	Maximum and minimum values of the X-axis for the polar plot of ray path
YMAX1 )	Scalar	Maximum and minimum values of the Y-axis for the polar plot of ray path

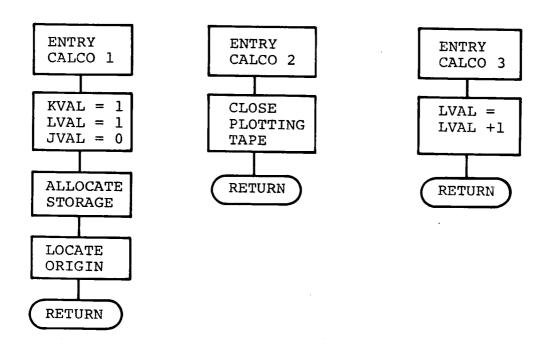


Figure 16A. - Flow Chart of Subroutine CALCO

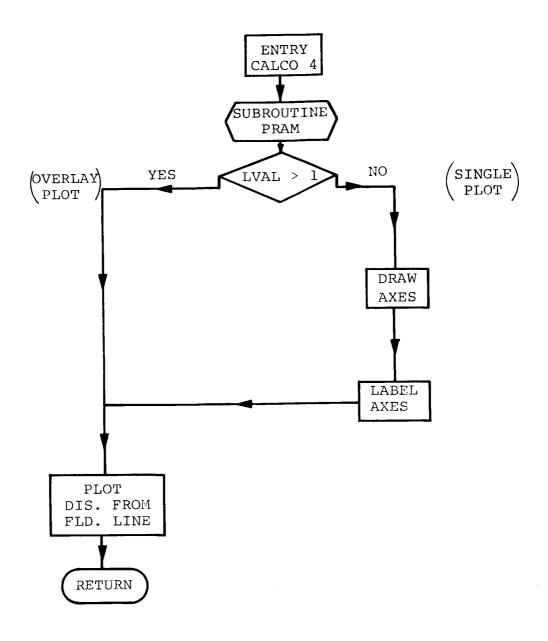


Figure 16B. - Flow Chart of Subroutine CALCO

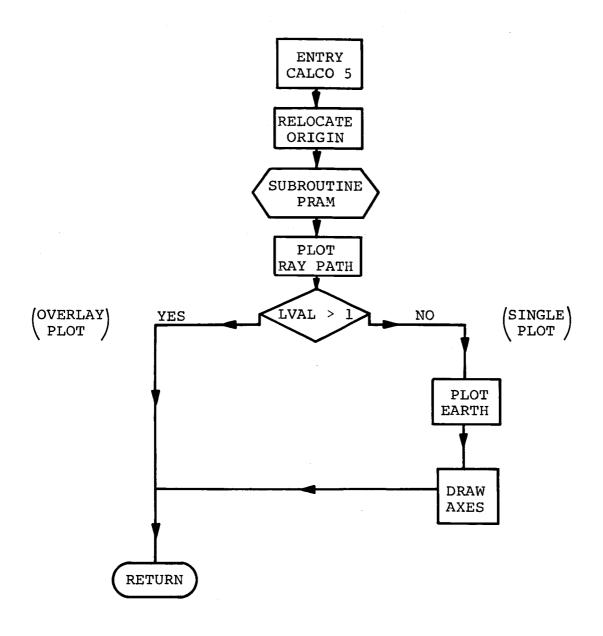


Figure 16C. - Flow Chart of Subroutine CALCO

#### Subroutine FORCE

Description. - Subroutine FORCE solves the equation.

$$Y_1^2 + Y_2^2 + Y_3^2 = \mu^2$$
.

In theory this relationship holds all along the ray path but in fact it does not. We make it hold by scaling  $y_1$ ,  $y_2$  and  $y_3$  down proportionately. This process is called "Normalization" of the Y vector. FORCE is called by MAIN only.

Also see flow chart, Figure 17.

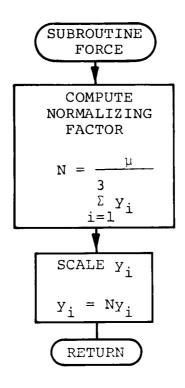


Figure 17. - Flow Chart of Subroutine FORCE

## Subroutine POLAR

<u>Description</u>. The expression  $R = E_{\overline{X}}/E_{\overline{Y}}$ , a complex number, is the polarization term.  $E_{\overline{x}}$  and  $E_{\overline{y}}$  are the components of the electric vector of the wave along axes (x,y) in the wave front, y being in and x perpendicular to the plane containing the magnetic field of the Earth.

$$|R| = \text{modulus of } R = \frac{1}{Y_L} \left[ \frac{\frac{1}{4} Y_T^4 + A + Y_T^2 A^{1/2} \cos \frac{\theta}{2}}{d} \right]^{1/2}$$

$$\Phi = \text{ argument of R} = \tan^{-1} \frac{-\frac{1}{2}(1-X)Y_{T}^{2} \pm A^{1/2} \left(\cos \frac{\theta}{2}(1-X) - Z \sin \frac{\theta}{2}\right)}{\frac{1}{2}ZY_{T}^{2} \pm A^{1/2} \left(\sin \frac{\theta}{2}(1-X) + Z \cos \frac{\theta}{2}\right)}$$

$$d = (1-X)^{2} + Z^{2}$$

$$A = \left\{ \left[ \frac{1}{4} Y_{T}^{4} + Y_{L}^{2} d \right]^{2} + \left[ 2ZY_{L}^{2} (1-X) \right]^{2} \right\}^{1/2}$$

where

$$\theta = \tan^{-1} \left\{ \frac{-2(1-X) Z Y_L^2}{\frac{1}{4} Y_T^4 + Y_L^2 d} \right\}$$

Also, see flow chart, Figure 18.

#### Mathematical Subroutines

CST1 and TOR. - CST1 evaluates the sine and cosine integrals  $S_i(x)$  and  $C_i(x)$ . It is called only in MAIN and in turn calls TOR. TOR evaluates n: and is called only by CST1.

Minv.- MINV solves three sets of three simultaneous equations using a Gaussian method with pivot selection. It is called by POWERL and calls no other subroutine.

SMARK and MARK. - Subroutines SMARK and MARK constitute the integration package. MARK is a MAP language subroutine originally written by the Jet Propulsion Laboratory. The purpose of SMARK is to allow an interface with the main program written in FORTRAN IV.

Listings of the five mathematical subroutines are appended in Appendix B. A complete description of the integration package is found in Appendix A.

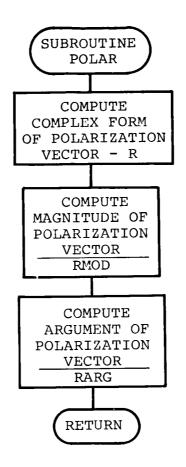


Figure 18. - Flow Chart of Subroutine POLAR

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#### APPENDIX A

## DESCRIPTION OF THE INTEGRATION PACKAGE

#### Introduction

The integration package is composed of two subroutines, SMARK and MARK, both written in the MAP assembly language. Subroutine SMARK serves as a connecting link between the FORTRAN IV monitor and subroutine MARK. Subroutine MARK as originally written was designed to operate in a non-FORTRAN environment. The integration of the differential equations is performed by MARK.

## Subroutine SMARK

This subroutine is buffer between MARK, a differential equation solving routine written in MAP language, and a main program written in FORTRAN. SMARK allows a program written in FORTRAN IV to use most of the features of MARK.

Usage of SMARK. - A knowledge of MARK is assumed.

Calling sequences:

CALL SMARK, KIND, N. HBANK, NRTN, NTRG

EUBAR, ELBAR, HMAXT, HMINT, YCLOW

LV1, TV1,

LV2, TV2,

LV3, TV3, etc.,

. . . . up to 10 triggers

where

KIND = type of integration

0 = fixed AM integration

2 = RK integration

4 = Variable Adams-Moulton integration

N = actual number of differential equations

NRTN = return indicator from SMARK

1 = EOS

2 = DER1

3 = DER2

4 = trigger return

5 = error return

NTRG = return indicator from SMARK which designates which trigger has been activated. 1 for first trigger, 2 for second, etc.

EUBAR, ELBAR, HMAXT, HMINT, YCLOW same as in MARK

LV1 = location of variable being tested

TV1 = location of desired value of the variable tested

CALL TRA14 returns control to SMARK and causes a TRA 1,4 return to MARK.

CALL TRA24 returns control to SMARK and causes a TRA 2,4 return to MARK.

CALL ON (N) turns trigger N on.

CALL OFF (N) turns trigger N off.

The order of the differences to be carried in the Adams-Moulton integration must be stored in HBAND(1), the nominal step size in HBAND(4), the maximum number of equations allowable in HBANK(5), and all independent and dependent variables initialized before calling SMARK. The double precision part of the independent variable HBANK(7) is set to zero by SMARK.

#### Subroutine MARK

MARK is a closed subroutine designed to solve the first n of a set, N, of first-order differential equations utilizing Adams-Moulton open or open and closed formula types. A Runge-Kutta fourth-order integrator is used as a starting routine to generate backward differences initially. Provision is made for interrupting the integration process at specific values of either the independent or the dependent variables. The order of differences (m) used in the Adams-Moulton mode is less than or equal to nine (9) (m  $\leqslant$  9).

Restrictions. - The following restrictions to subroutine MARK apply:

- (1) MARK will not integrate backwards in the independent variable. The nominal step size, H, must be positive. Changes in H must be accomplished by the use of a "doubling" or "halving" procedure in MARK that will double (set H = 2H) or halve (set H = 0.5H) the integration step size.
- (2) Underflow and overflow are not checked internally.
- (3) The user must provide the necessary interruption subroutines, an auxiliary program to evaluate the n first-order derivatives, and a bank of storage for internal calculation.
- (4) This is an FAP program and is not FORTRAN compatible.

Integration technique.- The following integration technique
applies:

- (1) MARK permits the user to solve the N differential equations by one of three options:
  - a. Runge-Kutta fourth order.
  - b. Adams-Moulton with a fixed step size, H, and the ability to alter H by the doubling and/or halving procedure using Runge-Kutta to initially generate backward differences. This applies to either a predictor or a predictor with q corrections (open or open and closed type formulas).
  - c. Adams-Moulton as mentioned in b. using an automatic variable step size control. Halving and doubling are controlled automatically. The correction formula is applied only once.
- (2) Both the independent and the dependent variables are automatically carried internally in partial double precision to control round-off error locally. The user, however, will recognize the variables only as single precision quantities. However, the user may carry the independent variable in full double precision by option.

<u>Usage of MARK.-</u> The following usage of MARK applies: Calling Sequence:

CALL MARK or TSX \$MARK,4

PZE HBANK, P, EOS

PZE DERI, ¢, DER2

ERROR RETURN

Pfx Bl,,Yl

PZE Z1

Pfx B2,, Y2

PZE Z2

•

Pfx BJ,,YJ

PZE ZJ

PZE O

where the symbols are defined as follows:

- HBANK The location of a bank of storage to be described below.
  - O The independent variable is carried in partial precision.
  - P double precision (single precision to the user).
  - 1 The independent variable is carried in full double precision.
  - EOS The location of a user "end of step" routine. This routine must terminate with a TRA 1,4 command. It is used to evaluate variables that are needed only after a full integration step is completed.

- DER1 The location of the entry to the user's derivative routine that carries out all calculations that involve the independent variable. This routine must terminate with a TRA 1,4 command.
- DER2 The location of the entry to that portion of the user's derivative routine that carries out all calculations that do not involve the independent variable but are required to evaluate the derivatives.

A simple example of the use of DER1, DER2 follows:

Suppose we are to solve

$$\frac{dy}{dx} = ax^2 + by$$

then

Thus, the DERl entry calculates the extra term involving the independent variable x. This provides a saving of real machine time, particularly during the Runge-Kutta phase of integration, and also saves machine time when the closed type formula is used with Adams-Moulton integration.

- 0 Adams-Moulton integration with fixed step size
- $\phi$  = 2 Runge-Kutta integration only
  - 4 Adams-Moulton using automatic variable step size control

The pairs of locations in the calling sequence are specified as:

Pfx BJ,,YJ

PZE ZJ

are defined as "triggers"

These triggers are the linkage control to the user's interruption subroutines. The triggers state that control is transferred to location BJ when the contents of location YJ are equal to
the contents of location ZJ. Thus BJ is the location of a user's
interruption subroutine, YJ is the location of a variable being
checked, and ZJ is the location that contains the desired value
for YJ.

Triggers are separated into two classes: Independent variable triggers called T-stops and dependent variable triggers called Y-stops.

(1) Independent variable triggers called T-stops. These triggers interrupt on values of the independent variable of integration. All T-stops must have YJ = 0. That is, they must have the following format in the calling sequence:

Pfx BJ

PZE ZJ

The logic used to execute T-stops is as follows:

Let  $t_{s1}$ ,  $t_{s2}$ ,  $t_{s3}$ .... $t_{sk}$  be a set of values of the independent variable for which interruptions are desired.

MARK sets  $t_m = Min \ [t_{s1}, \ t_{s2}, \ldots, t_{sk}]$ . Integration continues normally until the independent variable reaches the condition:

$$t_n < t_m \le t_n + 1$$

The step size is set =  $(t_{\eta + 1} - t_m)$  and integration is carried to  $t_m$  where all the values of the variables including derivatives and end of step values are calculated and control is then transferred to the user's interruption routine, all values are reset to station  $t_{\eta - 1}$  and the next  $t_m$  is determined. If no other  $t_m$  exists within this step, integration continues. Thus, interruption routines for all  $t_m$  within a given step are executed before integration continues. There is no limitation on the number of T-stops permitted (except for machine size, of course).

(2) Dependent variable triggers called Y-stops. These triggers are interrogated at the beginning of an integration step and a value.

$$i_j = y_n = y_j$$

is calculated and saved for each of the j Y-stops. At the end of the integration step the difference,

$$r_j = y_{\eta + 1} - y_j$$

is calculated and the algebraic sign of  $r_{j}$  is compared to  $l_{j}$ :

Ιf

$$sgn l_j \neq sgn r_j$$

then the condition  $y=y_j$  has occurred within the integration step and a linear interpolation search procedure is executed to determine the value of the independent variable, t, such that  $y=y_j$ . When the  $\Delta t$  calculated by the search procedure is such that

$$\Delta t < \delta_u$$

where

$$\delta_{u} = \begin{cases} 2^{-26} \text{ Max } H, t & \text{for } P = 0 \\ 2^{-42} \text{ Max } H, t & \text{for } P = 1 \end{cases}$$

then convergence to  $t_{\rm j}$  is assured. At this point all values of the dependent variable including their respective derivatives and any end-of-step calculations are determined and control for the corresponding Y-stop is returned to the user's interruption routine. If more than one Y-stop trigger occurs within an integration step, then the triggers are executed in the order of the smallest value of the independent variable determined for the respective Y-stops. Thus, the order of execution is determined by the independent variable. After all Y-stops within an integration step have been determined and executed, the conditions at station  $t_{\eta}+1$  are restored for all dependent variables and their derivatives and end-of-step calculations, if any. Integration then continues normally.

Up to and including 50 dependent variable triggers are permitted. However, this number may be altered by changing the symbolic card "OMAR EQU 50" in the symbolic program deck to the desired number.

It remains to define Pfx of the trigger pair. This is utilized to permit the user to render triggers "active" or "inactive". Active means that a trigger is to be interrogated and executed if necessary. Inactive means that the trigger is to be ignored.

Thus, if

The interruption routines provided by the user must terminate with either a TRA 1,4 command or a TRA 2,4 command.

TRA 1,4 is used when the interruption does not constitute a discontinuity in any of the calculations.

TRA 2,4 is used when a discontinuity exists. Under this condition a "restart" procedure is initiated by MARK by continuing beyond the discontinuity point using Runge-Kutte until a sufficient number of backward differences are determined to switch to Adams-Moulton integration.

Comments on triggers. - The following are comments on triggers:

- (1) There is no limitation on how many times a trigger may be executed.
- (2) Care must be exercised in updating the ZJ of triggers. If the ZJ are not updated after a trigger returns control to the user, a machine loop will result, since MARK will continue to return control to the user, a machine loop will result, since MARK will continue to return control to the user's respective interrupt routine on the basis of the current ZJ. Thus, a trigger must either be updated or rendered inactive to looping.
- (3) In all cases where more than one trigger is to be executed ted at a single point (t<sub>j</sub>) the triggers will be executed in order of their ascending appearance in calling sequence
- (4) Control is returned to the error return of the calling sequence whenever  $t_m < (t_\eta \delta_u)$  or when the number of Y-steps exceeds 50.

The entire list of triggers must be terminated with PZE 0. This is the end of the calling sequence for MARK.

The bank of storage specified by the location HBANK is as follows:

PZE m

PZE NH

PZE ND

#### **HBANK**

DEC H

PZE N,,n

DEC t<sub>1</sub>

DEC to

```
DEC y<sub>1</sub>
DEC y<sub>2</sub>
DEC y<sub>n</sub>
\mathtt{DEC} \ \mathtt{y}_{N}
DEC y1
DEC y2
DEC yn
DEC y_N
                 3N + 2N(m + 1) for \phi 0, 2
BSS
                  5N + 3N(m + 2) for \phi 4
```

where

m = order of differences to be carried in the Adams-Moulton mode.  $m \leqslant 9$  (fixed point in the address portion of the word) for  $\phi = 0$ .

 $m \leq 8 \text{ for } \varphi = 4.$ 

NH = number of times to sequentially halve the step size in the Adams-Moulton mode (fixed point in the address portion of the word).

#### NOTE

NH takes precedence over ND and doubling is not executed until the number of times to halve is completed. If these numbers are introduced initially in the HBANK, the procedure is commenced automatically when conversion from Runge-Kutta to Adams-Moulton is completed. NH and ND are ignored when using the automatic variable step size mode. NH and ND may be set by dependent variable or independent variable interruption routines in the Adams-Moulton fixed mode. Control is returned to the user anytime through an interruption The number of times halving routine. and/or doubling have/has been completed is available in the decrement portion of NH and/or ND. If additional halving and/or doubling requests are entered in the address portions of NH and/or ND before a preceding request is completed, the sum of the additional request and those remaining uncompleted will be executed.

- H = nominal step size (floating point).
- N =total number of 1st order differential equations (fixed point).
- n = total number of the first n lst order differential equations to be integrated by MARK.  $n \le N$  (fixed point).

#### NOTE

H and N must not be altered unless a restart procedure is executed after

the inital entry to MARK. Item n may be altered after the inital entry to MARK through an interruption routine. If n is increased, MARK restarts. Care should be exercised in setting the initial conditions corresponding to the additional equations to be integrated. If n is decreased, MARK continues normally integrating the new n set of differential equations.

- t<sub>1</sub> = single precision value of the independent variable
   in floating point.
- double precision value of the independent variable  $t_2$  = in floating point. This must be zero initially if P = 0 (single precision).
- $\mathbf{y}_1$  to  $\mathbf{y}_N$  values of the N differential equations for the dependent variables. The initial or starting values must be predetermined and set by the user (floating point).
- y'l values of the derivatives of the dependent variables calculated and stored by the user's derivative routine (DER1, DER2). An initial pass is executed through DER1, DER2, and EOS by MARK before the integration process is commenced (floating point).

MARK entry points. - Provision is made through entry points to MARK to transmit certain information to MARK or to render certain information available to the user that is stored internally in MARK:

HC By using the command

CLA\* \$HC

the user has direct access to the current step size being used in the integration process. This is not necessarily the nominal step size, H, introduced by the user in the HBANK (floating point).

NI By using the command

STO\* \$NI

the user informs MARK that he desires i corrections to be performed on the predictor formula used in the Adams-Moulton fixed mode of integration. See Mathematical Description in this Appendix for description of the predictor-corrector formulas being used. In the automatic step size control mode i is automatically 1, and MARK ignores NI. Thus 1 correction is made for each prediction in this mode (fixed point).

TGLO By using the command

CLA\* \$TGLO

The user has direct access to the most recent  $t_{\eta+1}$  calculated, where  $t_{\eta+1}$  represents the value of the independent variable at the end of an integration step (floating point).

Y The command

CLA\* \$Y

gives the user access to the location of the dependent variables (single precision) in the HBANK. This appears as L(Y), where index register 1 set to n and counted down renders all the variables to the user (floating point).

YDOT The command

CLA\* \$YDOT

Y(2) performs the same function as Y for the derivatives of the dependent variables (floating point).

The command

CLA\* \$Y(2)

renders the location of the double precision part of the dependent variables available to the user (floating point).

The commands

CLA\* \$YO

CLA\* \$YO(2)

YO

render the locations of the single and double precision values of the dependent variables at  $t_\eta$  available to the user. Item  $t_\eta$  represents the value of the independent variable at the beginning of an integration step (floating point).

The following symbols refer to entry points used for the automatic step size mode.

EUBAR

The command

STO\* \$EUBAR

stores  $\overline{E}$  for use in automatic error control (floating point).

ELBAR

The command

STO\* \$ELBAR

stores E in floating point for use with AEC.

HMAXT

STO\* \$HMAXT

stores maximum allowable H for AEC (automatic error control) (floating point).

HMINT

STO\* \$HMINT

stores minimum allowable H for AEC in floating point.

YCLOW

STO\* \$YCLOW

stores  $\underline{Y}$  for AEC in floating point.

## CLA\* \$RGERR

permits access to the maximum  $\textbf{E}_{\eta} + \textbf{1}$  for the user in floating point.

NOTE

EUBAR through YCLOW are consecutive locations in MARK.

Space required. - MARK requires  $3453_8 = 1835_{10}$  storage locations. No COMMON is required. The user must supply

$$5N + 7 + 2N(m + 1)$$

storage locations for  $\varphi$  = 0,2 or 7N + 7 + 3N(m + 2) for  $\varphi$  = 4. N = maximum number of differential equations; m = order of differences to be carried in the Adams-Moulton mode.  $\varphi$  = 0,2 is for Runge-Kutta integration or for Adams-Moulton integration in the fixed mode. Also, whatever storage is required for the user's derivative box and trigger control must be supplied.

Timing information. - MARK will do approximately 40 integration intervals per second. (This time was obtained from solving a set of 14 first-order differential equations.)

Checkout. - MARK has been checked out rather extensively using a variety of programs at the Jet Propulsion Laboratory. These programs include the JPL tracking program, a low thrust trajectory program, and a program of a general nature that solves a system of differential equations starting with five equations, repeating these five and adding sets of five with repetition until a maximum of thirty equations have been reached and integrated.

#### Mathematical Description

The classical Runge-Kutta fourth-order equations. - Let the system of equations to be solved be in the form,

$$y'_{j} = f_{j}(t, y_{1}y_{2}, ..., y_{n}) j = 1, 2, ..., N$$

Let  $y_{j,\eta}$  be the value of  $y_j$  at  $t=t_\eta$  and  $f_{j,\eta}$  be the derivative of  $y_j$  at  $t=t_\eta$ . Let h be the step size of the independent variable t. Then,

$$K_{1} = h f_{j}(t_{\eta}, y_{j,\eta})$$

$$K_{2} = h f_{j}(t_{\eta} + 1/2 h, y_{j,\eta} + K_{1}/2)$$

$$K_{3} = h f_{j}(t_{\eta} + 1/2 h, y_{j,\eta} + K_{2}/2)$$

$$K_{4} = h f_{j}(t_{\eta} + \Delta t, y_{j,\eta} + K_{3})$$

$$y_{j,\eta + 1} = y_{j,\eta} + 1/6 (K_{1} + 2K_{2} + 2K_{3} + K_{4})$$

The Adams-Moulton predictor-corrector equations. - Let Yj,Yj be defined as above. Then,

$$Y_{j,\eta+1}^{P} = y_{j,\eta} + h(a_{o}\nabla^{o} + a_{1}\nabla^{1} + ... + a_{m}\nabla^{m})y_{j}$$
(open type)

where  $\nabla$  is a backward difference operator operating on  $y_{j,\eta}^{!}$  and

$$\nabla^{\circ} y_{j,\eta} = y_{j,\eta}$$

The predictor coefficients  $\mathbf{a}_{\mathrm{m}}$  are:

$$a_0 = 1.0$$
 $a_1 = 0.5$ 
 $a_2 = 0.416666666$ 
 $a_3 = 0.375$ 
 $a_4 = 0.348611111$ 
 $a_5 = 0.329861111$ 
 $a_6 = 0.315591936$ 

$$a_7 = 0.304224539$$
 $a_8 = 0.294868003$ 

$$a_{q} = 0.2870754484$$

$$y'_{j,\eta+1} = f_{j}(t_{\eta}, y_{j}) \quad j = 1,...,N$$

$$y_{j,\eta+1}^{1} = y_{j,\eta} + h(b_{o}^{\nabla^{o}} + b_{1}^{\nabla^{1}} +, ..., + b_{m}^{\nabla^{m}}) y_{j,\eta+1}^{P}$$

where  $\Delta$  is defined as above, 1 is the first corrector application, and the corrector coefficients  $b_{\text{m}}$  are:

NOTE

$$b_{m + 1} = a_{m + 1} - a_{m}$$

continuing

$$y_{j,\eta + 1}^2 = y_{j,\eta} + h(b_0 \nabla^0 + b_1 \nabla^1 + \dots + b_m \nabla^m) y_{j,\eta + 1}^{'1}$$

$$y_{j,\eta + 1}^{(i + 1)} = y_{j,\eta + 1}^{(i)} + h \sigma \epsilon$$
 (i)

where

$$\sigma = \sum_{i=0}^{m} b_{i}; \quad \epsilon^{(i)} = y_{j,\eta+1}$$

i is the ith correction on the predictor formula.

The formula for interpolation to interrupt on a dependent variable in the Adams-Moulton mode. The following formula applies:

$$q_j = (-)^q \quad \begin{vmatrix} \mu \\ j \end{vmatrix} \quad \text{where } \mu = \frac{t_{\eta + 1} - t_{\mu}}{h_c} \geqslant 0$$

and

$$\begin{vmatrix} \mu \\ j \end{vmatrix} = \frac{(\mu-1) (\mu-2) \dots (\mu-j)}{(j+1)!}$$
  $j = 1, \dots, m$ 

$$c_{j} = b_{j} + \sum_{i=0}^{J} q_{i}b_{j-i} \quad j=1,...,m$$

b<sub>i</sub> = corrector coefficients described in 2 above.

$$d_j = c_j^j$$
  $j = 1, ..., m$ 

$$y_{\ell,\mu} = y_{\ell,\eta+1} - h\mu (y_{\ell,\eta+1}' + \sum_{j=1}^{m} d_{j}) \ell = 1,...,n$$

Figure A-1 describes the configuration.

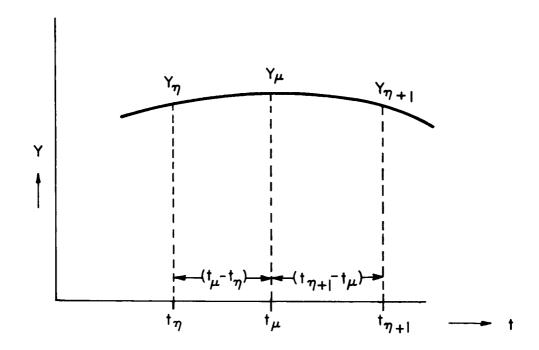


Figure A-1.- Plot of y versus t

The formula for interpolation to halve the step size (H), dropping the subscript j.- The following formula applies:

$$y'(\bar{t}) = \sum_{k=0}^{m} q_{-k}^{(m)} (\mu) y'(t_{\eta-k})$$

where

$$q_{-k}^{(m)}(\mu) = \frac{1}{m!} \quad \frac{m}{\prod_{i=1}^{m}} (i + \mu)$$

$$\overline{t} = t_{\eta} - n\ell h$$
  $n = 1, 2, ...; \ell = 1/2, 1/3, ...$ 

$$\mu = \frac{t_{\eta} - n \ell h - t_{\eta}}{h} = -n\ell$$

Let  $\ell=1/2$ , then  $\mu=-1/2$  where n represents the absolute value of the subscript of  $\overline{t}$  in Figure A-2.

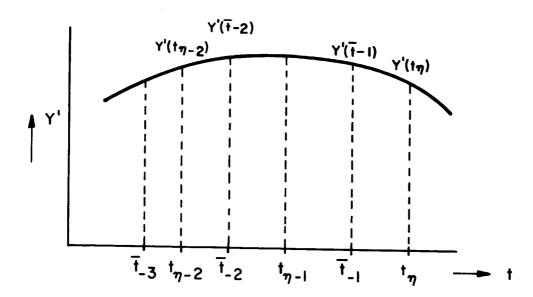


Figure A-2.- Plot of y' versus t

In the program:

$$q_0 = \frac{1}{m!}$$
  $(i + \mu)$  and  $q_{k+1} = q_k$   $\frac{(\mu + k) (m - k)}{(\mu + k + 1) (k + 1)}$ 

where k is the absolute value of the subscript of t in Figure A-2.

Automatic step-size control. - The following denotes automatic step-size control:

$$E_{\eta + 1} = MAX \begin{vmatrix} y_{j, \eta + 1}^{P} - y_{j, \eta + 1}^{c} \\ A D_{j} \end{vmatrix}$$

where

$$A = \left| \frac{a_{m}}{b_{m+1}} \right|; \quad D_{j} = MAX \quad \left| y_{j,\eta+1}^{c} \underline{y} \right|$$

The expression  $E_{\eta}+1$  represents the maximum error in any of the dependent variables in the final iterate  $y_j$ ,  $\eta+1$  due to truncation error in the step from  $t_{\eta}$  to  $t_{\eta}+1$ . The user, through the entry points, supplies MARK with a set of values to be described as follows:

- (1)  $\overline{E}$  upper bound on the truncation error  $E_{n+1}$ .
- (2) E lower bound on the truncation error  $E_{\eta} + 1$ .
- (3)  $h_{\text{max}}$  maximum allowable value of the step size.
- (4)  $h_{min}$  minimum allowable value of the step size.
- (5) y a constant used to prevent unnecessary reduction whenever  $|y_{i,n} + 1|$  is small. y > 0.

The step size, h, is doubled, left alone, or halved depending on the following inequalities:

- (1) If  $E_{\eta} + 1 \le \overline{E}$  for m successive steps, the step size, h, is set = 2h.
- (2) If  $\underline{E} < E_{\eta + 1} \leqslant \overline{E}$ , the step size, h, is left alone.
- (3) If  $E_{n+1} > \overline{E}$ , the step size, h, is set = 1/2 h.

The program preserves all the conditions  $y_j$ ,  $\nabla_j^m + 1$  at  $t_\eta$  and integrates to  $t_{\eta} + 1$ .

- If (1) holds, then MARK sets up the doubling procedure and integrates m + 1 more steps checking that (1) holds at each step. If (1) holds, the doubling procedure is completed and h = 2h.
  - If (2) holds, integration continues normally.
- If (3) holds, then MARK restores  $y_j$ ,  $\eta$ ,  $\nabla_j^m$ ,  $t_\eta$ ,  $y_j^t$ ,  $\eta$ . It executes the end of step box to restore those values at  $t_\eta$ . Finally, the halving procedure is executed and h=1/2 h. Thus, it is never necessary on the basis of error control to restart the integration procedure in the Runge-Kutta mode. Item  $\overline{E}$  is approximately equivalent to specifying the number of significant figures to preserve locally throughout the integration. Item  $\overline{E}$  should normally range from  $10^{-8}$  to  $10^{-3}$ .  $\underline{y}$  may be determined by the user but should probably range from  $10^{-5}$  to 1.

# APPENDIX B COMPUTER PRINTOUT

COMMON YOUTH, RIGHT, PART, PAR	MAIN - EFN	'N SOURCE	SIALEMENT	r IFN(S)	: 1· •	69/90/20	PAGE 1
COMMON   CONSTITUTION   CONSTITUTI	/DATA/	S I W	TMAX	TMIN	PMAX	MAINGOOS	
A		T. T. T.	KELEKK	A04	08.00	MAINOOD4	
COMMON / HEBANKI / HEMPER   DEPTI	ď	10 A 10 II.	OTH	107L	- 25 - 25	MAINCOCK	
COMMON / HEANIN / MACES   COMMON / HEANIN / MACES   MACES		OND .	4 d	FMU	PTYSOR	MATNO007	
CUMMON / HEANNY / MATCH   MA		F21	j	FHP	COSPSIA	MAINDOOB	
COMMON CREATEST   CONTINUE		UFHDR	UFHDT	DCPDT	nCPDY1.	MAIN0009	
CUMMON / HBANKI / MORDER   MORDER   MORDER   MAINDIS		OCPUY3.	5P2	EMUINI	EMUS	MAINDOID	
LUMMON ACKSAL C. SETIS.TZ.EM. IEMM.TERP.2 MO(11)	N / THRANK 1/ W		9	_		MAINOOLL	
COMMON / NEW PLOTULADOT	T. C.	14	NVPI YO	(11)		SO MAINDIS	
COMMON/ESTINATION TO COMMON / RECT / LUMP: NTUL EMBAD DUBLISTO DELICION TO COMMON / RECT / LUMP: NTUL EMBAD COMMON / RECT /	JCKSK/ CARC	PSTIZIEM	IEHM. TERME	PRMODIRAK		MAIN0014	
COMMON / POWLOS/STIGNED PER PER PET TOWN TEXPELS	COMMON /NEW/ PLOTG, RDC	TO S				MAIN0017	
COMMON / FOWLOS / INQUERE DEPURED DEPU	COMMON COCKY TOCK	ייייייייייייייייייייייייייייייייייייייי				MAINIUSB	
COMMON / POWLOS/ CrS4	COMMON/GAUSS/YSQUAP-OC	CPURIDCPUP	*OFHUP *F17	ONMNTR. D	5673	WAT NOO 19	
Denyli	COMMON /POWLOS/ COSA	<b>\</b>	DWD	TOMO	!	MAINOSO	
DHILDS   DHILDS   DHILDS	ā	. DMDY2	DMD	SOMO		MATNO021	
DIMENSION DEFICIAL DEMUNSA:  DIMENSION DEFICATION DEFICIAL EMRAD  DIMENSION DU (3002): SOA (3002)  COMMON / RECT / DD : SOA   LB  COMMON / RECT / DD : SOA   LB  COMMON / CONST / ONTER: EUBAR-ELDAR-ICLOA-BMAXI-HMINI-ND  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  COMMON / GRAPHU / X-AXI : XMINI : TMINI-NDATE  NYDI = 0  NAINNO42  MAINNO44  M	i	i			C	MAIN0022	
DIMENSION DATE(04) * PLT(12)  DIMENSION DATE(04) * SOA * LB  COMMON / RECT (		-	1			MAIND23	
COMMON / KECT / DU ' SOA ' LB  COMMON / KECT / DU ' SOA ' LB  COMMON / CONST / OKNER' EUBAK:FLLBAK:TCLO2.HMAXI.HMINT.KN  COMMON / GKAPHI/ X:AXI XMINI 'YMXI.'NHINI.DAE  COMMON / GKAPHI/ X:AXI XMINI 'YMXI.'NHINI.DAE  COMMON / GKAPHI/ X:AXI XMINI 'YMXI.'NHINI.DAE  COMMON / GKAPHI/ X:AXI XMINI 'YMXI.'DAE  COMMON / GKAPHI/ X:AXI XMINI 'YMXI.'DAE  DAIA PIZ ' PAD / 6-2831853 ' 0-0174533 /  NIEST = 0  NAINO28  NOTE = 1  NYOI = 0  INS = 0  INS = 0  INS = 0  IN		ŝ					
COMMON / KDDIS / JUNE / NVDI COMMON / CONST / OKNER EUBAR/SCLOZ/HMAXILHMINI/KN MAINNOTE COMMON / GRAPHI/ X.AXI XMINI : TMAXI : YMINI : PATE COMMON / GRAPHI/ X.AXI XMINI : TMAXI : YMINI : PLT	DECT /		1				
COMMON /CONST / OKDER: EUBAK: ELBAR: ICLO_ALHWAXI. HMINO16  COMMON /GKAPHI/ X:AXI :XMINI : PAIN: DATE  COMMON /GKAPHI/ X:AXI :XMINI : PAIN: DATE  DATA PIZ : RAD / 6.2831853 : 0.0174533 / MAIN0028  DATA PIZ : RAD / 6.2831853 : 0.0174533 / MAIN0028  102 NEE = 1  NYDI = 0  IGH CALL INPUT  PRINOPHNI  PRI	/ KD0TS /		9				
COMMON / CONST / OWNER: EUBAR: ECLOALHMAXILHMINING MAINNUS COMMON / GRAPHI/ X:AXI : XMINI : TMAXI : YMINI: DATE  COMMON / GRAPHI/ X:AXI : XMINI : TMAXI : YMINI: DATE  COMMON / GRAPHI/ X:AXI : XMINI : TMAXI : YMINI: DATE  DATA PIZ : PLO / 6.2031853 : 0.0174533 / MAINNUSS  NOTES = 11  NATUREST = 0  MAINNOWS MAINNO						MAIN0026	
COMMON / GRAPHU/ X:AXX : XMINI : YMAXI , YMINI: DATE  COMMON / GRAPHU/ X:AXX : XMINI : YMAXI , YMINI: PLT  DATA PIZ : PAD / 5.1415027 : 1.5707023 /  DATA PIZ : PAD / 6.24316027 : 0.0174533 /  102 NIEST = 0  NIEST = NIEST = 0  NIES = 0  NIEST = 0  NIES = 0  NIEST =	/CONST / OK		BAR YCLOAR	HMAXTVHMI	J.KD	MAINNU16	The second secon
MAINNO15  DATA PI2 ' PAD / 6.2831853 ' 0.0174533 /  102 NIEST = 0  NATIONO29  NOGG = 11  NYD1 = 0  NY	/GKAPH1/ X		YMAX1 ,YMI Ymaxu ,Ymi	N1,DATE NO . PLT			
DATA PI ' P104 / 3:4415927 * 4.570793 / MAIN0028  102 NIEST = 0  NIEST = 0  NIEST = 0  NATIN029  NOEG = 11  NYD1 = 0						MAIN0015	
102 NIEST = 0	PI , P104 7	1415927	1.5707903	,			
MAINDUSS  MAINDUSS  NOEG = 11  NYD1 = 0  IRSN = 0  IN = 0  IN = 0  IN = 0  NUM = 0	DATA FIZ . RAD /			`			
MAIND 29  MAIND 29  MAIND 20  MAIND 30  MAIND		!				MAINUNG	
NOÉG = 11  KU=4  39 CONTINUE  NYD1 = 0  IRSN = 0  ILB = 0  NAIND042  IGA CALL INPUT  IF ( IRSN .EG. 1 ) GU IO 39  PRITO=PRI PLOIT  PRITO=PRI PLOIT  PRITO=PRI PLOIT  PRITO=PRI PLOIT  PRITO=PLOIT  MAIND043  MAIND045  TESJJ=HGANK  MAIND046  DO 20 II = 1*10  MAIND049  MAIND049  20 CALL ON(II)	NI III					WATNO 29	
NYD1 = 0	11	!	•	:		MAIN0030	The same of the sa
104 CALL INPUT  104 CALL INPUT  104 CALL INPUT  104 CALL INPUT  105 CALL ON(11)  106 CALL ON(11)						MAINDU31	
NYD1 = 0   IRSN = 0   LB = 0   NU = 0   NU = 0   IG4 CALL INPU]   IF ( IRSN .EG. 1 ) GU 10 39   PRNTO=PRNT   MAINDOWS   MAINDOWS 	Ç						
IRSN = 0   LB = 0   NU = 0   NU = 0   IG4 CALL INPU]   IF ( IRSN .EG. 1 ) GU 10 39   PRNTO=PRN   MAINDG43   PRNTO=PRN   MAINDG43   PRNTO=PRN   MAINDG43   PRNTO=PRN   MAINDG43   PRNTO=PRN   MAINDG43   PRNTO=PRN   MAINDG44   MAINDG46   PRNTO=PRN   MAINDG45   MAINDG46   PRNTO=PRN   MAINDG46   PRNTO=PRN   MAINDG46   PRNTO=PRN   MAINDG46   PRNTO=PRN   MAINDG46   PRNTO=PRN   MAINDG46	NYD1 =			:	:		
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104 CALL INPUT  IF ( IRSN .EW. 1 ) CU 10 39  PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT PRNTO=PRNT MAIND043 MAIND045  TESJJ=HBANK  DO 20 II = 1*10  MAIND046  20 CALL ON(II)	18						
104 CALL INPU!  IF ( IRSN .EW. 1 ) cu 10 39  PRNIO-PHNI  PRNIO-PHNI  PRNIO-PHNI  MAINDU43  MAINDU43  MAINDU44  MAINDU45  20 CALL ON(11)  MAINDU46  MAINDU49  MAINDU49	1				1		
IF( IRSN .EW. 1 ) GU 10 39  PRINCEPRINT PRINCEPRINT PROTT PROTT PROTT PROTT MAINDQ4 MAINDQ4 MAINDQ4  DO 20 II = 1*10 MAINDQ4B  20 CALL ON(II) MAINDQ4B	104 CALL						
PRNTO=PRNT PLOIT = PLOID MAINNOUS MAINNOUS TESJJ=HBANK DO 20 II = 1/10 MAINNOUS PRINTOUS	IF ( IRSN .EW. 1 ) GU				* *		
PLOIT = PLOIN MAINNOG44 MORDER = URDER MAINNOG45 TESJJ=HBANK  DO 20 Il = 1/10 MAINNOG46  20 CALL ON(Il) MAINNOG49	:	1	:				
MORDER = UNDER TESTJ=HBANK DO 20 II = 1/10 MAINNO46 20 CALL ON(II) MAINNO46	PLOIT = PLOID					MAINOORS	
TESTJ=HBANK  DO 20 II = 1+10  RAINDQ46  20 CALL ON(II)  MAINDQ49	MORDER II CRUEK	;				TATION TO THE	
20 CALL ON(11) MAINDU46	:	!				MAINDOC	
CALL ON(II) MAINIUMB	11 00 00						
	CALL ON(II)		:				

- EFN SOURCE STATEMENT - IFN(S)	- (9	· · · !	PAGE.
105 CALL OFF(9) MUFLAG = 0 FINVP=0. FINVPI=0. NUAR=10 PROFI=1.	MAINDD47 INPUND74 INPUND75 MAIND52	7.2	
1047 CALL SMARK(KD,NUAK,MOKDER,NKTN,NTKG,EURAR,ELBAR,HMAXT,HMINT,YCLOW,MAINDGS, 1FINVP,PRNIO YO(1),DMAX,YO(1),RMIN,YO(2),TMAX,YO(2),TMIN,YO(3),PMAXMAINDGS 1,YO(3),PMIN,FINVP,TESIJ,YD(1),RUOT,FINVP,PLOTI ) 105 GO TO (40,41,42,43),MRIN	XXI,HMINI,YCLOW,MAINNOSS TWIN,YO(3),PMAXMAINNOSS MAINNOSS MAINNOSS	2,	
41 C=COS(Yu(2)) RCT=Y0(1)*C S=SIN(Y0(2)) RST=Y0(1)*S YSQUAR = 0.0	MAINDDS7 MAINDDS8 MAINDDS9 MAINDO60	35.	
DO 50 I = 4.6 YADU = YOLI) YSQUAR + YAUD * YADU SQUARINUE = YSQUAR + YAUD * YADU SQUARINUE = SQRI( YSCUAR )  107 CALL DENSE X = FN / C1	MAIND063	9h	
X JE OF TE 2000,200 2) TERM AAIN TEP		6 7	
108 CONTINUE  IERM2 = IERM * 1ERM  CALL COLL( YO(1) * YO(3) * GNU )  7 = GNU/F * 1591 * 1991		53	
110 CALL FIELD  Y = FH / F  YI = Y * SINPSI  YI = Y * YI	MAINOD70	56	
YLYI = YL * YL YLYI = YL * YT EM = 145 * YIZ / IERM EMRAD = PLUS * SGPT( EM* EM + YL2 ) EMD = 14 - EM + EMRAD EMUS = 14 - X / EMU		58	

THE TARGET OF THE PRINCIPAL PRINCIPA	
IF( EMUS ) 20U3/2004 20U3 WRITE(6/2005) EMUS 20U5 FURMAT(13H MAIN EMIS = 'E15.5 )	
2004 CONTINUE	
116 EMU=SQRT(EMUS)	MAINDGR2
117 CALL FORCE	MAINNOR3
118 DMD=F2*TEKM	MAINOBH
DANI IFFE ST.	MAINDORS
DMT.J=EM/12400.	MAIN CORT
DMT2=DMN2/UMD	MAINORB
DMUN2=YL2/COSPSI	MATNOOD
DMD1=EMU/.5*EMD	MAIN0091
DMUG1=C1+UMD1	MAINOGS
	MATN0093
COMPUTE DERIVATIVES OF M	MAINDO94
	MAINN096
IZO UNDORTO DE LOS CONTROLOS COMO DE LA CONTROLOS COMO DE LA CONTROLOS CONTR	MATNOG97
UMDY = COMNT * UP HOLIOPOLIOPOLIOPOLIOPOLIOPOLIOPOLIOPOLIO	MAINDO98
DMDY1=DMT2*UCPDY1	MAINITO
	MATNOIDI
DMD13=DM12*DCFD13 121 DMDF=+12/F*1.F*1.F*1.F*2	MAINDIOS
	MAINOLOG
COMPUIE DERIVATIVES OF MU	MAINILOS
122 DMUDR=(EN*((EM*UMDR+DMUN1*DFHUR+DMUN2*DCPDR)/EMKAD	MAINOIDS
	MAINDID8
1 - CMCT - CENT CENT - CMCT + UMONT + UT + UMONT + UCD T - CENT AD	MATN0109
UN1*DFHUP+DMUN2*DCPUP)/EMRAD	AAINII C
	WAIN0112
	AIN0113
(IMDDTZ=(\EM*DMDTZ+PMOVZ*DCPDYZ)\EMRAD=DWDY2)*UMUN3 DMDDY3=(\EM*DMDY3+PMOVZ*DCPDY3)\FMRAD=PWDY3\*DMUNX	MAIND114
1.F-6) /FMPAD)*	MATNUTAL MATNUTAL
ENDWG 1	MAINOI17
	MAIN0118
COMPLITE KAPPA	WAINO119
124 EMZ = Y12/(1EKM2 + 2**2)*.5	MAINDISO
A=EMZ*TERM	ATINITAL ATINITAL
	MAINOLDS
U#A**2=B**2+YL2	MAINO124
į	MAINO125

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MAIN - EFN SOURCE STATEMENT - IFN(S) -			
	ACTONTAM.	7.	
ローストの一つにファルの	CHICALON		
745 (747) T1017 T1	MAINOLOG		
	MAIN0132		
C COMPUTATION OF EPSIFIN CONDITION	MAIN0133		
	MAINDIST		
1CO ETO-11N-15+7/74+10+47-15	CCTUNIEW		
C COMPUTE COS(ALPHA)	MATNO 137		
! : : :	MAINOISB		
127 DMDSI=YLYT/TEKM	MAINOLIS		
- 1	MAINOIHU		
	MAIN0141		
128 CUSA=EMU/SQRT(EMUS+1MVDSI**2)	MAINO142		
COMMUTE DEBINATIVES OF DAY COMPUTED	MAINOIRG		
C CUMPULE DENIVALIVES OF RAI COURDINALES	MAINHIGH		
129 YD(1) = (YO(4) MU*(MU)Y1) ZEMUS		2	
YD(2)=(YO(5)-EMU*D:\DD(2)/EMUS/YO(1)	MAINDIGZ		
	MAINDIAB		
= DMUDR/EMU + YU(2)*YU(5) + YL	MAIN0149		
# (DMUDI/EMII - YD(1)*YD(5) +	MAINDISD		
YD(6) = (DMUDP/EMU - 10(6)*(YD(1)*S+YD(2)*RGT))/RST	MAINOISI		
10.17 = 10.17 = 11.4 ± 4.1 ± 1.4 ± 0.1 ± 0	MAINOISS		
VI (4) = 1 = 1 ADDA / THIP* V (9)	CTINITY W		
	MAINDISS		
C. 10.COMPUTE THE DOPPLER SHIFT USING JUNES METHOD	MAIN0156		
	MAINO157		
	MAIN0158		
		A5	
	MAIN0160		
ن د	O.	œ	
42 IF (NTRG .Eu. 3 .Arib. J .Eg. 2 ) NTRG = 11	MAIN0163		The second secon
CALL OUTPUT (NIRG)		93	
	MAINO165		
CALL TRAIL	OUTINITEM		
		, ,	
* : X : 4 : 4 : 6 : 6 : 6 : 6 : 6 : 6 : 6 : 6	0	96	
40G IF LATUI = 2 JAUUNTAULIAUUI 40G1 CALI OUIPUT(1)		100	The state of the s
J. W.	•	•	
		03	
4000 CALL TRA14			
	+	70	
47 PL017 = PL011 + PL610	MAIN0168	C01	
	MAINO169		
(E)NO - 197 4T		α ο -	
134 CALL OFF (6)	MAIN0171	112	

				:		
CALL UN(9)	WAIN0172	114				
TINDOMENTE G. 1. AND NOAK-FE-10) GO TO 1045	MAIN0173					
CALL IKAI4	MAIN0174					
COMPUTE FOWER LOSS IN NEAR FIRE D						
		,			:	
NUAK=1.1	MATAIN 175	118			•	
HBANK I • U01	MATING 76			İ		
THE I A=THE I AU*KAU	MATAIN 27					
EMUPI=EMUINI*PI	MATNOTA		:		•	
	0/1/11/15					
ALL CSINT (EMUPI+CTMUPI+SIMUPI)		100				
CALL CSINT (EMUINT*:12 CIM2PI SIM2PI)		31				
		124				
EMUPIZ=EMUINT*P102	MATANTA	j				
DENORT - 5772+ALOG(E-UP1)-CIMUPI+SIN(EMUPI)/2.* (SIM2PI-2.* CMIPI)	MATANTAS	-		:		
+COS(EMUPI)/2++(_57/2+ALOG(EMUPI2)+CI_02F1-2-+CIMUPI	TO TONE ON					
COSPSIESTN (THETA) ACTN (YOUR STATES OF STATES	CATINITAN	126	126 127 12A	129	!	
#COS (THEIA) #COS (VO(2))	MAINCIAG					
R02=R0**2	MAINOLAS	130	131 132	133	134	The second secon
R2=Y0(1)**2	MAINITHO					
<b>アナの十次の十大の11/10 + 成コチン(1) + COプロペト</b>	MAIN0187				:	
RF=SORT (RP2)	MAINDIAB					
PS1:P1-ARCOS (RP2+F02-RV) / (1.*RP+KO))	WALCOLD W	135			1	
PROFIE((COS(EMURIZ+COS(PSI))+COS(EMUPIZ))<		34				
/(PI2*RP2*DENOM)*.7161972E-2/F2/FMIINT	TATIMITATION OF THE PROPERTY O		i	;		
60 10 1047	MAIND193	ž .	0#1 6CT	141		
۲۵(۴) = -۲۵(۴)		:	:	!		
	MAINI194					
) i (3)	MAIN0195	!				
	MAIN0196	146				
NTO + DIO. I	MAIN 197	148				
	MAIN0198				1	
	MAINU199	:	; ;			
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and the same of th	MAINOSOO	15.5				
		Š				
FOUR TARES PELOKN FROM MARKS	MAINNZNZ				-	

	#X, INPUGGG #U, INPUGGG FN, INPUGGG FN, INPUGGG FN, INPUGGG *1, INPUGGG *1, INPUGGG *1, INPUGGG *1, INPUGGG *1, INPUGGG INPUGGG INPUGGG INPUGGGG INPUGGGG INPUGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGG	
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AMON / CKSK/ C.RCT.S.PST.Z.EM.TERM.TERM.TERM.TERM.TERM.TERM.TERM.T	INPU0017 INPU0018	
AXU 'XMIND 'YMAXU 'YMIND 'PLT TLE TLE 5) U-U196 ' 0.0016 / 265-98 ' 1056-3 / 265-98 ' 1056-3 / XMAXU ' XMINU ' YMAXU ' YMINU ' XMAXI ' XMINI ' YMAXI ' YMINI URUEK ' EUDAR ' ELDAK ' TCLOW ' HMAXI ' HMINI ' KD TCLOW ' HMAXI ' HMINI ' KD		
USION TITLE(20) USION PLT(15), DATE(4) USION DL 30)  LIST / XMAMES / XMAXU , XMINU , YMAXU , YMINU , XMINI , YMINI , YCLOW , HWAXI , HMINI , KD , CLOW , HWAXI , HMINI , KD , CLAST , NITILE , MCONSI , MI STATEMENTS AT (8F10.3)		
XMAXU , XMINU , YMAXU , YMINU , XMAXI , XMINI , YMAXI , YMINI , QBUER , EUBAR , ELRAR , FLOW , HMAXI , HMINI , KD , U , LASI , NIILE , NICONSI ,		
FURMAT STATEMENTS FURMAT (BF10+3) FURMAT(10x+5F10+4)	29	
FUKMAT (10x of 10 of 4)		
FURMATICADA) FURMATICALL) FURMATICALL FURMATIC 1H1 + 20X + 20A4 ) FURMATIC // 2UX + 3UHINITIAL RAY FOSITION + 1UX + 3UHINITIAL RAY LIMECTION + 1		
PACIEKIST	F6.2 / F6.2 / J	

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HU = D(23) PKFKAC = D(24) AMBUL = D(25)		1		
CALCULATE NO.	: : : : : : : :			
AMBUA = AMBUL + KRERU THO = THETAO + RHEND				
SNLAMI = SIN( AMBUA ) SNLAM2 = SNLAM1 * SNLAM1 SNLAM3 = SNLAM2 * CHLAM1			21	
SNTHOL = SIN( THO ) SNTHOL = SNIHUL * SNTHOL SNIHOL = SNIHUL * SNIHOL			22	
TNTHO1 = 1AN( THO ) INTHO2 = 1NTHO1 * INTHO1			23	
STSL = SNTHOL / SMLAML ZMI = SGKT ( 4.0 - 3.0 * SNTHOZ ZM2 = SGKT ( 4.0 - 3.0 * SNLAMZ ZM3 = ZM2 * SNTHOX ZM4 = ZM1 * SNLAM3 ZM5 = ZM3 / ZM4 ZM5 = ZM3 / ZM4			25.	
H = H0 * ZMS HPRIME = .707 * h HPRIMI = SGRT ( 1.0 + 4.0/ INIHO2	102 )			
SIZMS = ZMS IF ( NAUIO -LF, U ) GO TO 60 RO = REARIH * SICL * STSL - I	HPR.IM.		26	
CALCULATE 40				
WALSHI = U.5 * IAN( THO ) WALSHZ = ATAN( WALSHI ) WALSH3 = WALSH2 / RYEKD AU = WALSH3 + DELAO D(04) = AO			32	
	THETAO, PHIO			
W1 = ( RU = 6728. ) / 50. T17 = 0.5 * ( 1.0 - W1 - EXP(-W1) ) ENF_= 2.765 * EXP(_I17 )	(		7.3 3.6	

INVO - ETA SOURCE STATEMENT - ITANO		
JAN = U.U JAN 1 = 1.5 JAN = ENXH + V(I) * EXP( -ZX / W(I) ) JAN = SOHT( ENAR ) JAN = 4.U * ENAR	## 0#	
ENX = ENXR * ( 1.659E3 * ABS( 1HV = 1.5707963 ) + 16570. )  IF( RO = 7378. ) 40.41.41.  40 TM = (RO = 7378.) 500.  CACTOD = 640( = 1.87M.)	7.47	
FAX = ENX + FACTOR +1 EN = ENX + ENP PADELN = PKFRAC + FM		
PLT(02) = THE1A0		
0 0 0 0	:	
in a n		:
11 11 11		
= MODE		
A = A0 * RPERU		
(U1) (U2) (U3)		
F2 = F * F C1 = 1.24E4 * F2	52 53	
112 CALL DENSE	INPUNDA4	
x = EN / C1		

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	INPU - LFW SOURCF STATEMENT - IFN(S) -	100000	Fage 11
01101	IF( TERM, ) 2000/2000/2001		
2002		ς. O	
, .	TERM = TERM = TERM C = COS ( HO )	41	
	\(\frac{1}{2}\) \(\frac{1}\) \(\frac{1}{2}\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(\frac{1}2\) \(1	84	· control of the cont
	YUG2 = YO(6) + YO(5) YSQUAR= YO42 + YO52 + YU62 RIYSOR = SWRI( YSOUAR )		
115	115 CALL FIELD	63 INPUNU91 65	
	Y = F1 / F YI = Y * SINCSI Y(2 = Y  * 1T		
	. 4.2		The second secon
	1 0.55 %		
	TEST IF VALUE OF EVUS IS ABMORMAL		
2003	IF ( FMUS ) ZOU3/20r3/20u4 ) IKSN = 1 WKIIF(6-2005) EMUS FPENRAT( 14H INPUT FMUS = / £15.5) PETURN	70	
2004	CONTINUE FMUZ = SORT( EMUZ) FMUINT = EMUZ	22 24	
	YU(U4) = YO(U4) + EMUZ YU(U5) = YO(05) + EMUZ YU(U5) = YO(05) + EMUZ		
	TEST PROGRAM UPITON INDICATORS		
	IF ( r.P.LOT .LF. U ) 60 TU 9		

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SIBFTC OUTPU LIST, REF

0.0 TP 0.0 T	MOEO, OUTPOULS MA(260) OUTPOULS MA(260) OUTPOULS OUTPOULS OUTPOULS OUTPOULS SI OUTPOUS 21 OUTPOUS 22 OUTPOUS		NUTPNU24 NUTPNU25	ისТРпиว6 ისТРпиэ7 ისТРпиз28	nuTPnu29 nuTPnu3u	00TP0033 00TP0033 00TP0034 00TP0037 00TP0038	00TP0041 00TP0042 00TP0043 00TP0044
ž 200	* 2118 CMU PUTM YUTM			(IUP/RCT) **?)			
RELEPRY PAIO MOARY OFFID	PUYS, SP2,  NU, MUELACOL  NO, ALEOL  T.Z.FM.IERM'IERM'S  R.DC D.P. NOHUP; NMONY,  OWONY, OMONY,  OWOUT, OMONY,  OWULL	2) PLT(15)	SOA • 1.15 NYU1	200 DSH1FT=-2.424067E-n.*F*YO(10) 201 VALCRT=SGKT(PMUUR*~MUUR*(UMUNT/YO(1))**z+(PMHUP/RCT)**?) 1 /(20.943933*F*EMUS)	TU 101 GU 10 1UA	;	
	DUZE. DCI NY NACHDER! FINALY FRCTISKS: GUATION COSA! DMIUR!	20	. UO (S) (A) (E) (A) (E) (A)	-: *F *YO (	50 TO 101 ) GO TO	10) 60 To 46	

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                                                            OUTPOU49
OUTPOU50
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  OUTPNURS
                                                                                                                                                                                                                                                                            22 wKIIE(6,1003) FINVG,YO(1),THF1A,PHI,YO(3),NBHIFI,PL,
1 YO(7),YO(4),YO(5),YO(3),FEHSTIN,
2 YO(8),RMOU*NAKG,VALLPI,EN,GNII,GKODEL
         SOUPLE STATEMENT - IFN(S)
                                                                                                                                                                                                                                                                                                                                                   216 6U T() (29,4U,41,42,43,44,45,29,47,29,29) , JFLAG
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            IF (ABS(THEIA - 90. ) .LT. 2.0 ) 60 TO 101
NYD1 = RYD1 + 1
                                                                             27 YUSUR = YU(4)**2 + YO(5)**2 + YU(6)**2
                                                                                                                                                                                                                 DELSEO.0
60 10 22
PLEID.*ALUGIA(EMU*CHOPT*FXP(-Y0(11)))
                                                                                                      GROUP DELAY IN MIL! 1SECONDS
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL CALCOUT LB + "U + SOA )
CALL CALCOST LL + "A + YY )
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           46 IF ( PPLOT .LO. U ) REIUNN
                                                                                                                                                                                          213 IF (NPOWER.NE.U) 60 f0 21
214 PL=0.0
          빌
                                                                                                                                                      212 CALL POLAK
FARU = KAKG*57.295-795
                              26 IF(N.NE.13) GO 10 27
209 PKITE(6.1007) TITLE
28 WKITE(6.1002)
210 to = 1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               VRITE (672046) YD(1)
                                                                                                                              211 GKOUEL=10(7)/3.UE2
                                                                                                                                                                                                                                                                                                                                                                                                    WK11E(6+2041)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              PESET COUNTERS
                                                                                                                                                                                                                                                                                                                                                                                                                 60 10 217
WKITE (6,2042)
                                                                                                                                                                                                                                                                                                                                                                            ERITE(6,204U)
60 In 217
                                                                                                                                                                                                                                                                                                                                                                                                                                                 43 FKIIF (6,2045)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         44 FKIIF (6,2044)
60 TO 217
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 45 WKITE (0,2045)
217 JUMP = 2
         04100
                                                                                                                                                                                                                                                                                                                 215 1 = 1 + 1
                                                                                                                                                                                                                                                                                                                                                                                                                                       GU 10 217
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PAGE																
05/06/69			OUTPARA	9600TDO	OUTPOIND	OUTPOINT	OUTPOINS	DUTP0103	0UTP0104	LONGITUDE7X100UTP0105	PATH6X2HY1140UTPn1n6	RAY PATHBX26HOUTP0107	OUTP0108	001P0109	OUTPO110	0UTPn112
OUTPU - EFN SOURCE STATEMENT - IFN(S)	29 RETURN	C FORMAT STATEMENIS	2040 FORMAT (25H0STOPPED ON TEST FOR KMAX)	2041 FURMAT (25HOSTOPPED ON TEST FOR HMIN)	2042 FORMAT (30H0STUPPEL) ON TEST FOR THETA MAX)	2043 FURMAT (30HOST UPPEL ON TEST FOR THETA MIN)	2044 FORMAT(28HOSTOPPED ON TEST FOR PHI MAX)	2045 FORMAT (28HOSTOPPEL ON TEST FOR PHI MIN)	2046 FORMAT (9HOKDOT = £15.6 )	1002 FORMAT(10X10HPHASE PATHEXEHRADIUS10X10HCOLATITUDEEX9HLONGITUDETX10CUTP0105	1HABSORPTION6X10HDUPPLER SP6X1UHPOWER LOSS/10X10HGROUP PATH6X2HY1140UTP0106	2X2HY214X2HY314X5HMI**<11X4HY**212X1UHEPSTEIN_CD/10X8HR	3POLARIZATION - MOD AND ARGEXENDEL MOIDX1HN15X2HNU14X	411HGROUP DELAY)	1003 FORMAT(/6x1P7E16.7/(6x7E16.7)) 1007 FORMAT( 1H1 , 2UX , 2UA4 )	END

SC - EFN SOURCE STATEMENT - IFN(S) -	UZ/UB/CGG
BLOCK DATA COMMON (GRAPHE) X AXU •XMIND •XMAXE •XWIND • PLT	
COMMON /GRAPHI/ XNAXI ,XMINI , YMINI,DATE	
COMMON /CONST / ORDER' EUBARIELBARITCLOWINMAXIIHMINIIKD	MAINDO16
C NUMINAL PLOI LIMITS	
U	
DAIA YMING , YMAXA / U.0EG , 1.2E4 /	
DATA XMINO , XMAXA /-1.8E1 , 2.0EU /	
DATA XMINI * XMAX1 / 0.0E0 * 2.0E4 /	
DATA YMINI • YMAX1 / 0.UEG • 1.UE4 /	
C NOMINAL INTEGRATION PARAMETERS	
<b>5</b>	
DATA ORDER , EUBAR , ELBAR / 1.0E U , 1.0E-5 , 1.0E-7 /	
DATA YCLOW . HMAXT . HMINT Z 1. DE-7 . 1. UE 4 . 1. 0E-7 /	
J.	

SIBFIC SCA

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02/06/69 PAGE			
SCA - EFN SOURCE STATEMENT - IEN(S) -	SUBROUTINE PRAMIX:Y:LL:XMIN:YMIN:XMAX:YMAX:XLEN:YI.EN) DIMEMSION X(1):Y(1)	Y( LL + 1 ) = XMIN	X ( LL + 2 ) = ( XMAX - XMIN ) / XLEN Y ( LL + 2 ) = ( YMAX - YMIN ) / YLEN RETURN

PAGE 21

SUBROUTINE CALCOUTINE CALCOUTINE	
COMMON ZGRAPHUZ XWAXU *XMIND *YMAXU *YMIND*PLT COMMON ZGRAPHIZ XWAXI *XMINI *YMAXI *YMINI*DATE	
C DIMENSION PLDAT(3bn) : X(3u02) : Y(3u02) DIMENSION PLT(15) : DATE(5)	
MODE = PL1(13)	
CALL PRAMICKITILLIVMINGITMINGITMAX0ITMAX0112.1	
IF( LVAL .NE. 1 ) GO TO 12 CALL AXISTO.0.0.0.21HUIS FROM FLD LA IN KM/21/10.090.01 X(LL+1).	
1 X(L  +2)) CALL AXIS(0.00.00.04HUIS ALONG FLD. LN. IL. KM	
בסיטי זינריבליי	7,1
CALE SYMBOL (1.0.9.6.0.10.8HRU = 10.0.1	16
CALL NUMBER (2.0/9.6/0.1) PLIMIN 1 U.U. + 2 L. CALL SYMBOL (4.0/9.6/0.10/8HAO =:0.0/8)	20
NUMBER (5.019.610.11 PLT(04) 1	22
CALL SYMBOL (7.0/9.0/0.10/8HDELAO =:00.0/8)	hc 76
SYMBOL (1.0.9.2.0.10.8HTHE1A =	. 80 ±
CALL NUMBER (2.1/4.9.2.1/1) PLING2) & 0.11 + 3.1 CALL SYMBOL (4.0/9.2.1/10/8HRO =:0.0/4)	32
NUMBER (5.019.210.11 PLT(05) 1	34
CALL SYMBOL (7.0.9.2.0.10.8HHPRIME =:0.0.0.8)	36
SYMBOL (1.0'8.8'0.10'8HPHI	0 n
CALL NUMBER (2.0.8.8.0.1) PLI(0.5) . 0.0 . 3 /	7th
NUMBER (5.0'8'8'0'1' PLT(08) "	9ħ
SYMBOL (1.006.4.0.10.8HLAMBDA = NIMBER (2.0.8.4.0.1. Pt 7(07) -	8.4 0.50
SYMBOL (4.0.8.4.0.10.8HH0 =	C1 ::
CALL NUMBER (5-0-6-4-0-1- PLIVIO) - 0-0 - 3 /	56
NUMBER (2.0.6.0.0.1. PLT(12) .	58
CALL SYMBOL (4.0/8.0/0.10/8HH1) = 10.0/0/8) CALL NUMBER (5.0/8.0/0.1/2.PLT(11) / 0.0 / 3 )	40
100	42
10 CALL SYMBOL (7.0'6.8'0'1'18HEXTRAORUINARY MODE:0'0'18)	99
11 CALL SYMBOL (7.0'8.8'0'113HORDINARY MOUF!0.0'13)	69
1	
ENTRY CALCOS(LL,X,Y)	
CALL PLOT(17.5/5/1-3)	ħL

	1
Y(11)=X(11)=A=141=9/18u= X(11)=AR=SIN(Y(11))	
600 Y(II)=AR*CUS(Y(II))	
CALL PKAM(X+Y+LL+XMINI+YMINI+XMAXI+YMAXI+110++5.)	87 01.
IF(LVAL.NE.1) KET.HN  CALL AXIS(0.eu.elh1010.0.e.0.e. X(LL+2) )  CALL AXIS(0.eu.elh e 10 4.090.0.e. Y(LL+2) )	96
IC=201	101
00 300 I=1,IC X(1)=6378.*SIN(PH;) Y(1)=6378.*CUS(PH;) 300 PHI=PHI+,U3141796	107
CALL PRAMIX.Y.IC.XMIN1.YMIN1.XMAX1.YMAX1.105.)	114
CALL LINE(X,Y,IC,1,0,0) KETURN	116
ENTRY CALCOL	
LVAL E. 1.	
CALL PLOTS(PLDAT(1):350 )  CALL PLOTS(PLDAT(1):350 )	122 124
CALL PLOT(20.,0.5,-3) RETURN	124
ENTRY CALCO2	
CALL PLOT(15,00,0-3) CALL PLOT(0,0,999) RETURN	12a 131
ENTRY CALCOS	
CALL PLOT ( -17.5 , -5.0 , -3) LVAL = LVAL + 1	134
RETURN	

NSE (3002) 1 SOA(	DENS0004	
CUMMON / KELT / DU , SOA , LB		
CUMMON /DATA/ RMAX(19): EN: DIADRE UNDIE DIADRE	DENSUBTU DENSUBTU DENSUBTS	
COMMON /HBANK1/ MOPUER(7): YOL11). YOL11): SCR(260). COMMON / KBLK1 / STZMS : HPKIME : PKD <sub>E</sub> LN : AMBNL : HO	DENSO014	
0.01446400	NENSn015 NENSn015	
RAD = 6.378 PLSMAX = 2.0		
K = Y0(1) TH = Y0(2)		
AMBUA = AMBOL * PPEKD		
SNLAM1 = SIN( AMBUA ) SNLAM2 = SNLAM1 * CNLAM1 SNLAM3 = SNLAM2 * CNLAM1	· · · · · · · · · · · · · · · · · · ·	
SNTH1 = SIN( TH ) SNTH2 = SNTH1 * SFTH1 SNTH3 = SNIHZ * SFTH1		
CSTH1 = COS( TH )		
INTH! = JAN( TH ) INTHE = INTHE * THEFT	<b>5</b>	
SISL = SNIH1 / SriLAM1		
ZMI = SGRI ( 4.0 - 5.0 * SNIHZ ) ZMZ = SGRI ( 4.0 - 5.0 * SNIHZ ) ZM3 = ZM2 * SNIH3 ZM4 = ZM1 * SNIH3	7	
= ZM3 / H0 * ZM5		
DIEF = 1.0 - (KAU / K) * SISL * STSL TWO = 2.0 / INIH1 DIHETA = DIEF * TUO / ( 1.0 + TWO * 1WO ) THETA1 = TH + DIHETA		

CALCULATE ELECTROM DENSITY OF F-KEGION -ENF-

W1 = (R - 6728,) / 50.0

:

σ

:

"1 - EAP(-W1)   - EXP(-W1)   - EXP(-W1)   - 6476.78   - 6476.78   - 22402XDR44.970 - 22402X		UENS - EFN SOURCE STATEMELT - IFM(S) -			a.	PAGE
			•			
CALCILLATE ELECTRON DENSITY OF EXUSAMERS. = Finy = 12		= 0.5 * ( 1.0 = w1 = 2.7F5 * EyP(f17)	10			
CALCILLATE ELECTROD DENSITY OF EXUS-MERGFRY-   CALCILLATE ELECTROD DENSITY OF EXUS-MERGFRY-   CALCILLATE   CHARA-/TOL(1) ***   CALCILLATE   CHARA-/TOL(1) ***   CALCILLATE   CALCILATE	ن دن	= -0.01 * ( 1.0 - EXP(-W1) ) *	1			
2X	) U (	ELECTRON DENSITY OF EXUSPHERE	•			: :
U.Z.O.   U	j	= 6878.0 * ( 1.0	Ŋ			
1 - ZAVIDSOAS) 1 - ZAVIDSOAS) 1 - ZAVIDSOAS) 1 - ZAVIDSOAS) 1 - ZAVIDSOAS 2 - ZAVIDSOA		NXK = (68/8-/10(1))**Z NXK = S@KI(.9788*FXP(-ZX/60.540)+.U	;			
ERM = ERM = * (1.5.59L * A * EMS( TH 1.5.70/956.) * 1.5620.)     DEMMIN =55EM/CEXA************************************		1 -ZX/1U56.57) FNXK = 4.0 * ENXO	<del>د</del>			
1 / Zeby-9k-KP(-ZX/Zeb-9R+*OUR)/1056*3*Ex0(-ZX/1056*3)) 17 18 11 ( Zeby-9k-KP/-ZX/Zeb-9R+*OUR)/1056*3*Ex0(-ZX/1056*3)) 17 18 11 ( INNN) = 1.6-59 2 - e.NRR / RPERO		ENX. = ENXR * ( 1.459E 3 * ABS(.TH.=.1.5707963 ) + 16620 )	:		1	
I = I = I = I = I = I = I = I = I = I		1 /265.96*EXP(=ZX/ZE5.98)-4.010/1056.3*Exp(=ZX/1056.3)	17			
40 FGIONE ENKYLINGTON.  ENK = EIN * FACTOR  TENNAR = UFIXINR*FACTOR - ENX*Z**(TOLI)-7478*)/5u0.**?  UENARDE = UFIXINR*FACTOR - ENX*Z**(TOLI)-7478*)/5u0.**?  UENARDE = UFIXINR*FACTOR - ENX*Z**(TOLI)-7478*)/5u0.**?  UENARDE = UFIXINR*FACTOR - ENX*Z**(TOLI)-7478*)/5u0.**?  CALCULATE UFIXINTYES OF ELECTHON UENSITY  FAKEAC = PACLON/FN**(SIZMF/ZAS)  FACTOR = CONTON + ENX*Z**(TOLI) + FACTOR + EXA*Z**(TOLI) + FACTOR + EXA*Z**		[JENXI]] = 1.0539E 3 * ENXK / KPER] IF(Y0(1)=737R+) 4U,41.41				
TENNON = DENIALDR*FARION = LANX2**(YO(1)-777A*)/500***2	Ť		2			
CALCULATE DEMIVATIVES OF ELECTHON DENSITY  PKFAZC = PKUELN/FN, (SIZMS/ZMS)  FRACIN = PKFRAC = FAPLIN  T3.1 = EMILAL  T3.1 = EMILAL  T3.1 = EMILAL  T4.1 + COSTACL  TA.2 + COSTACL  TA.3 + COSTACL  TA.3 + COSTACL  TA.3 + COSTACL  TA.4 + COSTACL  TA.5 + COST	1		: : !			
PKFKKC = PKUELN/EN*(SIZMS/ZNS) FRACIN = FKFRAC * rAPI=(D1S/H)**2)  CDDN = -2.*U1S/H**2 * FRACIN  131 = EN/(11+FRACIN)*UFUN/(11+H*/JA,1(TH_TAL1)**2)  CNONC = COS(TO(2))  ONDI = -CTOZ/ANS/CVO2)*(DENXDI +EN/(11+FRACIN)*UFUN/(1.+.25*TAN)  1 HETA1)**2**Y0(1)  118 DND = -CTOZ/ANS/CVO2)*(DENXDI +EN/(11+FRACIN)*UFUN/(1.+.25*TAN)  118 DND = -CTOZ/ANS/CVO2)*(DENXDI +EN/(11+FRACIN)*UFUN/(1.+.25*TAN)  118 DND = -CTOZ/ANS/CVO2)*(DENXDI +EN/(11+FRACIN)*UFUN/(1.+.25*TAN)  118 DND = -CTOZ/ANS/CVO2)*(D 12  116 D15 .CT .U1SMAX ) GO TO 12  117 [LB .CT .Z996 ) GO TO 12  118 LB + 1  DULLB = U1 S  COAM = COS(ANADA ) **2  SIAMS = SIN (AMADA ) **2  SOA(LB) = .005 CYC(2)	<b>0</b> 0 0					
DFDN = -2.*UIS/H*** * FRALIN   131   25   25   25   26   26   26   26   26	ا د					
### CONTINUE    CPUN = -2.*UIS/H*** * FRACIN   CLAM***   CLAM**   CLAM***	ں ں		7			
CONDK = DENFUR + DE.XDK + 131  CONDK = DENFUR + DE.XDK + 131  CONDK = COSYMOL2)  1 THETA1)**2)**YO(2)**(DENXDI +EN/(1.+FPACIN)*DEUN/(1.+.25*TAN)(  27  118 DND1 = -CTOOLASSICVOL2)**TO(1)  118 DND2 = YO(2)*57.29  3 FORMAT ( 1H *4PEID:1.2PEIL2.3:IPAEI1.3 )  IF( DIS *0T * UISMAX ) 60 TO 12  IF( DIS *0T * UISMAX ) 60 TO 12  IF( LB *0T * 2996 ) 60 TO 12  IF( LB *0T * 29		= -2.*UIS/H**p * FRACIN : EN/11.+FRACIN)*UFDNK(1.+4./1A.1	25			
DNDI = -CTOCZABS(CVO2)*(DENXDT +En/(1.+FPACIN)*DFUN/(1.+.25*TAN) 27  118 DNDI = -CTOCZABS(CVO2)*(DENXDT +En/(1.+FPACIN)*DFUN/(1.+.25*TAN) 27  3 FORMAT ( 1H '4PF1>-1.2PF12.3*1PAE11.3 )  1F( DIS .GT . DISMAX ) GO TO 12  1F( DIS .GT . DISMAX ) GO TO 12  1F( DIS .GT . DISMAX ) GO TO 12  1F( LB .GT . 2996 ) GO TO 12  1F( LB . 2996 ) GO T		= UENFUR + DEFXDR + [3] = (05(Y0(2))	96			
118 DNDF= 0.  AY2 = Y0(2)*57*29  3 FORMAT ( 1H , 4PE12-1.72PE12-3.1PAE11.3 )  IF ( D1S . of . D1SMAx ) 60 TO 12  IF ( LB = LB + 1  LB = LB + 1  DD(LB) = UIS  COBAMBDA ) **2  SIAMS = COS(AMMDA)   **2  SIAMS = SIN( AMBO ) **2  SIAMS = SIN( AMBO ) **2  SIAMS = SIN( AMBO ) **2  SIAMS = SORT(1.33335-C1AMS)  SI = SORT(1.33335-C1AMS)  SI = SORT(1.33335-C1AMS)  SI = SORT(1.33335-C1AMS)  I ( COS(YO(2) ) + CI J J / J / J ** J / J / J ** J / J ** J / J /		= -C102-3-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	2 2			
3 FORMAT ( 1H '4FEI>-1'2PEI2-3'1PAEI1.3 )  IF ( DIS -6T . 2996 ) 60 TO 12  IF ( LB .6T . 2996 ) 60 TO 12  IF ( LB .6T . 2996 ) 60 TO 12  IF ( LB .6T . 2996 ) 60 TO 12  I	116	0. Yu(2)*5	j			
IF( DIS . LoT. DISMAX ) GO TO 12  IF( LB . cst. 2996 ) GO TO 12  LB = LB + 1  DU(LB) = DIS  COAM = COS(AMUDA)  SIAMS = SIN( AMUDA )**2  SL = SORT(1.3333-C1AMS)  SL = SORT(1.3333-C1AMS)  SL = SORT(1.3333-C1AMS)  SL = SORT(1.3333-C1AMS)  SOA(LB) = **866U254/C1AMS}  SOA(LB) = **866U254/C1AMS}  1 ( COS(TO(2) ) + CL J J/3* ) **RAU  1 ( COS(TO(2) ) + CL J J/3* ) **RAU  RETURN  END  PENSOR?	į Į	FORMAT ( 1H .44PE1>.1.2PE12.3.1PAE11.				-
IF ( DIS . 61 · 61 · 62 · 63 · 64 · 64 · 65 · 64 · 65 · 64 · 65 · 64 · 65 · 64 · 65 · 65	, , ,				!	The same of the sa
LB = LB + 1  DU(LB) = UIS  COAM = COS(AMUDA)  SIAMS = SIM (AMUDA) +*2  SLAMS = SIM (AMUDA) +*2  SL = SORT(1.33335-c1AMS)  SI = SORT(1.33335-c1AMS)  SI = SORT(1.33335-c1AMS)  SOA(LB) = BOGNUSSH/CIAMS*(COAM*SL-COS(YO(2)) **ST+ ALOG( (COAM+SL)/  1 (COS(YO(2)) + cl) 1/3* )*RAU  12 CUNTINUL  RETURN  FRUCH		DIS .6T. DISMAX ) LB .6T. 2998 )		:		The state of the s
COM	<b>,</b>	L8 = L8 + 1				
SIAMS = SLM AMBDA )**?  SL = SQRT(1.35333-CIAMS)  SL = SQRT(1.35333-CIAMS)  SOA(LB ) = SGEGU254/CIAMS*(COAM*SL-COS(YO(2) )*ST+ ALOG( (COAM*SL)/  L (COS(YO(2) ) + CL ) 1/3* )*RAD  12 CUNIINUL  RETURN  FRIUND		3.7				
ST = SQHT(11,3333-CIN(YO(2))**2)  SOA(LB) = 866U254/CIAMS+(COAM*SL-COS(YO(2))**ST+ ALOG( (COAM+SL)/  1 (COS(YU(2)) + CI) 1/3* )*RAU  12 CUNIINUL  RETURN  END  PENSOR?		ž 11	80 K			
1 ( COS(YU(2) ) + cl. ) 1/3. )*RAD 12 CUNIINUE RETURN END RESORRE		= SQRT(1+33333=c1N(YO(2))+*2 )	0 17	4.1		
12 CUNTINUE 42 43 ELURN ELURN PENSONA7	•					
CONTINUE REIURN END			42			
	12	CONTINUE RETURN				

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SUBMOUTINE FIELD	V 20014 014 V 014		47.57.5P.025Y3L	راد <u>۲</u>	FIELOUGS	ıδ				
COMMON/EXPLD/DACTIRED COMMON /DATA/ RMAX.	RMIN	-	IN STEEL	PMAX	FIELDON	<b>±</b>		•		
-NIMO	PKNI	PELCPH	AO.	90.	FIEL0005	5				•
	THEIAD	Prilus	PLUS.	NPOWFK.	FIELNUM	9				
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the state of the s	DIADI	יאטייט	E MU	PTYSOK	FIFLUUUB	96				
1		10	Ï	124500	FIELOUO9	6				
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COMMON /HBANK 1/ MOKDER	PER . NO	•	H HBOOO	HBALLK!	NOEG: FIELDO13	2				
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TO THE PROPERTY OF THE PROPERT	G D C B C B C B C B C B C B C B C B C B C	ີ			FIEL0015				1	
STATE OF THE PARTY	24. A. F./3.	THE TANK	T. B. S. BMOD & AKG. YOF	6. YOF	FIFL0016	9				
					FIEL0017	17				
2++0++C++T-1T4 OOT					FIFL 0018	90				
					F1F1 0019	6				
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103 DFHUR=-3.*FH/Y0(1)					FIELDOSS	10				
					2.00.131.2	J ~				
_						2 5				
_		i			001111	,				
	(5) *5) ZDM	ANTR			FIELOUZO					
107 SP2=1COSPSI**2					トルにしいりどの	é				
IF (SP2 .LE. U.U ) S	Sr2 = 0.0				i	,			1	
YO45 = S* YO(+)					F1EL0027	- 6				
YUSC = C* YU(5)					FIELOUZB	20				
SINPSI = SIGN (SORT (SPZ) (YOSC*2.	(SP2)+(Y05)	3*2 YO45))	<u> </u>		FIELOU	<u>ر</u>	2			
_					FIELOUSO	30				
UCPUT = F2T * COSPCI + (Y05C - Y045*2.) / UNMNTR	+ (Y05c -	104S*5.)/	UNMITE		FIELNO31	31				
DCPLP=0.		i		•	FIEL0032	2				
F1P=C0SPS1/YSQUAR					FIELOUSS	33				
druk(h) CX-XLXWNC/O** OHIO Side O	0(4)*616				FIFLOO34	<b>+</b>				
OCPUYORS/INMANIR-YOLD) *FIP	) *F1P				FIEL0035	35				
OCD: VAIL YO (A) #F1P	i				FIFLOU36	36				
COCKOTH-YO (5) *DCPD+/YSQUAK+# . /DNMNTA	YSOUAK+# ./	DAMNTA*C/F1	1-		FIEL0037	77				
/// UCUC#! UCUC#! // // UCUC#! // UCUC#! INTO // UCUC#! UCUC#! // UCUC#! // UCUC#! // UCUC#! // UCUC#! //	(1+1)CPD.(+)C		ISANIS/(2**TUPNIS	PSI	FIELOUSB	98				
			!		FIEL0039	96				
250.75					TIEL DOM	04				

Dimension A (13.1) to (13.5)   Dimension A	SUBROUTINE TO COMPLIFE POWER LOSS SUBROUTINE POWERL	POWER LOSS			POWENON2 POWENON5 POWENON5	
COMMON / CRSY CASA	DIMENSION A(3,3), th(3,0)				POWE 0007	
MANIA   PANIA   PANI	ATA/		TMINE	PMAX	POWEDDIB	
NUMBER   N			PLUS	NPOWER	POWE0010	
DNDR,   DNDIT,   DNDP1,   DN				* Zie ()	POWEN011	
SIMPST   LIETURE   DEPOTE   DEPOTE   DEPOTE	JNG .			COSPSI.	POWE 0013	
DCPDY2,   DCPDY3,   SP2, EMUINT, FMIS, POWED015	OUNTO	H-HO	DCPDIA	DCPDY14	POWE 0014	
СОМНОИ / ИВВАИК / МОКОВ Р. РОМЕЙО В НАВАКК / ИОСВО РОМЕЙО В БЕЛИКР / БЛИРЕТ В ТОТІТІ / ТОТІТІ / ТОТІТІ / ТОМЕДО В РОМЕЙО В СОМНОИ / РОМЬО В РОМЕЙО В БЕЛИКР / ТОТІТІ / ТОТІТІ / ТОМЕДО В РОМЕЙО В РОМЕМ	DCPU	S.	EMUINT	EMUS	POWE 0015	
COMMON / POWLOS, CASA, Y: DMDA: DMD1: MA(260)POWE0019 COMMON / POWLOS; CASA, Y: DMDA: DMD1: DMD1	10.4400	JUN P	1	į	POWE 017	
COMMON / POWLOS / CASA Y PUNDR DMDS I DMS I	NOWWOO			İ	0) POWEDD18	
DMINITY	COMMON /POWLOS/	<b>&gt;</b> (			POWE 0019	
COMMON CKESN CREATER   CANDUS   COMMON CKESN CREATER   CANDUS   COMMON CKESN CREATER   CANDUS   COMMON CKESN CREATER   CANDUS   COMMON CKESN CREATER   CANDUS   COMMON CKESN CREATER   CANDUS   COMMON CKELLO COLOR CODE   COMMON CKELLO COLOR CODE   COMMON CKELLO COLOR CODE   COMMON CKELLO COLOR COLOR COLOR CREATER   COMMON CKELLO COLOR CREATER   COMMON CKELLO COLOR CREATER   COMMON CKELLO COLOR CREATER   COMMON CKELLO COLOR CREATER   COMMON CKELLO COLOR CREATER   COMMON CKELLO COLOR CREATER   COLOR CREATER		DMDIZE		۲	POWEOU21	
COMMON / CKSK/ C*RCT*S*RST*Z*EM*TERM?*RMOD**RAG*YO6 POWE NO25 COMMON/CASS/YSQUAR**DECPUP*DFHU2*EIT*DNMYR*LUEL2\$ COMMON/CASS/YSQUAR**DECY2T*DZSYZT*DNMYR*LUEL2\$ COMMON/CASS/YSQUAR**DECY2T*DZSYZT*DNMYR*LUEL2\$ COMMON/CASS/YSQUAR**DECY2T*DZSYZT*DNMYR*LUEL2\$ COMMON/CASS/YSQUAR**DECY2T*DZSYZT*DZSYZP POWE NO27  YZ=Y**Z  TERMCI = TERM*CI  TOPE NO29  POWE NO29  POWE NO37  POWE NO35  POWE NO35  POWE NO35  POWE NO37  POWE NO41  FICHETAGZST*CASSZ  FHCSPZ=Z**FHU3D**COST*COST*COST*COST*COST*COST*COST*COS	2	OMILIST		1	POWE 0022	
COMMON/CAUSS/YSUUAR: DCPDR.DCPUP.DF.HUP.E.T.T.DNNNTR.LIEL2S  COMMON/CAUSS/YSUUAR: DCPDR.DCPUP.DF.HUP.E.T.T.DNNNTR.LIEL2S  COMMON/CAUSSYTR.D2CY2T.D2CY3T.D2CY3PP DOWE 0025  EQUITALENCE(YE(1)1.x0(1))  COMPUTE MISCELLANEAUS VARIABLES  COMPUTE MISCELLANEAUS VARIABLES  COMPUTE MISCELLANEAUS VARIABLES  COMPUTE MISCELLANEAUS POWE 0029  Y2=1/4*2  AA2 = EMD4*2  AA2 = EMD4*2  AA2 = EMD4*2  TERM#C1 = TERM#C1  COSES = COSESI**2  AA2 = EMD4*2  TERM#C1 = TERM#C1  POWE 0035  ENDAZC = EN/AA2C1  TERM#C1 = POWE 0035  ENDAZC = EN/AA2C1  TO ETHE TAO. SOURCE  ENDAZC = AFH *COSES  FH CSPS = 2*FH *COSES  TERM#COSES  TERM#COSES  SIDOSINICO  COPOCCOS (FO)  POWE 0045  POWE 0045  POWE 0045  SIDOSINICO  SIDOSINICO  COPOCCOS (FO)  POWE 0045  POWE 0045  TO ETHE TAO. SOURCE  SIDOSINICO  SIDOSINICO  SIDOSINICO  POWE 0045  POWE 0045  POWE 0045  POWE 0045  TO ETHE TAO. SOURCE  SIDOSINICO  SIDOSINICO  SIDOSINICO  SIDOSINICO  SIDOSINICO  POWE 0045  POWE 0045  POWE 0045  POWE 0045  SIDOSINICO  SIDOSINICO  SIDOSINICO  SIDOSINICO  SIDOSINICO  POWE 0045  POWE	COMMON ACKSRA CARCTAS	, RST , Z , EM , TEKM , TER	MOPRMODINANG	• Y06	POWE 0023	
COMMON/EXFLUXUZCYIP.DZSYIR.DZSYZT.DZSYZT.DZCY3P.DZSY3P POWE 0025  COMPUTE MISCELLANEAUS VARIABLES  COMPUTE MISCELLANEAUS POWE 0027  TERMAT = TEKM*CI  COSPSZ = COSPSI**2  AA2 = EMD**2  AA2 = FMSACZ = POWE 0031  POWE 0035  ENGRADZ = EMD**2  ENGRADZ = EMD**2  FMCAPZ = **F***COSPSZ  EMRADZ = EMD**2  FMCAPZ = **F***COSPSZ  EMRADZ = EMD**2  FMCAPZ = **F***COSPSZ  EMRADZ = EMD**2  FMCAPZ = **F***COSPSZ  EMCAPZ = **F***COSPSZ  EMCAPZ = **F***COSPSZ  FMCAPZ = **F***COSPSZ  EMCAPZ = **F***COSPSZ  FMCAPZ = **F***COSPZ  FM	COMMON/GAUSS/YSWUAR D	CPDR DCPUP DEHUP F	LTLDNMNTRLDE		POWE 0024	
COMPUTE MISCELLANE (YP(1))*YOLTJ)         POWE 0027           COMPUTE MISCELLANE (YP(1))*YOLTJ)         POWE 0027           Y2=Y**E         POWE 0029           Y2=Y**E         POWE 0029           Y2=Y**E         POWE 0029           Y2=Y**E         POWE 0029           Y2=Y**E         POWE 0023           Y2=Y**E         POWE 0031           Y2=X**COSFS1         POWE 0035           Y2=X**COSFS2         POWE 0042           Y2=X**COSFS2         POWE 0043           Y2=X**COSFS2         POWE 0044           Y2=X**X**COSFS2         POWE 0044           Y2=X**X**COSFS2         POWE 0044           Y2=X**X**X**COSFS2         POWE 0044           Y2=X**X**X**X**X**X**X**X**X**X**X**X**X**	COMMON/EXFLU/U2CY1P+D	ZSY1R.D2CY2T.D2SY2	T,U2CY3P,D2S	Y3P	POWE 0025	
COMPUTE MISCELLANEAUS VARIABLES  COMPUTE MISCELLANEAUS VARIABLES  POWERD	EQUIVALENCE (YP(1) + YO				POWE0027	
Y2=T**2  Y2=T**2  Y2=T**2  Y2=T**2  Y2=T**2  Y2=T**2  Y2=T**2  Y2=T**2  AA2 = END**2  AA2 = END**2  AA2 = END**2  Y2=T**2  AA2 = END**2  Y3=T**2  AA2 = END**2  Y3=T**2  POWEND32  POWEND33  Y4=T**2  POWEND32  POWEND34  AA21 = AA2**1  POWEND35  POWEND35  FACT = AA2**1  POWEND35  FACT = ENTAARC1  XTEM=ENDA2C = ENTAARC1  XTEM=ENDA2C = ENTAARC1  XTEM=ENDA2C = ENTAARC1  XTEM=ENDA2C = ENTAARC1  Y2=T**2  POWEND35  POWEND35  POWEND35  POWEND35  POWEND41  Y2=T**2  Y2=	SUPPLIES MISCELL ANE SUS	VARIARI FS			POWE 0028	20.00
Y2=Y**2  TERMC1 = TERM*C1  CGSPS2 = CGSPS1**2  AA2 = END**2  YC = Y2*CGSPS1  YC = Y2*CGSPS1  YC = Y2*CGSPS1  AA2 = END**2  AA2 = AA2 = POWE 0 0 3 3  POWE 0 0 3 5  POWE 0 0 3 5  POWE 0 0 3 7  EMRAD2 = END **2  FOWE 0 0 3 7  EMRAD2 = END **2  FOWE 0 0 3 7  FOWE 0 0 4 3  FOW					POWE0029	
TERMCI = TERM*CI  COSPS2 = COSPSI**2  AA2 = EMD**2  AA2 = AA2*CI  AA3 = AA2*CI  AA3 = AA2*CI  AA3 = AA2*CI  AA3 = AA2*CI  AA3 = AA2*CI  AA3 = AA2*CI  AA3 = AA3*CI  AA3 =					POWE 0030	
COSPSZ = COSPSI**2  AA2 = EMD**2  YC = XA2*C1  AA2 = EMD**2  AA2 = EMD**2  FMD**2  AA2 = EMD**2  FOWEOU35  POWEOU35  ENDAZC = EN/AA2C1  ENDAZC = EN/AA2C1  ENDAZC = EN/AA2C1  ENDAZC = EN/AA2C1  FOWEOU35  ENDAZC = EN/AA2C1  FOWEOU35  FHCSD2=2*FH*COSPST  FHCSD3  FH	TERMC1 =				POWER031	
AAA2 = ENU**2  AAA2 = ENU**2  AAA2 = AAA2	COSPS2 = COSPSI**2				POWF 0033	
AA2C1 = AA2C1  AA2C1 = AA2C1  AA2C1 = AA2C1  ENDA2C = EN/AA2C1  POWE 0.037  FERMAD2=EMRAD2=EMFO.036  FERMAD2=EMRAD2=EMFO.037  FOR THE AGO TO	<u>"</u> 1				POWE 034	
ENDA2C = EN/AA2(1)  XTEKM=ENDA2C (2.*E.*U)  XTEKM=ENDA2C (2.*E.*U)  XTEKM=ENDA2C (2.*E.*U)  XTEKM=ENDA2C (2.*E.*U)  XTEKM=ENDA2C (2.*E.*U)  XTEKM=ENDA2C (2.*E.*U)  POWE 0.037  POWE 0.039  POWE 0.039  POWE 0.039  POWE 0.041  POWE 0.041  POWE 0.041  POWE 0.042  POWE 0.043  POWE 0.043  POWE 0.043  POWE 0.043  POWE 0.044  POWE 0.045  POWE 0.051  POWE 0.051  POWE 0.051  POWE 0.053  POWE 0.053  POWE 0.053  POWE 0.053  POWE 0.053  POWE 0.055	12				POWE0035	
XTERM=ENDA2C/(2**E,U)  KEMAD2=EMRAD*E  EMRAD2=EMRAD*E  FHEROPS=EMRAD*E  FHEROPS=EMRAD*E  FOWE 0039  FHEROPS=2*FH*COSPST  FOR END ED EMRAD ED POWE 0039  FHEROPS=2*FH*COSPST  FOR END ED EMRAD ED POWE 0040  FOR ED EMRAD ED EMPE 0050  FOR ED EMPE 0050  FOWE 0051  FOWE 0055	ENDASC = EN/AA2C1				POWE 0036	
EMRAD2=EMRAD**2 FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=2**FH*COSP5T FHCSP2=3*FH*COSP5T FHCSP3+2*FH*COSP5T FHCSP3+3*FH*COSP5T FHCSP3	XTERM=ENDA2C/(2.*ENU)				POWE0039	
FHCSPZ=2************************************	EMRAD2=EMRAD**2				POWE0039	
F.CF.C.   POWE NOW   1					POWE 0040	
TOTHETAO/57,2957795 POWE0042 POWE0043 PO=PHIO/57,2957795 POWE0043 PO=PHIO/57,2957795 POWE0043 POWE0045 COPO=COS(FO) POWE0045 POWE0045 COTO=COS(TO) POWE0049 POWE0049 POWE0049 POWE0049 POWE0049 POWE0049 POWE0049 POWE0049 POWE0051 SIPPLESIN(YP(3)) SIPPLESIN(YP(3)) POWE0051 POWE0051 POWE0051 POWE0051 POWE0051 POWE0051 POWE0051 POWE0051 POWE0051 POWE0055 1+COTO*C)					POWE0041	
PO=PHIO/57.2957795 PO=PHIO/57.2957795 POWEOU45 SIPO=SIN(PO) COPO=COS(FO) POWEOU45 POWEOU45 POWEOU45 POWEOU46 POWEOU47 POWEOU47 POWEOU49 POWEOU49 POWEOU49 POWEOU49 POWEOU51 SIPO=SIN(YP(3)) SIPO=SIN(YP(3)) SIPO=SIN(YP(3)) POWEOU51 POWEOU51 POWEOU51 POWEOU51 POWEOU51 POWEOU51 POWEOU51 POWEOU51 POWEOU55 POWEOU55 POWEOU55 POWEOU55 POWEOU55 POWEOU55 POWEOU55 POWEOU55					DOME DOME	
SID=SIN(PQ) COPO=COS(PO) SID=SIN(IQ) FOWEGOU45 SID=SIN(IQ) FOWEGOU47 FOOECOS(TO) FOWEGOU47 FOOECOS(TP(3)) SID=SIN(IQ) FOWEGOU47 FOOECOS(TP(3)) SID=SIN(IQ) FOWEGOU49 FOWEGOU49 FOWEGOU49 FOWEGOU49 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU51 FOWEGOU55 FOWEGOU55 FOWEGOU55 FOWEGOU55 FOWEGOU55	PO=PHIO/57.2957795				POWF 0044	<b>y</b>
COPECUSIFOR  SITO=SIN(IO)  COTO=COS(TO)  COTO=COS(TO)  ROZ=RO**2  ROZ=RO**2  ROMEDGE = 1  COPECOS(TP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  SIPM=SIN(YP(3))  POWENDS  POWENDS  POWENDS  1+COTO*C)  POWENDS  PO	SIPO=SIN(PO)				POWE0045	7
COTO=COS(TO)  RO2=RO**2  RO2=RO**2  RO2=RO**2  ROPEGOUT  ROPEGOUT  ROPEGOUT  ROPEGOUT  SIPPESIN(YP(3))  SIPPESIN(YP(3))  SOPMP=COS(YP(3))  ROPEGOUT  ROPEGOU	COPOLICOS (PO)				POWE 0046	8
ROZ=RO##2  MUFLAG = 1  FOWEGOIGH	010=000				POWE 0047	σ
MUFLAG = 1  COP=COS(YP(3))  SIP=SIN(YP(3))  SIP=SIN(YP(3))  SIP=SIN(YP(3))  SIPMEDSIN(YP(3))  SIPMEDSIN(YP(3))  POWEND52  COPMP=COS(YP(3)-PQ)  POWEND53  POWEND54  POWEND54  POWEND55  1+COTO*C))  POWEND55  POWEND55  POWEND55  POWEND55	R02=R0**2				POWEDD48	
COP=COS(YP(3))  SIP=SIN(YP(3))  SIP=SIN(YP(3))  SIPMP=SIN(YP(3)-PO)  COPMP=COS(YP(3)-PO)  POWEOUS3  POWEOUS3  POWEOUS4  POWEOUS5  1+COTO*C))  POWEOUS5  POWEOUS5	ļ.				POWEDURY	10
SIP=SIN(YP(3))  SIPMP=SIN(YP(3)-PO)  COPMP=COS(YP(3)-PO)  COPMP=COS(YP(3)-PO)  POWEOD53  1+COTO*C))  POWEOD55  POWEOD55  RP=SORT(RP2)	- 1				POWE 0051	13
POWE0053 COPMP=COS(YP(3)-PU) RP2= (RO2+YP(1)**2-2*0*YP(1)*RO*(SITO*S*COPMP POWE0054 1+COTO*C) POWE0055 RP=SORI(RP2)	SIPESIN(YP(S))				POWE 0052	10
ROZ= (ROZ+YP(1)**2-2*0*YP(1)*RO*(SITO*S*COPMP POWEOO59 1+COTO*C)) POWEOO55 RP=SGRI(RP2)	CODMD=COC(YP(3)-PO)				POWE0053	15
1+C0TO*C)) POWE0055 RP=SGRT(RP2)	E LOCAL	-2.0*YP(1)*RO*(SIT	D*S*COPMP		POWE 0054	
CONTROL	1+C0T0*C				POWEROSS POWEROSS	a
	2 RP=SORT(RP2)				POWE 0050	

10   COPPER STATE   COPPER STATE   DESCRIPTION	FOWER - FFN SOURCE STATEMENT - IFN(S) -		
INTERPRETATE   INTERPRETATE   DONE ORGONAL			
DNETECT   DNETECT   DNETECT   DNETECT   DNETECT	COPP=(RST*COP-RU*S+10*COPO)/RP/SITP		
DOMERONG	DRPUR=(YP(1)-RO*(S;10*S*CUPMP+CUTU*	POWE 0060	
ALL		POWE 0061	
ALLA   ENGINE   ALLA   ENGINE		POWE DOKE	
A (1.2.) = TESTS HOWS STEWP         POWEGOGS           A (2.2.) = TESTS STOWN         POWEGOGS           A (2.2.) = TESTS STOWN         POWEGOGS           A (2.2.) = TESTS STOWN         POWEGOGS           B (2.2.) = TESTS STOWN         POWEGOGS           B (2.2.) = TESTS STOWN         POWEGOGS           B (2.2.) = TESTS STOWN         POWEGOGS           B (2.2.) = TESTS STOWN         POWEGOGS           B (2.2.) = TESTS STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE STOWN         POWEGOGS           D DONE S		アンを行っている	
A (12.2) = 2.5.5.CP         DOME006           A (12.2) = 2.5.5.CP         DOME006           A (12.2) = 2.5.TF (12.CP)         DOME006           A (13.1) = C.         DOME007           A (13.1) = C.         DOME007           B (12.1) = C.         DOME007           B (13.1) = C.         DOME007           B (12.1) = C.         DOME007           DEDMEPALL I. I.         DOME007           DEDMEPALL I. I.         DOME007           DEDMEPALL I. I.         DOME007           DEDMEPALL I. I.         DOME007           DEDMEPALL I. I. I.         DOME007           DEDMEPAL I. I. I.         DOME007           DEDMEPAL I. I. I.         DOME007           DEDMEPAL I. I. I. I. I. I. I. I. I. I. I. I. I.	A(1,3)=RS1+HO+SITO+SIPMP	POWENOS	
ALG.2.31=CRT.45.2P         POWE COT           ALG.2.31=ERTAS.1P         POWE COT           ALG.2.31=CRT.45.2P         POWE COT           ALG.2.31=ERTAS.2P         POWE COT           ALG.2.31=CRT         POWE COT           BLA1.13=CRT         POWE COT           DEMPERATION OF A PARTY AND A PARTY AND A PARTY AND A PARTY AND A PARTY A	A(2,1)=S*COP	POWE0066	
A   3.1   2.6	A(2,2)=RCT*COP	POWE 0067	
A	4/2/3/=-KS/KS/F	POWEn068	
R14.21=0.0   R14.11=ERC   R14	A(3,0)1-C	POWEROAS BOSESSAS	
B(12.1)=SIP*COPP	A(3,3)=0.0	POWE 071	
BIG2115517P\$COPP		POWE0072	
R(12.12) = CUTP   R(12.12) =	B(2.1)=SITP*COPP	POWE ng73	
RILLAD   20.0	R(3-1)=C0TP	POWED074	
CALLULAIS INVIGATED POWERONS  DEMBRE-ALIA  D		POWE 0075	
DEMYSTALL   1			
DIDRP=A(2.1) DEDRE=A(3.1) CALCULAIE INTERMEDIATE DERIVAITVES  CALCULAIE INTERMEDIATE DERIVAITVES  DEMYIR = -(FHCSP2*DCPUY1/F2*DFHUR**C*UCPDY1** (UCPDH/SINDS1/F2*DFHUR**TERMC1)- EH**2*SINDS1/F2*DFHUT**YC*UCPDY2*  LUCPDIZSINPS1/F2*DFHUT**YC*UCPDY2*  LUCPDIZSINPS1/F2*DFHUT**YC*UCPDY2*  LUCPDIZSINPS1/F2*DFHUT**YC*UCPDY3* (UCPDF/SINDS1/F2*DFHUF*YC*UCPDY) * FMRAN  DEMYIR = -U2MY1R + (UMUR*DMDY1+EM** U2MY1R + (FHCSP2/F2*DFHUF*YC*UCPDY) * FMRAN  LEM**DEMYIR**YC*UCPDY * FMRAN  CEM**DMUX**FFHUR**YC*UCPDY * FMRAN  DEAY1R = -U2MY1 + (UMUR**DMDY1+EM**DLYC**YC*UCPDY) * FMRAN  CEM**DMUX**TC**DCPUY1) * LUCPDY3**TC**DCPUY3**TC*			
CALCULAIE INTERMEDIATE DERIVATIVES  CALCULAIE INTERMEDIATE DERIVATIVES  CALCULAIE INTERMEDIATE DERIVATIVES  LUCPOLYSTENCIA  CORNING = -(FHCSP2*nCPUYJ/F2*nFHUR-YC*uCPDY1*  LUCPOLYSINESI/F2*uCSYIB/TERMC1)-  E H**2**SINPSI/F2*uCSYIB/TERMC1)-  DEMY2T=-(FHCSP2*DCDUYZ/F2*DFHUT-YC*uCPDY2*  LUCPOLYSIA-ECOSPSI-DNDI/TERMC1)-  DEMY3P=-(FHCSP2*DCFOY3/F2*DFHUP-YC*uCPDY3*  LUCPOLYSIA-SINPSI/F2*DFHUP-YC*uCPDY3*  LUCPOLYSIA-SINPSI/F2*DFHUP-YC*uCPDY3*  LUCPOLYSIA-SINPSI/F2*DFHUP-YC*uCPDY3*  LEM*UMNY1+YC*DCPUY1)/EMRAD2)/FMRAD  E H**2**SINPSI/F2*UFDY1)/EMRAD2)/FMRAD3  *(EM*UMUY1+YC*DCPUY1)/EMRAD2)/FMRAD3  *(EM*UMUY1+YC*DCPUY1)/EMRAD2)/FMRAD3  *(EM*UMUY1+F2-+YC*UCPDI)  DEAY3P=-U2MY2P-TC*DCPUY2)/EMRAD2)/FMRAD3  *(EM*UMUY2+YC*DCPUY3)/EMRAD2)/FMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD2)/FMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD2)/FMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  *(EM*UMUY3+YC*DCPUY3)/EMRAD3  DABY3 = -DMUY2+(EM*UMUY3+YC*DCPUY3)/EMRAD3  DABY3 = -DMUY4+(EM*UMUY3+YC*DCPUY3)/EMRAD3  DABY3 = -DMUY4+(EM*UMUY3+YC*DCPUY3+YC*DFUY3)/EMRAD3  DABY3 = -DMUY3+YC*DCPUY3+YC*DCPUY3+YC*DFUY3+YC*DFUY3+YC*DFUY3+YC*DFUY3+YC*D	DIRREA(201)	DOMEGODO	
CALCULAIE INTERMEDIATE DERIVATIVES  DEMYIR = - (EHCSP2*nCPUY1/F2*DFHUR-YC*UCPNY1*  (DCPDK/SINPS1/F2*USY18/IFEM  DEMY2T=-FHCSP2*nCPUY2/F2*DFHUT-YC*UCPN?*  LIGCPD1/SINPS1/F2*USY18/IFEM  DEMY2T=-FHCSP2*DCDUY2/F2*DFHUT-YC*UCPN?*  LIGCPD1/SINPS1/F2*DFHUT-YC*UCPN?*  DEMY2T=-FHCSP2*DCDUY2/F2*DFHUT-YC*UCPN?*  DEMY2T=-FHCSP2*DCDUY2/F2*DFHUT-YC*UCPN?*  LOCPDP/SINPS1/F2*DFHUP-YC*UCPN;  EH**2*SINPS1/F2*DFHUP-YC*UCPN;  FH**2*SINPS1/F2*DFHUP-YC*UCPN;  LEM*UMUY1-YC*DCPUY1)*EMRAD2/FEM  - (EM*UMUST-YC*DCPUY1)*EMRAD2/FEM  - (EM*UMUST-YC*DCPUY1)*EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY1)*EMPAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY1)*EMPAD2/FEM*ZH  - (EM*UMD7-YC*DCPUY2)/EMRAD2/FEM*ZH  - (EM*UMD7-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRAD2/FEM*ZH  - (EM*UMUST-YC*DCPUY3)/EMRADA/FEM*ZH  - (EM*ZH  -			
CALCULATE INTERMEDIATE DERIVATIVES  DZMYIR = -(FHCSP2*hCPUY1/F2*DFHUR-YC*UCPDY1*  UCPDH/SINDSI*COSFSI-UNURTERME1)-  PH**2*SINDSI*F2*USSYIR/ITEMM  DZMYZP=-(FHCSP2*DCPUYZ/F2*DFHUT-YC*UCPDY2*  LUCPDI/SINDSI*COSFSI-UNURTIEMMC1)-  EH**2*SINDSI*COSPSI-UNURTERMC1)-  DZMYZP=-(FHCSP2*DCPUYZ/F2*DFHUP-YC*UCPDY3*  UCPDH/SINDSI*COSPSI-UNURTERMC1)-  FH**2*SINDSI*COSPSI-UNURTERMC1)-  FH**2*SINDSI*COSPSI-UNURTERMC1]-  FH**2*SI	1	POSEDORI	
D2MY1R = -(FHCSP2*nCPUY1/F2*DFHuR-YC*UCPNY1*  (UCPDH/SINPSI/E2*U2SY1R)/IERM  LEH**2*SINPSI/E2*U2SY1R)/IERM  LOCAM2I=-(FHCSP2*DCDUY2/F2*DFHUT-YC*UCPNY2*  LOCAM2I=-(FHCSP2*DCDUY2/F2*DFHUT-YC*UCPNY2*  LOCAM2I=-(FHCSP2*DCPUY3/F2*DFHUT-YC*UCPNY1*  LOCAM2I=-(FHCSP2*DCPUY3/F2*DFHUP-YC*UCPNY1*  LOCAM2I=-(FHCSP2*DCPUY3/F2*DFHUR-YC*UCPNY1*C*DCY1R  -(FHCSP2/F2*DFHUR-Y2*UCPNX1*DCPUX1*C*DCY1R  -(FHCSP2/F2*DFHUR-Y2*UCPNX1*C*DCY1R  -(FHCSP2/F2*DFHUR-Y2*UCPNX1*C*DCY2Y  -(FHCSP2/F2*DFHUR-Y2*UCPNY1*C*DCY2Y  -(FHCSP2/F2*DFHUP-Y2*UCPNY1*C*DCPNY3+C*	CALCULATE INTERMEDIATE DEKIVATIVES	POWEDORS	
DEMTIK = -ITHGSPZ*NCPU11/FZ*DFHUR-"C*UCPDY1*  LUCPDN/SINDS1/FZ*DFHUR-"C*UCPDY1*  LUCPDN/SINDS1/FZ*DFHUR-"C*UCPDY2*  LUCPDN/SINDS1/FZ*DFHUT-YC*UCPDY2*  DEMY2T=-(FHGSPZ*SIDPS1/FZ*DFHUT-YC*UCPDY2*  DEMY3E=-(FHGSPZ*DCPU72/FZ*DFHUT-YC*UCPDY3*  LUCPDN/SINDS1/FZ*DFHUP-YC*UCPDY3*  LUCPDN/SINDS1/FZ*DFHUP-YC*UCPDY3*  LUCPDN/SINDS1/FZ*DFHUP-YC*UCPDY3*  LUCPDN/SINDS1/FZ*DFHUP-YC*UCPDY3*  LEM*DMUNTA-YC*DCPU71/FEMAD2*  LEM*DMUNTA-YC*DCPU71/FEMAD2*  LEM*DMUNTA-YC*DCPU71/FEMAD2*  LEM*DMUNTA-YC*DCPU71/FEMAD2*  LEM*DMUNTA-YC*DCPU73/FEMAD2*  DADY3 = -DMUY3+YC*DCPU73/FEMAD2*  DADY3 = -DMUY3+YC*DCPU73/FEMAD2*  DADY3 = -DMUY3+YC*DCPU73/FEMAD2*  DADY3 = -DMUY3+YC*DCPU73/FEMAD2*  DADY3 = -DMUY4+YC*DCPU73/FEMAD2*  DADY3 = -DMUY4+YC*DCPU73/FEMAD2*  DADY3 = -DMUY4+YC*DCPU73/FEMAD2*  DADY3 = -DMUY4+YC*DCPU73/FEMAD3*  DADY3 = -DMUY4+YC*DCPU73/FEMAD3*  DADY3 = -DMUY4+YC*DCPU73/FEMAD3*  DADY3 = -DMUY4+YC*DCPU73/FEMAD3*  DADY3 = -DMUY4+YC*DCPU74/FC*DCPU73/FEMAD3*  DADY3 = -DMUY4+YC*DCPU74/FEMAD3*  DADY3 + FEMAD3*  DADY4+YC*DCPU74/FEMAD3*  DADY4+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DADY5+YC*DCPU74/FEMAD3*  DAD		POWENDR3	
LUCPORTSINESITE CONSTITUENT ERMCI) -  LUCPORTSINESITE CONSTITUENT ERMCI) -  EHH*2#\$SINESITE CONSTITUENT ERMCI) -  ZEH*2#\$SINESITE ERDCEPT (2 CCCPD 72 +  LUCCPORTSINESITE ERDCEPT (2 CCCPD 72 +  LUCCPORTSINESITE ERDCEPT (3 F C E E E E E E E E E E E E E E E E E E	= - (FHCSP2*DCPUY1/F2*DFHDR-YC	POWEDOR4	
D2MY2T=-(FHCSP2*DCDDY2/F2*DFHUT-YC*CCPDT2* 1/LUCPDI/SINPS1*COSPC1/SINPS1-DND1/IEAMC1)- 2FH**2*SINPS1*COSPC1/SINPS1-DND1/IEAMC1)- D2MY3F=-(FHCSP2*DCDDY3/F2*DEHUP-YC*UCPDT3* 1		POWEROR5	
102PIT/SINPSIECOSPEI/SINPSI—DNDI/IERMEI)— 2FH4*2*SINPSIECOSPEI/SINPSI—DNDI/IERMEI)— D2WISPE—(FHCSP2*DCFQY3/F2*DCFUDDI/IERMEI)— 1	DOMYOTH (FECAPORDCO)YZ/F9#DEHOT#YC#D	DOMEONG	
D24Y1R= -(FHCSP2*PCCPDY3/F2*PDCT21/TERM  D24Y1R= -(FHCSP2*PCCPDY3/F2*PDCT21-DNUP/TERMC1)-  (LCPDP/SINDSI/F2*PDCT21-DNUP/TERMC1)-  E HT**2*SINPSI/F2*PDCT3-DNUP/TERMC1)-  EH**2*SINPSI/F2*PDCT3-DNUP/TERMC1)-  D24Y1R= -U2MY1R + (DMUP*DMDY1+EM * U2MY1R + (FHCSP2/F2)-FHDR*Y2*DCPDY) * PMRAD  CEM*UMUX1+YC*DCPUY1)/EMRAD2) / FMRAD  A (EM*UMUX1+YC*DCPUY1)/EMRAD2) / FMRAD  D24Y2T=-D2MY2F + (DMUP*DMDY2+EM*D2*Y2)+  CEM*UMUY2+YC*DCPUY2)/EMRAD2)/EMRAD  D24Y3P= -U2MY3P + (OMUP*DMDY3+EM * U2MY3P + (FHCSP2/F2*CHUPP)*DCPUY3+YC*DCPUY3)/EMRAD  D2AY3F= -U2MY3P + (OMUP*DMDY3+EM * U2MY3P + (EM*UMUX3+YC*DCPUY3)/EMRAD2) / FMRAD  D2AY3F= -U2MY3P + (OMUP*DFUZ*YC*UCPUP)  CEM*UMUDP*PFRUP*F2*CY*CUCPUP)  *(EM*UMUDP*PFRUP*F2*CY*CUCPUP)  *(EM*UMUX3+YC*DCPUY3)/EMRAD2) / FMRAD  DABY1 = -UMUX1+(EM*UMUX1+YC*DCPUY1)/EMRAD  DABY2 = -DMUY2+(EM*UMUX2+YC*DCPUY3)/EMRAD  DABY3 = -DMUY3+(EM*UMUY2+YC*DCPUY3)/EMRAD  DABY3 = -DMUY3+(EM*DMNY2+YC*DCPUY3)/EMRAD  DABY3 = -DMUY1+(EM*DMNY2+YC*DCPUY3)/EMRAD	L(DCPD1/SINPSI*COSP~I/SINPSI-DND1/IEA*C1)+		
D2MY3P=-(FHCSP2*DCrDY3/F2*DFHUP-YC*UCPDY3*  (UCPDY-SINDSI*COSFSI-DNUP/YERMC1)-  EH**2*SINDSI*COSFSI-DNUP/YERMC1)-  EH**2*SINDSI*COSFSI-DNUP/YERMC1)-  EH**2*SINDSI*COSFSI-DNUP/YERMC1)-  * (ER*2MURT-FHOR*F2*UCPDR,* **CPUY1+YC*PDCY1R  -(ER*2MURY-FHOR*F2*UCPDR,* **CPUY1+YC*PDCY1R  * (ER*2MURY-FHOR*F2*UCPDR,* **CPUY2+YC**UCCY2T  * (ER*2MURY-FE-YC**UCPDT)  S* (EM*2MURY-FE-YC**UCPDT)  S* (EM*2MURY-FE-YC**UCPDP)  S* (EM*2MURY-FE-YC**UCPDP)  S* (EM*2MURY-FE-YC**UCPDP)  * (EM*2MURY-FHUP-FE-YC**UCPDP)  * (EM*2MURY-FHUP-FE-YC**UCPDP)  * (EM*2MURY-FE-YC**UCPDP)  DADY2 = -DMUY2+(EM**UMUY2+YC**UCPDP)  DADY3 = -DMUY3+(EM**UMUY2+YC**UCPDP)  DADY3 = -DMUY3+(EM**UMUY2+YC**UCPDP)  DADY3 = -DMUY1-(EM**UMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY3 = -DMUY-FE-YC**UCPDP)  DADY4DMUY-FE-YC**UCPDP)  DADY5	2FH**?*SINPSI/F2*D2cY2I)/TERM	POWE 1089	
1 (UCPDY/SINDSIACOSPS1-DNUP/TERMC1)- EH**2*SINDSIACOSPS1-DNUP/TERMC1)- FH**2*SINDSIACOSPS1-DNUP/TERM  LEH**2*SINDSIACOSPS1-DNUPLEM** LEH**2*SINDSIACOSPS1-DNUPLEM** LEH**DMURA-FHUR**E2C+YC*UCPDK)  **(EM**DMUNTA-YC*CPUTA-YC*CPDK)-X-FMRAN  DZAY2T=-D2MY21+(DMDT**UMUY2+EM**D2MY21+  **(EM**DMUNTA-YC*CPUTA-YC*CPTA-YC*UCPDK)  S*(EM**DMUY2*YC*DCPTA-YC*UCPDY)-X-PC**D2CY2T  **(EM**DMUY2*YC*DCPUY2)-YEMRAD  D2AY3F=-D2MY3P+(**DCPDY3)-YEMRAD  **(EM**DMUY2*YC*DCPUY3)-YEMRAD  **(EM**DMUY3*YC*DCPUY3)-YEMRAD  DABY3=-DMUY3+YC*DCPUY3)-YEMRAN  DABY1=-DMUY2+(EM**DMUY1+YC*DCPUY3)-YEMRAN  DABY3=-DMUY2+(EM**DMUY2+YC*DCPUY3)-YEMRAN  DABY3=-DMUY3+(EM**DMUY2+YC*DCPUY3)-YEMRAN  DABY3=-DMUY3+(EM**DMUY2+YC*DCPUY3)-YEMRAN  DABY3=-DMUY3+(EM**DMUY2+YC*DCPUY3)-YEMRAN  DABY3=-DMUY3+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3=-DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3DMUY1+(EM**DMUY4+YC*DCPUY3)-YEMRAN  DABY3DMUY1+(EM**DMUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY3)-YEMRAN  DABY3DMUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY3)-YEMRAN  DABY3DMUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY1+YC*DCPUY3-YC*DCPUY1+YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUY3-YC*DCPUX3-YC*DCPUX3-YC*DCPUX3-YC*DCPUX3-YC*DCPUX3-YC*DC	513 D2MY3P=-(FHCSP2*DCPDY3/F2*DFHUP-YC*UCPD <sub>Y3*</sub>	POWEnoa0	
DEAYIR= -U2MY1R + (UMUR*DDMDY1+EM * U2MY1R + (FHCSP2/F)*PINTSITY=*U2SY3PINTER*DDMDY1R* * U2MY1R + (FHCSP2/F)*PINTER*DCPUNI**PINTER*DDMN* * (EM*UMUR*R-F)*PINTER*DDMN*   FMRAN   * (EM*UMUNI*TC*DCPUNI) / FMRAN   * (EM*UMUNI*TC*DCPUNI) / FMRAN   * (EM*UMUNI*TC*DCPUNI) / FMRAN   * (EM*UMUY*1*TC*DCPUNI*TER*DCMN*   * (EM*UMUY*1*FEC+YC*UCPUNI*TER*C + YC*UCPUNI*TER*C + YC*UCPU	CCPOP/SINDSI*COSPSI-DNDP/TE	POWE n091	
D2AY1R= -U2MY1R + (UMUR*DMADT1+EM * U2MY1R +(FHCSP2/F9*0FHUR+Y2*UCPDK1)*NCPUY1+YC*N2CY1K -(EM*UMUY1+YC*DCPUY1)/EMRAD2//FMRAD D2AY2T=-D2MY21+(DMDT*UPCPUY1)/EMRAD2//FMRAD NE(EM*UMUY1+YC*DCPUY1)/EMRAD2//FMRAD2//FMRAD2/ NE(EM*UMUY1+YC*DCPUY1)*UCPUY2+YC*U2CY2T NE(EM*UMUY2+YC*DCPUY1)*UCPUY3+EM*U2MY3P NE(EM*UMUY2+YC*DCPUY2)/EMRAD2//FMRAD2/ NE(EM*UMUY3+YC*DCPUY3)/EMRAD2//FMRAD2/ NE(EM*UMUY3+YC*DCPUY3)/EMRAD2//FMRAD2//FMRAD2/ NE(EM*UMUY3+YC*DCPUY3)/EMRAD2//FMRAD2//	TH**X*OINDOILEANDSOXON	POWE01092	
+ (FHCSP2/F9*0FHUR+Y2*UCPDK1)*NCPUY1+YC*N2CY1K - (EN*UMUY1+YC*NCPDK1) *NCPUY1+YC*N2CY1K - (EN*UMUY1+YC*NCPUY1)/EMRAD2 / FMRAD			
	ı	POWED095	
1 E R E M B M D M D M D M D M D M D M D M D M D	:	POWENDA6	
(FHCSP2/F2#UF   VUMNIT   VUM	**************************************	POWEn097	
D-2AY3P= D-2AY3P + (UMDP-2D/EDT)  S*(EM*UMUT-DFHUT*FEC+YC*UCPDT)  D-2AY3P= - U2AY3P + (UMDP-2DMDY3+EM * U2MY3P	1.05.07.1.1.1.00.1.1.1.1.1.1.1.1.1.1.1.1.1.1	POWEROOS	
194 (EM*UMUY2+YC*DCPUY2)/EMRAD2)/EMRAD D2AY3P= -U2MY3P + (OMUP*DMDY3+FM * U2MY3P -LEM*DMDY3+YC*DCPUY3+YC*D2CY3P -(EM*UMUP3+FFHUP*F2=YC*C+YC*DCPUY3+YC*D2CY3P -(EM*UMUP3+YC*DCPUY3)/EMRAD2) / FMRAD DERIVATIVES OF A WITH RESPECT TO*Y1*Y2*Y3*PHI*THETA*P DADY1 = -UMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY2)/EMRAD DADY3 = -DMUY3+(EM*UMUY2+YC*DCPUY2)/EMRAD DADY3 = -DMUY3+(EM*UMUY3+YC*DCPUY3)/EMRAD DADY3 = -UMUT1+(EM*DMNY+F2C*DCPUY3)/EMRAD	2-(Ex+DMDT+OFHDT+F20+YC+COPDT)		
DZAY3P= -UZMY3P + (UNUP*DMDY3+EM * UZMY3P + FFHCSP2/F3-PGFHUP+Y2*UCPDP) *DCPUY3+YC*D2CY3P - (EM*UMUP+FFHUP*EZC+YC*UCPDP) * (EM*UMUY3+YC*DCPUY3)/EMRAD2 / FMRAD DERIVATIVES OF A WITH RESPECT TO*YI.Y2*Y3*PHI*THETA*P DADY1 = -UMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY2)/EMRAD DADY3 = -DMUY3+(EM*UMUY2+YC*DCPUY3)/EMRAD DADY3 = -DMUY3+(EM*UMUY3+YC*DCPUY3)/EMRAD DADY3 = -UMUR1+(EM*MDMCPUY3+YC*DCPUY3)/EMRAD DADY3 = -UMUR1+(EM*MDMCPUY3+YC*DCPUY3)/EMRAD		POWED101	
+ (FHCSP2/F0+0FHUP+Y2*UCPDF)*DCPUY3+YC*D2CY3P - (EM*UMUP+nFHUP+Y2*UCPDF) * (EM*UMUY3+YC*DCPUY3)/EMRAD2) / FMRAD DERIVATIVES OF A WITH RESPECT TO*Y1.Y2*Y3*PHI*THETA*P DADY1 = -DMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY2)/EMRAD DADY3 = -DMUY4+(EM*UMUY2+YC*DCPUY3)/EMRAD DADY3 = -DMUY4+(EM*DMUY2+YC*DCPUY3)/EMRAD DADY3 = -DMUY4+(EM*DMUY4+YC*DCPUY3)/EMRAD DADY3 = -DMUY4+(EM*DMUY4+YC*DCFUY3)/EMRAD		POWENTOS	
**CEM*UMUP+nFHUP*F2C+YC*UCPDP)  **(EM*UMUY3+YC*DCPUY3)/EMRAD2) / FMRAD  DERIVATIVES OF A WITH RESPECT TO*Y1*Y2*Y3*PHJ*THETA*P  DADY1 = -DMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD  DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY1)/EMRAD  DADY3 = -DMUY4+(EM*UMUY2+YC*DCPUY2)/EMRAD  DADY3 = -DMUY4+(EM*DMUY2+YC*DCPUY3)/EMRAD  DADY3 = -DMUY4+(EM*DMUY2+YC*DCPUY3)/EMRAD  DADY3 = -DMUY1+(EM*DMUY2+YC*DCPUY3)/EMRAD	1 + (FHCSP2/F>*DFHUP+Y2*UCPDP)*DCPUY3+YC*D2CY3P	POWENINS	
** ** ** ** ** ** ** ** ** ** ** ** **	2 *(EM*UMUP+nFHUP*F2C+YC*UCPD*)	POWEning	
DERIVATIVES OF A WITH RESPECT TO/Y1/Y2/Y3/PHI/THETA/P  DADY1 = -UMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD  DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY2)/EMRAD  DADY3 = -DMUY3+(EM*UMUY2+YC*DCPUY2)/EMRAD  DADY3 = -DMUY4-(EM*UMUY3+YC*DCPUY3)/EMRAD  DADK= -UMUR4-(EM*DMUY +F2C*DFHUYC*)/EMRAD  DADI = -DMUT4-(EM*CMO)+F2C*DFHUYC*	5 *(EM*UMUTS+TC+UCPUTS)/EMRADZ) / FMRAD	POWE 1105	
DADY1 = -UMUY1+(EM*UMUY1+YC*DCPUY1)/EMR4D DADY2 = -UMUY2+(EM*UMUY2+YC*DCPUY2)/EMR4D DADY3 = -UMUY2+(EM*UMUY2+YC*DCPUY2)/EMR4D DADY3 = -UMUY2+(EM*UMUY3+YC*DCPUY2)/EMR4D DADY3 = -UMUY4-(EM*UMUY4-YC*DCPUY3)/EMR4D DADY3 = -UMUY4-(EM*UMUY4-YC*DCPUY3)/EMRAD	A WITH RESPECT TO:Y1.	POWEN106	
DADY1 = -UMUY1+(EM*UMUY1+YC*DCPUY1)/EMRAD DADY2 = -DMUY2+(EM*UMUY2+YC*DCPUY2)/EMRAD DADY3 = -DMUY3+(EM*UMUY3+YC*DCPUY3)/EMRAD DADY3 = -DMUX4+(EM*UMUY3+YC*DCPUY3)/EMRAD DADK= -DMUX4+(EM*UMUY4+F2C*DFHDY4+YC*UCPUN)/EMRAD DADY1 = -DMUY1+(EM*NMO)+F2C*DFHDY4+YC*UCPUN)/	A WITH RESPECT TOTAL	POWERIN/	
DADY2 = -DMUY2+(EM+DMUY2+YC+DCPUY2)/EMRAD DADY3 = -DMUY3+(EM+DMUY2+YC+DCPUY2)/EMRAD DADY3 = -DMUY3+(EM+DMUY3+YC+DCPUY3)/EMRAD DADK= -DMUR+(EM*DMUY + F2.2 b F HUR + YC * UC+DR)/ EMRAD DADK = -DMUR+(EM*CMU + F2.2 b F HUR + YC * UC+DR)/ EMRAD	DADY1 = -UMUY1+(EM*UMUY1+YC*D(PuY1)/	POWENTOS	
3 = -DMDY3+(EM*DMUY3+YC*DCPUY3)/EMRAD = -DMDR+(EM*DMDX +F2C * DFHUR +YC *UCPDR)/ EMRAD = -DMDT+(EM*CMD1+F2C*UFHD1+YC*	DADY2 =		
= -UMUR+(EM*DMnx +F2C * DFHUR +rC *UCPDR)/ EMRAD = -UMUT+(EM*AMD(+F2C*)FHD(+*C*	= -DMDY3+(EM*UMUY3+YC*DCPUY3)/	DOMEOSTS	
II -DECT+(FERCED(+DFFDT+YC+	-UMUR+(EM*DMNK +F2C * DFHUR +rc *UCPDR)/	POWER112	
	I -DMDT+(EM*CMD (+F2C+DFHDI+YC*		

STAGED TALKNED	
10CBJ11/EMABL   5.10 NDBJ21-WHADL   5.10 NDB	
5.17 INNOVET CHURCH CONTROL OF THE C	
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DOUGNETALT - PROPERTY	
DRDPI-LDMD-POINTS	
SEC   DERMOUST = DIMPORT   POWE   DERMOUST = DIMPORT   POWE   DOWE   D	
S20   DZWUSKE   FHCSSP2*SINES  1*DFHURFFFFFFF (**COSP-CZ/SINES  1*SinFs 1**)	
SEC DEMUSATE   CHECKPRESTINES   SHOPH HURFFFFFFFFFFF   CHECKREAZIS   DEMUSATE   CHECKPRESTINES   SHOPH HURFFFFFFFF   CHECKPLESTINES   STEATUREST   SHOPH HURFFFFFFF   CHECKPLEST   CHECKP	
1 (CRM) 51 (FICE) 52 STINES 1 (FICE) 54 FFLY L1 \$5 STINES 1 F5 STI	
DCBUIST = Inch Per STRONG	
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SECUND DEMOSP = (FRCSC2**SINcSI40FHIPFEFIFF   ** (~* CGSFG2/SIAPSI+SINPSI)*   POWE   DOWE	
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5.22 D2UUSRE — LUMUDSI/EMILORPENDUR/EMD-5DMUDS.1 + XTERM *  CIULUSRE — LUMUDSI/EMILOPDR/EMBORINGSI + (UMUS) + **LUMPE-1**DENR + **YC** COSPSI POWED 13.3  2	
22 U2UUSR - UMUUSIK-UDRADK-EMRAD-PARELY - TELWAD PARELY - TELWAD STANDER -	
1 (1-02/MOJNY-DARCHER NET STANDS) INDEPT STREAMS (1978) 1978 1978 1978 1978 1978 1978 1978 1978	
2	
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DZULOS   1 - DMULD   1 - DMU	
1 (-O_EMOS_1 = DHUTERRAA-POD_S) + FUNDURP   FEM=DEMINS   2 - 2 * FEC/COSFS   FOREITS   3 / SINDS   FOREITS   1	
2-2.*F2C/COSPS.15 JINDS.14.8.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.15.1 JINDS.14.1 JINDS.14.1 JINDS.14.1 JINDS.14.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.14.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.15.1 JINDS.14.1 JINDS.1	
3/SINSIEDCPUT) / EMHAND > TERM#FADDI/EMD*DMD_SI + XIERM * POWE 0134   D2ULSPE - UMUUD:I/EMI#FONDUP/EMD*DMD_SI + XIERM * POWE 0134   1	
D2UUSPE LONUDS.I/EMIL*DMUUDP.EMD*EMD*S.I + XIERM *    1	
1 (-D2MUSP+(rMD5I*DMDP+EM*D2MJSP 2 -2**P2C/COCOS1*SINDSI*DMDP+EM*D2MJSP 3 /SIMPSI*DESI*DESI*DEDP/EM*AD*DDP/FMD*DMDPSI) POWED140 3 JC1MPSI*DCC-D*DAYZINDSI*DCP/FMD*DMDDSI) POWED141 1+D2A1TR*ENDAGC-2**rMUNT-2**EN/EMD*DADI) POWED142 1+D2A1TR*ENDAGC-2**rMUNT-2**EN/EMD*DADI) POWED143 1+D2A1TR*ENDAGC-2**rMUNT-2**EN/EMD*DADI) POWED144 1+ENDAGC*D2A7ZI-2**rMUNT*DMUNT2)/2**LMU 1+ENDAGC*D2A7ZI-2**rMUNT*DMUNT2)/2**LMU 1+ENDAGC*D2A7ZI-2**RMUDY2)/2**LMU 1+ENDAGC*D2A7ZI-2**LMUADCC*DADP/EMD) *DADY3+ POWED145 1*ENDAGC*D2A7ZI-2**LMUDY3)/(2**EMU) *DADY3+ POWED149 524 YPEMDU = YP(4)-EMU*DMUDY3 524 YPEMDU = YP(4)-EMU*DMUDY3 525 YF3MDU = YP(5)-EMU*DMUDY3 526 XTEM2=EMUS*DMUDY3 526 XTEM2=EMUS*DMUDY3 526 XTEM2=EMUS*DMUDY3 526 XTEM2=EMUS*DMUDY3 527 DUY3RP=DCUZYI*DRP*DMUDY3 528 RDOID=IURFDR*YTEMDI*DRP*DMUDYP*NPDRPP 528 RDOID=IURFDR*YTEMDI*DRP 528 RDOID=IURFDR*YTEMDI*DRP 528 RDOID=IURFDR*YTEMDI*DRP 528 RDOID=IURFDR*YTEMDI*DRP 529 RDVINTRP=DCUZYI*DRP 529 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 521 RDVINTRP=DCUZYI*DRP 522 RDVINTRP=DCUZYI*DRP 523 RDVINTRP=DCUZYI*DRP 524 RDVINTRP=DCUZYI*DRP 525 RDVINTRP=DCUZYI*DRP 526 RDVINTRP=DCUZYI*DRP 527 RDVINTRP=DCUZYI*DRP 528 RDVINTRP=DCUZYI*DRP 528 RDVINTRP=DUSSRP 529 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP=DCUZYI*DRP 520 RDVINTRP 520 RDVI	
2	
3 /SINPSI*DCCUP)/EMRAD -D&DP/EMRAD*PDSI-DADP/FMD*DMDSI) POWEn141 D2UXIR = ( (DADY1/AA>C1)* (DNUK-2**EN/EMD*DADR) 1+D2AYIRENDAGC2-2***NUUR*BNUURY)/C**EMU*DARDR) 1+D2AYIRENDAGC2-2***NUUR*BNUURY)/C**EMU*DABDI) D2UXZI = ( (DADY1/AA>C1)* (DNUK-2**EN/EMD*DADR) 1+ENDAZC*DZAY21-2***NUUR*CHUURY)/C**EMU*DADRI) 523 D2UXZP = ( (UNUP/AA>C1-2***FNUURZC*DADP/EMU) *DADY3*+ POWEn145 1ENDAZC*DZAY3P-2**U**UMDY1 1*ENDAZC*UZAY3P-2**U**UMDY1 1*ENDAZC*UZAY3P-2**U**UMDY1 1*ENDAZC*UZAY3P-2**U**UMDY1 1*ENDAZC*UZAY3P-2**U**UMDY1 1*EMU*DMUUNTY1 1*EMU*DOMUUNTY1 1*EMU*DMUUNTY1 1*EMUNTY1 1*EMU*DMUUNTY1 1*EMU*DMUUNT	
D2UY1R = ((DADY1/AA>C1)*(DNDR-2**EN/EML*DADR)	
1+DZAYIR*ENDAZC=2**NMUDR*DMUDY1)/2*/EMU  DZUYZI = ((UAUYZ/AAZC1)*(UNUT=2.*ENVEMD*DADT)  DZUYZI = ((UAUYZ/AAZC1)*(UNUT=2.*ENVEMD*DADT)  POWED144  523 DZUYZR== ((UNUP/AAZC1)**(UNUT=2.*ENVEMD*DADF)  IENDAZC*DZAY3P=2 **ENUDZC*DADF/EMU) *DADYZ+  POWED145  DYPEMDU = YP(5) -EMU*DMUDY3 / (2 **EMU)  \$24 YPEMDU = YP(5) -EMU*DMUDY1  POWED149  POWED149  \$25 YP3MDU = YP(6) -EMU*DMUDY3  YPZMDU = YP(6) -EMU*DMUDY3  POWED152  POWED153  POWED154  POWED154  POWED155  POWED164  S29 DELSS=(2 **EMU/KP+DMUDRP*DMUDYZ+EMU*DMUDKP*DM	
DEUTY2T = (IUAUYZEAAZCI)*(UNILT=2.*ENNEMD*NADI)	
1+ENDA2C C*DCAY21-2**FMUDT*DMIDY2)/2*/LMU 523 D2UY3P = (UNLDP/AA2C1-2**FMUDA2C C*DGAPC/EMU) *DADY3+  1ENDA2C C*UZAY3P-2**FMUDT(1-2**EMU) *DADY3+  1ENDA2C C*UZAY3P-2**L**FMUDDY3  524 YPEMDU = YP(4)-EMU*DMUDY1  YPEMDU = YP(5)-EMU*DMUDY2  YPEMDU = YP(5)-EMU*DMUDY2  S26 XTEM2=EMUS+UMUDDY3  S26 XTEM2=EMUS+UMUDS1**2  XTEM=SQRT(XTEM2)  POWE 0152  POWE 0153  POWE 0154  POWE 0155  POWE 0156  DUY2RP=D2UY2T*DIDRP  DOWE 0157  DUY2RP=D2UY2T*DIDRP  DOWE 0157  DOWE 0157  DOWE 0156  229 DEL 2S=(2**EMUZNP+DMUDRP*DMUDY2**EMU*DHYRP) + PROWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DMUNY1*EMU*NIXT*RP) + DROWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DMUNY1*EMU*NIXT*P) + DOWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DANY1*EMU*NIXT*P) + DOWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DANY1*EMU*NIXT*P) + DOWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DANY1*EMU*NIXT*P) + DOWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DANY1*EMU*NIXT*P) + DOWE 0156  ZP(1)**(YPEMUUNY1*EMUDNP*D*NEN*UMDRP*DANY1*EMU*NIXT*EMU*	
523_DUY3P = (IUNDP/AA2CI-2**ENUAZC*DADP/EMU)*DADY3+  IENDA2C*U2AY3P-2 **U.*UPP*UMUDY3)/(2**EMU)  1ENDA2C*U2AY3P-2 **U.*UDP*UMUDY3  524 YPEMDU = YP(4) -EMU*UMUDY1  524 YPEMDU = YP(4) -EMU*UMUDY3  525 YP3MDU = YP(5) -EMU*UMUDY3  526 XTEM2=EMUS+UMUDSI**2  XIEM=SGRI(XTEM2)  DUWDRP=DWUDK*URORP+UMUDI*TORP+UMUDP*UP)RP  DWUDRP=DWUDK*URORP+UMUDI*TORP+UMUDP*UP)RP  DWUDRP=DWUDK*RDRDRP  DWEN153  DOWEN154  DOWEN155  DOWEN156  DOWEN156  DOWEN156  DOWEN156  DOWEN157  DOWEN156  DOWEN156  DOWEN156  DOWEN156  DOWEN156  DOWEN156  S29 RDOID=[URPDR*YPEMUURP)*RUDIP=EMU*RUDIPXIEM2*(EMU*DMUNRP POWEN160)  POWEN156  S29 RDOID=[URPDR*YPEMUURP)*RUDIP=EMU*RUDIPXIEM2*(EMU*DMUNRP POWEN160)  POWEN156  S29 RDOID=[URPDR*YPEMUURP)*RUDIP=EMU*RUDIPXIEM2*(EMU*DMUNRP POWEN160)  S29 L11*(YPSMUUNTYPEMUURP)*RUNDRP*NMUNT1*EMU*NITTRPPTXYPOWEN163  1+UMUDSI*DUDSRP) -EMI*XTEM*(UMUDRP*NMUNT1*EMU*NITTRPPTXYPOWEN163)  S29 L11*(YPSMUUNTYPEMUURPPEMUNDRPPRAMUNTA*EMU*NITTRPPTXYPOWEN163)  S29 L11*(YPSMUUNTYPEMUURPPEMUURPPEMUURPPEMUNTA*EMU*NITTRPPTXYPOWEN163)  S29 L11*(YPSMUUNTYPEMUURPPEMUURPPEMUURPPEMUNTA*EMU*NITTRPPTXYPOWEN164)  S29 L11*(YPSMUUNTA*EMUNDRPPEMUURPPEMUURPPEMUNTA*EMU*NITTRPPTXYPOWEN164)  POWEN164  S29 L11*(YPSMUUNTA*EMUNDRPPEMULPPEMUNTA*EMU*NITTRPPTXYPOMEN164)  POWEN164  S29 L11*(YPSMUUNTA*EMUNDRPPEMUNDRPPEMUNTA*EMU*NITTRPPTXYPOMEN164)  POWEN164  S29 L11*(YPSMUUNTA*EMUNDRPPEMUNDRPPEMUNDRPPEMUNDRPPEMUNDRPPTXYPOMEN164)	
TENDA2C	
S24	
524 YPEMDU = YP(4) -EMU*DMUDY1  YPEMDU = YP(5) -EMU*DMUDY2  525 YP3MDU = YP(5) -EMU*DMUDY2  526 YP3MDU = YP(5) -EMU*DMUDY3  S26 XTEM2=EMUS+UMUDS1**2  XTEM=50RT (XTEM2)  DUUSARP=DQUDSR*DRDH*+DMUDT*UTDRP+UMUDP*UP)RPP  DUUSARP=DQUDSR*DRDH*  DUUSARP=DQUDSR*DRDH*  DUUSARP=DQUDSR*DRDH*  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DUYSRP=UZUY21*DTDRP  DOWE0155  DOWE0156  DOWE0156  S29 REALSS=(2*0*EMU/RP+DMUDRP)*RUDTPEMUSR*(UMUDRP*YP3MUDYREM2)*DRPDT/YPOWE0160  1*XTEM  S29 DELSS=(2*0*EMU/RP+DMUDRP)*RUDTPEMUSR*(UMUDRP*DMUDYREM3)*DRPDT/YPOWE0160  S29 DELSS=(2*0*EMUZYP2*DMUDRP*DMUDYZPEMUSR*(UMUDRP*DMUDYREM3)*DRPDT/YPOWE0160  S29 DELSS=(YPZMUDYRP2*DMUDRP*DMUDYZPEMUSUYA1*EMUSNYA1*DPRANST)*DOWE0161  S29 L11* (YPZMUDYRPDPXYST)*DRPDT/YFUNDYRENST)*DOWE0161  S29 DELSS=(YPZMUDYRPDTYRENDYRENST)*DRPDT/YFUNDYRENST)*DRPDT/YFUNDYRENST)*DOWE0161  S29 DELSS=(YPZMUDYRPDTYRENDYRENDYRENST)*DRPDT/YFUNDYRENDYRENTST*DRPDT/YFU	
YP3MDU = YP(5)-EMU*UMUDDY2 YP3MDU = YP(6)-EMU*UMUDDY3  XIEM2=EMUS+UMUDDI**2  XIEM2=EMUS+UMUDSI**2  XIEM2=EMUS+UMUDSI**2  XIEM2=SQRI[XIEM2]  DWGEN151  POWEN152  POWEN153  POWEN154  POWEN155  POWEN155  POWEN155  POWEN155  POWEN155  POWEN155  POWEN156  POWEN1	
YP3MDU = YP(6)-EMU*DWDY3  YP3MDU = YP(6)-EMU*DWDY3  XIEM=50RT(XTEM2)  DWUDRP=DQUDSR=DQUDST*DTDRP+UMUDP*DP\RP  DWUDRP=DQUDSR=DQUDST*DTDRP+UMUDP*DP\RP  DWUNRP=DQUDSR=DQUDST*DTDRP+UMUDP*DP\RP  DWY1PP=DQUDSR=DQUDST*DTDRP  DWY1PP=DQUYSP=DQUDST*DTDRP  DWY1PP=DQUDSR=DQUDST*DTDRP  POWEO156  DWY3RP=DQUYSP*DTDRP  DWY3RP=DQUYSP*DTDRP  POWEO157  DWY3RP=DQUYSP*DTDRP  POWEO156  DWE0158  POWEO161  POWEO161  POWEO161  ACCOUNT OF CANDOND ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS ACCOUNTS ACCOUNTS AND ACCOUNTS ACCOUNTS AND ACCOUNTS AC	
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XTEM2=EMUS+UMUDS1**2  XIEM250RI(XTEM2)  XIEM250RI(XTEM2)  XIEM250RI(XTEM2)  XIEM250RI(XTEM2)  POWEN154  POWEN154  POWEN154  POWEN155  POWEN155  POWEN155  POWEN156  POWEN160  POWEN160  POWEN160  POWEN160  POWEN160  POWEN161  POWEN160  PO	
XTEM=SQRICKTEM2)	
DMUDRP=DMUDR*UDRP*DMUDR*DTORP+LUMUDP*UP)RP	
DUDSRP=12/UDSR*0KDKR+DZUUSI*DIUKF+UZUUSP*NFUKP   POWEO157	
DUYIRP=D2DYIR*DKORP  DUYZRP=D2DYIR*DKORP  DIYZRP=D2DYZ#DIDRP  DOWEDISG  DOWEDISG  DOWEDISG  DOWEDISG  POWEDISG  POWEDISG  POWEDISG  POWEDISG  DOWEDISG  DOWE	
DAY2RP=D2UY2T#DIDRD  DAY2RP=D2UY3PP=D2UY3P#DIDRD  S28 RDOT3RP=L2UY3P*DDRDC  S28 RDOT3RP=L2UY3P*DDRDC  S28 RDOT3RP=L2UY3P*DDRDC  S29 DEL2S=(2.0*EMU-KP*DMURP)*RDOTP-EMU*RDOTP/XTEM2*(EMU*DMURP)  POWEO161  1-DMUDS1*DUDSRP)-EMILY (DRDDRP*DMULY2*EMU*DUTY1*EM)*DRPOTYPOWEO163  20 DEL2S=(2.0*EMU/KP*DMULY2*EMU*DUTY2*EMU*DUTY2*EMU*DUTY3RP)*DPWEO163  20 CONTROL OF CONTROL	
527 DUY3RP=12UY3P*DPDRP 528 BONEDID=1.09 528 ADDIP=1.08 528 ADDIP=1.08 529 DEL25=(2.0*EMU/RP+DMUDRP)*RUDIP-EMU-RUDIP/XIEM2*(EMU+DMUDRP 529 DEL25=(2.0*EMU/RP+DMUDRP)*RUDIP-EMU-RUDIP/XIEM2*(EMU+DMUDRP 1+DMUDSI*DUDSRP)-EMI-XIEM*(DMUDRP*NMUDY1+EMU*DIY1RP)+DRPDT-XPOWE0163 2.0.0.005	
528 RODOE=LURFDH*YPEMDis*PEMDIS*YPEMDIZ*YP.LIJ*DRPUP*TP.3MUOZ*SIJ. POWEDIS.L 529 DELZS=[2.0*EMU/RP+DMUDRP)*RDOIP=EMU*RUOIP-YXEMV*DINY1RP)+DRPDTA 1+DMUDSI*DUDSRP)-EMI.X TEM*(DRPUR*(DMUDRP*nMUDY1+EMU*DINY1RP)+DRPDTA*YPOWEDIS.3 2P(1)*(YYPOWDYTP)-EMI.X TEM*(DRPUR*(DMUDRP*nMUDY1+EMU*DINY1RP)+DRPDTA*XPOWEDIS.3 2P(1)*(YYPOMDYTP)-CARDIDAPS*VPAMUDY12+EMU*DINY2RP) 2P(1)*(YYPOMDYTP)-CARDIDAPS*VPAMUNI+DMILOP*DMUDY3+EMI*RUY3RP) POWEDIS.	
1/XTEM  1/XTEM  529 DEL2S=(2.0*EMU/RP+DMUDRP)*RUOIP-EMU*RUOIP/XTEM2*(EMU*DMUDRP POWEN162  1+DMUDSI*2NDSRP)*EM:/XTEM*(DRPUR*(DMUDRP*DMUDY1+EMU*DIY1RP)+DRPDT/YPOWEN163  2.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	
1-DMUDSI PARADLYRY-DMUDRY - KNOT PERMOTHER ALL MEAST AND THE STATEMENT OF	
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SSAL INTITI-DELEST ENGINEER POWERIES	
POWER 150	

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SUBROUTINE FORCE CUMMON /DAIA/ BMAX. PMIN,	RMIN. IMAXE PRNI. RELERRE		X. RMIN. IMAX. TMINE PMAX. N. PRNI RELERY AO. THETAO. PHIO. PLUS. NEOWERS.		FORCOORS FORCOORS FORCOORS	
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DO NYDER	DCPUY3. SP. SOLUTION MUFLA. R. MOMALF.	EMUINT LOUR.	FMUS 11)	NOEG.	FORCHOIU FORCHOIL NOEG, FORCHOIZ MA(260)FORCHOI3	
100 YNRMLZ=EMU/KTYSGR 101 YO(4)=YNRMLZ*YO(4) YO(5)=YNRMLZ*YO(5)	011	1		:	FORCO014 FORCO015 FORCO017	
102 TOTAL TINRMLZ*TOTAL RETURN					FORCA018	

20 0	20 304		
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COL - FFN SOURCE STATEMENT - IFN(S)			
SUBROUTINE COLL( YALYTOZYTOĞ'GNU )			
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KADIANS			
COLLISION ERFOUENCY			
DIMENSION A(b) r n(b) r.			
(5) (7)			
2-12847			
-1-47//E-/4-8192E-1			
-1.5422E-/* -1.4/UNE-Z *			
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DATA D / -1./828E-1, 5:339/E U / 5:00/20F U	COLLABO		
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1.474 - 1.00 - 1.00			
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5 ENITS 13527 - 07392*X	COLLBO24		
ON9***01:200 6	COLL/1025	æ	
	COLLOUZE		
6 COEFF=(C(1)*Y02+C(2))*Y02+C(3)+((U(1)*Y02+D(2))*Y02	COLL 0027	á	
1 + \$4(3.1) * (2.05) (7.03)	COLL0029		
7 (	COLLODSO		
XFAC = X * 0.1570H	C0LLn031		
OF SAN MINUTES	COLL 0032	12	
E=COS (XFAC)		13	
75 GNUE ((A(4)*X+A(3))*X+A(2))*X+A(1)+A(2)*E±A(0)*S±(((B(4)*X+B(3))*X.	- 1		
1+6(2))*X+6(1)+8(5)*E+b(6)*S)*COEFF			
6-01 09	COLL 1030		
8 X=X+475.	COLL 0030		
	COL 1 0030		
6 01 09	COLLOGAO		
END	V 011 110 1		

SUBROUTINE CSINT (*X*CI*SI)	CSTINUNZ		
꾀	CST10003		
[Min A2/335.b7/32.b70.23628/352.u1u5u+1114.9789/	CST10005	:	
	CSTINONE		
þ			
	900011SD	:	
1 E	CSTICOLO		
	CSTIND11		
4 POFX=0.0	CST10012		
DOI 1150 4 (1	CST10014		
0.00LU=0.00	CST10015		
S GN = +1.0	CST10016		
EKROR =	CST10017		
20 DO 40 N=1.15	CST10018		
ZIN*XIII	CST10019		
NN=NN+T	CST1n020		
N+IC*N	CST10021		
BN-1.0	CST1n022		
21 IF (M) 30 ,22, 22	CST10023		
22 POFX = POLD + S GN*IOR(NN)/X**CN	CST1n024	16 17	
IF (ABS (ABS )	CST10025		
1 + 11 ×	CST10026		
٠	CST10027		
_	CST10028		
1F (MM) 35	CST10029	İ	
OUFX = GOFX + S GN+TOK(NNN)/X**BN		26 27	
٦ :	CST10031		
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35 IF (M) 41.40.40	CS110035		
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11 V T T T T T T T T T T T T T T T T T T	CST10048		
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70#12 0 11 2 11 11	CST10051		
:		75	
-15	ST10053		
DO 440 N =2.50	CST10054		
	CST10055		

CSI - EFW SOURCE STATEMENT - IFN(S) -	02/06/69 PAGE 30	
C. II 50.40.0	Caretion	
421 IF (N) 431-420-420	ACT CARE	
) * ( CN-4 • 0 ) * ( CN-5	05.00.1.0.1 04.00.1.10.1	
TERM = P*(1.0/(CN-3.0)-PP/(((CN-1.0)**2)*(CN-2.0)))	CST1066	
1-ERRUR 425,425,43	CST10061	
TERM	CST1062	
60 10 430	CST10063	
425 M=-1	CST10064	
430 IF (MM) 435+431-431	CST10065	
tol 0 H 0*PPPV((CN-0)*(CN-0)*(CN-0)*(CN-0))	CST1n066	
TERS     -0*(1.0/(CN-0.0)+DF/((CN-1.0)*CN**U))	CST10067	
IF (ABS (TERM) - EPROK ) 434,44,43	CSTINGS	
433 CI + TERM	CST10069	
60 10 435	C <t10070< td=""><td></td></t10070<>	
	14001170	
435 IF (M) 500+440+440	CST10072	
ゔ	CST10073	
500 IF(XX) 501,503,503	CST10074	
- 1	CST10075	
503 RETURN	CST10076	
5002 CONTINUE	CST10077	
5005 xsg=x*+2	CST10078	
REC=1.0/XSQ	CST11079	
5006 DO 5007 I=1*4	CST1n0x0	
5007 OP(1)=REC*(MEC*(REC*AU(1)+A2(1))+A4(1))+A6(1)+X50	CST1n0A1	
5008 P = 0P(1)/(@P(2)*X)	CST100A2	
Q = 0P(3)*REC/GP(4)	CST100A3	
(x) = 0.05		
(x) VIS = SS	CST1100P5 101	
5010 SI = 1.5707963 -P*CC-u*SS	! !	
C1 = P*SS-0*CC	CST1110A7	
5011 60 TO 500	CST100AB	
	0001100	

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		SIBFIC POLA

	POLA -	EFN SOURC	E STATEMED	SOURCE STATEMENT - IFN(S)	(S)				*
J							POLADORE		
اٰ	SUBROUTINE TO COMPLITE POLARIZATION	IE POLARIZA	LION				Pol A0003		
ပ							POLAn004		
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v						_	POLANON6		
	COMMON /DATA/ RMAX.	RMIN	LMAX	IMIN	PMAX		POLAD007		
_	PMIN	PRNT.	RELERR	AO			POLADORB		
a	80.	THETAD	PHIO	PLUS	NPOWER		POLADO09		
**)	S NPLOT.	,	NOAR.	NIA			POLA0010		
**	ONDR.	DND	DND	EMU	RTYSOR,		POLADOLL		
3		F2,	15	H	COSPSIO		POLA0012		
0	SINPSI	DEHDR	UFADI	DCPDT	DCPDY1.		POLA0013		
	OCPOY2.	DCPDY3.	5P.2	FMUINT	FMIS		POLANO14		
• •		SNO.	MUFLAG	NTEST			POLAN015		
J							POLA0016		
	COMMON /HBANK1/ MORDER		NOHALF	NODOUR		VOE 0	POLA0017		
7					YD(11),	WA (260)	MA (260) POLA0018		
J							POLA0019		
ر	COMMON / CRSR / Cr RCTrSrRSTrZrEMIT	RCTISIRSTIZ	, EM, TERM, T	ERM. TERM2. RMOD. RARG. YOS	RARG TOE		POLA0020		
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102	102 RMODECARS(R)		11 1900 100	147 A''' & 1 LE	•	_	POLADO31	. R	
103	RARG=ATAN2 (AIMAG(R) , REAL (R)	REAL (R)					POLA0032		
	RETURN					_	POLA0033		
	QNL						1000 100		

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02/06/69 PAGE 43	TOR NUCE	TOR 0004 2 4	TOR 0005 TOR 0007 TOR 0008
TO - EFN SOURCE STATEMENT - IFN(S) -	FUNCTION TOR(N)	TEMP=N**N NOR=IEMP*EXP(-X)*SART(6.2831853*X)+.1	TOR=NOR RETURN END

	MTMMOON	
DIMENSION ALSESIEB(35.3) (IPIV(3)	SUCCINIE	
N-11-11 1 00	9UUUNIM	
1	MINVOOOT	
00 2 1=1.NMI	OCCONIW OCCONIW	
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(7) AIdi II PAI	MINCHOLS	
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- 1	MINVOOLS	
6 IMAXILU R CONTACTION	MINVU16	
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14 DO 15 J=ICOPI'N	MINCOOK	
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12 CONTINUE.	ESOUNIW	
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	SOURCE STATEMENT -	
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			MAIN PROGRAM	Я			
		3	COMMON VARTABLES				
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3	14421	-	PRNIO	14422		PLOIT	14423	•	
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. UNU6.	SECTION	37	•	FIL.	SECTION	38		• FICN.	SECTION	39
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14	ı	14562	39	6A		14571	104	11A		14576
21		23	105			.31	1047	31A		1119
33.		.05	04			55	41	348		717
58		09	43			17	<b>بر</b> 0	414		747
S)		56	200€			72	2001	51A		003
FOR	ľ	543	T004			56	108	52A		003
55		21	2003			02	2004	62A		113
FOR		50	116			13	117	65A		120
67		23	119			63	120	469		170
70		45	122			54	123	ACT		<b>+1</b> +
73		35	125			34	126	77A		552
78	:	7.1	128			90	129	81A		522
85		<b>‡</b>	131			47	132	92A		077
76		74	##			14	45	100		152
5		22	7.4			<b>†</b>	911	143		376
70		77	134			56	135	113		162
11		99	1046			00	137	121		107
12		31	141			25	142	144		00+
14		0.1	144			05	145	149		+11
		7	1000			n n				

- 1	NANT		STORAGE				
1		SUBAOUTINE	NE INPUT				
i		100	COMMON VARTAPLES	S		: : !	
	COMMON BLOCK	DATA	OKIGIN	10000	L.E.NGTH	00053	
1	NO.	SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
i	00003 K	PAA.	0000	* ~	DMTN	00005	4
		RELERK	00007	- CK	Φ0	00010	B
		0.00	00012	œ 0	THETAO	00013	∝-
	00017 I		00000	X -	NITAR	00021	-
	100022	Z H	0.0023	• 04	DNDR	00024	- 22
		DND	92000	œ	FMU	00027	oc (
		<b>L</b>	00031	at 1	F2	00032	œ (
	00035 5004	H. C	0000 44 6000	oc o	INDEAN I	00000	×α
}		D'P D'S	0000	2 02	DCPD Y2	00043	α
	##5000	248	00045	c 2¢	FMUINI	000	: <b>c</b> c
		z	00020	H	INC	00051	œ
į.	7 70000						
	COMMON BLOCK	HBANKI	ORIGIN	00054	LENGTH	00441	
	I 00000	NOHALF	10000	⊷ -	NOTOUB SYNTE	0000	⊷ α
1		YO YO	00007	÷ œ	, CA	00022	     
i					<b>a</b>	,	
	COMMON HLUCK	CHSH	ORIGIN	00515	LENGTH	00013	
	00000 K	PcT	00001	œ	νi	00002	oc o
-			40000	<b>X</b>	M L	50000	¥ 0
	00000 K	1ER⊪2 Y06	00012	* &	Oowa	01000	r
	COMMON BLOCK	CONST	ORIGIN	00530	LENGTH	70000	
	00000 R	ш	10000	<b>~</b>	FLRAR	0000	oc (
	00000	HMAXT	t und un	<b>Y</b>	HMIN	COOM	¥
				7			
	COMMON BLUCK	NEW RUOT	00001	00537 R	LENGTH	20000	
	COMMON BLOCK	RFCT	ORIGIN	00541	LENGTH	13565	
į	00000 H	SOA	05672	œ	<b>18</b>	13564	1
1	COMMON BLUCK	RSN	ORIGIN	14326	LENGTH	10000	
	COMMON HI UCK	RHLK1	OKIGIN	14327	HENGTH	00002	
	00000 00003 R	HPRIME H0	00001 00004	oc oc	PKNELN	00005	α
	COMMON HLOCK	GRAPHU	ORIGIN	14334	I ENGTH	00023	
١	00000	3		4	0.11	00000	

	O-LANT			STOKAGE MAP	4			
YMINO	00003	Ж	PLI	40000	æ			
	200	200	Guadh.	,	# # # # # # # # # # # # # # # # # # #			
XMAX1	00000	X X	XMTH1	00001	1435/	LENGTH	00000	c
YMINI	00003	*	DATE	00000	× 04	TWUY	200.00	¥.
	COMMON	HLUCK	GHAPH.	ORIGIN	14367	1	1000	
TITLE	00000	r						
			AIG	ENSTONED PROG	DIMENSIONED PROGRAM VARIABLES			
SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE	CYMBOL	OCATION	TYPE
>	14413	r	3	14416	~	c	14421	<b>a</b>
			MIGNI	ENSTONED PROG	LINDIMENSIONED PROGRAM VARIABLES			
SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE	CYMBO	MOTTAGO	TYDE
LAST	14457	<b>.</b>	NTITLE	14460	1	NCONST	14461	I
RE AUTH	79447	<b>-</b>	RAD	14463	В	RPERD	10464	œ
PLINT	14470	<b>.</b> 2	DELAO	14466	œ,	PRINT	14467	œ
NOVER	14473	-	NALITA	1447		JTEST	14472	•
AMBUA	14476	œ	TH0	14477	- a	CATE AND	C to T	× 6
SNLAMZ	14501	r	SNLAM3	14502	œ	SNTHOI	14503	× a
SNTHOS	14504	2	SNTHO3	14505	œ	TNTHOL	14506	: 0:
ZMZ	14507	rr	STSL	14510	œ	ZM3	14511	~
ZM5	14515	2 2	CMZ	14513	<b>a</b>	ZMt	14514	œ
WALSHI	14520	æ	WALSHZ	14521	ac oc	HPP IMI	14517	oc o
7 X Z	14523	<b>x</b> :	117	14524	~	FNF	14525	r oc
Z .	0701	נוצ	ENXH	14527	8	FNY	14530	œ
•	14534	x	P. P. P. C. C. C. S. C. C. C. C. C. C. C. C. C. C. C. C. C.	14532	<b>0</b> < 0	<b>;</b>	14533	OC 1
Y042	14537	¥	Y052	14540	2 02	2000	14000	¥   0
YSQUAR	14542	×		14543	: o <u>c</u>	7. L.	14544	ĸ œ
YLYT	14545	¥ 3	ا ن پر	14546	œ	۲۲۶	14547	œ
EMI 17	2000	2	EMKAD	14551	æ	FMD	14552	œ
3	2004	ا د		14554	œ			
				ENTRY POINTS	Ş			
INPUT	JT SECTION	13						
<u> </u>				SUBROUTINES CALLED	CALLED			
.FRUU			OFROD.		NO 15	• 100		
NIS		17	ZAL			CODT		
ATAN	SECTION		EXP	SECTION		SOR	SECTION	
DENSE		ļ	• FWRD.			FIF. 0		
CALCOL		9 8	CALCOS	O3 SECTION	0N 27	.FSLO.		28
FRIN	No Section	52	• EX			.UN05.	SECTION	
•		30	•FCN•	V. SECTION		20141		

PAGE	7	0 7	<b>2</b>	-		OCATION	14615	14623	15065	15730	16146	15175	16330	16370	
<b>a</b>	SECTIO	SECTION	SECTION			IFN	FOPMAT	FORMAT	FOPMAT	38A	54A	FORMAT	71A	78A	
	F.2	CC • 1	₩•33			Z.	500	1000	1003	100	112	2002	50u#	29	
05/06/69	36	39	42		NDENCE	CATION	4613	4617	14764	5643	5017	5175	6315	5377	
STORAGE MAP	SECTION	SECTION	SECTION		IFN CORRESPONDENCE				FORMAT			!			
STO	Н.	at Lu	CC • 3		EFN IF							:		!	
						i.	981	500	1002	9	41	200	200	6	•
	£	38				NOTACO	14011	14016	14711	16536	15776	79191	16234	15202	16374
INPU			SECTION	!		Z	FORMAT	FORMAT	FORMAT	405	#6A	58A	4 <del>1</del> 9	FORMAT	BIA
	1.00	F.3	2000	10.15		2	781	501	1001		2	2000	115	2005	i,

:			SUBROUTINE	E OUTPUT				
				į				
			NOU	COMMON VARTABLES	S			
	COMMON BLOCK		EPSIN	ORIGIN	10000	LENGTH	00005	
SYMBOL EPSTIN	LOCATION TY	TYPE K	SYMHOL	LOCATION 00001	TYPE R	TUBMAS	LOCATION	TYPE
	COMMON BLUCK		DATA	ORIGIN	50000	HEGING	F. 7.000	
RMAX	70000			00001	~	TMAX	0000	· œ
NIMI			PMAX	40000	×	PMTN	0000	e ox
80 P	00000 00011		RELERK	20000	oc s	AO	00010	æ
PHIO			1 1 1 2	0000	٠,	THETAO	00013	~
NPLOT	00017		נ	00000	× ۱-	X AND SELECTION	00016	<b>⊢</b> ⊦
ı			FIN	00023	~	ACNO.	1000	٠.
DND			DND	00056	: ac		0000	c 02
KIYSGR	2 05000		u.	00031	œ	F2	00032	~ ~
10000			F	00034	2	COSPSI	00035	œ
SINFOL	00036		DFHUR	00037	œ	DFH0T	04000	œ
OCOCY 3			DCPuY1	00042	R	DCPDY2	00043	œ
FMIN	Z 2000		sps :	00045	œ	FMUINT	9#000	œ
MUFLAG			z	חרווים	1	GNU	00051	~
Modelia	COMMON BLUCK		HBANK1	ORIGIN	00026	LENGTH	00441	
HHANK	70000		NOHAL F	00001	-	BI IONON	2000	-
FINVPI	20000		NOE ©	# CCCCC	⊷ :	FINA	00002	œ
				11000	*	Q <sub>A</sub>	0n022	œ
	COMMON BLUCK		CRSR	Mala	00617			
	00000			10000	7 600	LENGTH	00013	
			2	0000	. 02	20	20000	× 0
IERM	90000		TERNIS	000u	: œ	C 240	0100	< 0
KARG	00011 R		Y06	00012	œ			
9	OMMON BL		GAUSS	ORIGIN	00532	LENGTH	0000	
Z Q	00000		DCPuR	00001	æ	UCPUP	0000	œ
DEL 2S	00000 K		F1.1	90000	œ	NANTR	00005	ď
	CUMMON BL		PUWLOS	ORIGIN	00541	FNGTH	00023	
A SOS			>-	10000	æ	DAOR.	0000	~
	COOOU		DMD	000n	~	DMDY1	0000	: 0:
DMDUSI	20000		DMDY3	20000	œ	ISUMU	00010	~
DMUDP			THOUSE CO.	21000	~	TOING	00013	œ
¥ .			TACOMO	00015	œ	<b>NALIDY2</b>	00016	œ
EMRAD	77000		DMCDST	0000	8	FMD	00021	œ
	Y 23000							
	COMMON BLOCK		GRAPH,	00100	0000			

	NWOO OO OO	CUMMON BLUCK	PLCI.	SUA	OKIGIN UOUO1	00610 R	LENGTH I.B	00003	1
JUMP	COMM	COMMON BLUCK	RUOTS	NYDı	ORIGTN UOUO1	00613 I	I ENGTH	00005	
	:			DIMEN	JONEN PROGR	NIMENSIONEN PROGRAM VARIABLES			
SYMBOL XX PLT	LOCATION U0615 U2575	T X X		SYMUSOL	LOCATION U16n3	TYPE R	SYMBOL NATE	LOCATION 02571	TYPE R
				I IND I MEN	JONED PROGR	UNDIMENSIONED PROGRAM VARIABLES			
SYMBOL THE 1A	LOCATION U2014	፫ አ ፣ ዋ		SYM;;0L PHI	LOCATION 02615	TYPE R I	SYMBOL	LOCATION 02616 02621	TYPE R B
YOSOR	U2627	<b>4 Y</b>		GROUFL GROUFL	02623	œ	٦	02624	œ
					ENTRY POINTS	; Va	i i		
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i	- - - - - - - - - -	:		1	SUBRAUTINES CALLED	CALLFD			
SGR1		SECTION 12		FWKD.	SECTION	0N 13 0N 16	•FSLO• Exp	O. SECTION SECTION	
CALCO4 UNU6. SYSLOC				CALCOS •FFIL•	!		• FXEM•	:	N 20
			:	EFN	IFN CORKE	COPRESPONDENCE			
2 11	TEN	NOT FACO		Z	IFN	LOCATION	ž.		LOCATION
200	2A	03021		201	AN S	03027	101		03102
202	4A	03070		206 206	19A	03112	46		03454
29	79A	ივაიი		26	29A	03143	207		03131
209	32A	74150		27	36A E08447	03172	1007	35A	03007
211	34A	03205		212	38A	03210	213	414	03216
21	46A	03225		214	44A	03222	22	4º4	03250
1003	FORMA!	03003		215	50A	03330	01v	51A	03371
0 1	528 588	03400		117	60A	03407	45	62A	03416
7	55A	u3427		2040	FORMAT	02657	217_	63A	03424
2041	FURMAT	U2064		2042	FURMAT	02671	2043	FORMAT	02677
2044	FORMAT	40770		2045	FORMAT	02713	2046	FORMAI	77/50

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0000	IRA	COLPUT	02716	E C	u	ı		٩.	
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	၁	00000000000		ECI	1. IN)	03010	H	111 20X	
_	20	00000000000	02721 2046.	<b>1</b> 09		03011	BCI	1 r 20 A 4	
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_	S	00000000000	02723	1 C	1, E15.6	03013 1A	֓֞֜֝֟֜֜֝֓֓֓֓֓֓֓֓֓֟֜֜֟֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֜֓֓֓֓֓֓֡֓֡֓֓֡֓֓֡֓֓֡֓֡֓֡֓֜֝֓֡֓֡֓֡֓֡֓֡֡֓֡֓֡֓֡֡֡֓֡֓֡֓֡֓	10+1	
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	ဌ	164774272155	02725 1002.	<b>1</b> 09	11,100	97000	510		
	001	00000000000000	02726	HC1	1 + HPHASE	03016	LDB	į	
02634 C.7	ပ္ပ	205517n64546	02727	HCI	1, PATH6	03017	2 2 3 1		
02635_C+8	00	21000000000	02750	BC1	1.X6HRAU	- 1	ST0	PHI	
	0CT	00000000000	02751	108 108	1, IUS10X	03021 2A	ב ב		
02637 C.10	ວ	000000000000000	02732	128	1 • 10HCOL	03022	Q.	C•3	
02640 C.11	00	157435022421	02733	BC1	1 PATTTUD	0.3023	A C X		
02641 C.12	ဌ	000000000000000000000000000000000000000	02734	8C1	1,E6,Y9HL	03024	E P	¥0+0	
02642 C.13	00	0000000000	02735	<b>1</b> 09	1.0NGITU	03025	CFS SFS		
02643 C-14	133	211454000000	02756	I DA	1.DE7X10	0.3026	STO	Ų	
0.1	001	204500n00u0u	02757	EC.	1 • HARSOR	03027 3A	ح ت	DMUDT	
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1.5	150	20240000000	02741	HC.I	1 × X10HDO	03031	STO	• Z	
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02654 KU.	<u>ئ</u>	0000000000	##/ <b>2</b> 0	1	YUMO HILL	10000	2 6		
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05660	20	1.TOPPED	02750	S S	1 PATHEX	03040	4	N.	
02661	BC1	1. ON TE	02751	8CI	1,2HY114	03041	S <sub>10</sub>	n+• N	
02662	20	1.ST FOR	02752	BCI	1, X2HY21	03042	בפ	DMUDA	
02663	PC1	1. KMAY)	02753	HCI	1,4x2HY3	03043	T. S.	DMUDR	
02664 2041.	T C	1 · (25H05	02754	Ω̈́	1.14X5HM	03044	FAD	N+•N	
	E E	1, TOPPED	02755	BC1	1,0**211	03045	FAD	N+*Z	
02666	PC I	1. ON TE	02756	qC I	1 • X4H**	03046	510	N•+2	
02667	HC.	11ST FOR	02757	8C1	1,212X10	03047 4A	TS.	SORTIL	
0.56.70	HC 1	1. KMIN	0570	BCI	1, HEPSTE	03050	Ţ	-	
02671 2042.	HC.	1, (50HrS	02761	1 2 9	1.IN CD/	03051	PZE		
02672	HC1	1.TUPPFU	02762	BCI	1,10×8HR	03052	P7E	ž	
02673	12A	1. ON TE	02763	BCI	1.AY PAT	03053	STO		
02674	Ü	1.SI FOR	0/764	Ş	1. Hayaan	03054	2	L	
02675	H	1. THETA	0.765	HCI CI CI CI CI CI CI CI CI CI CI CI CI C	1. POI ARI	03055	Z C	C.7	
02676	1	1 MAX)	02706	i G	1.ZATION	03056	X		
02677 2043	֓֞֞֞֝֞֞֞֞֝֞֞֞֞֞֝֓֓֓֞֝֞֓֓֓֞֞֝֞֓֓֓֞֞֝֓֓֞֝֞֡֝֞֡֓֡֝֞֝֓֡֝֞֡֝֞֡֡֡֝	_	7920	ָב בּ		0.3057	Q N	FMIJA	
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. **n/ cn/20	֓֞֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	1.100000	27.70	֓֞֞֞֞֜֞֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֝֓֓֓֓֓֡֝֓֡֓֓֡֝֡֓֡֓֡֓֡֓֡֓֡֡֡֡֡֓֓֡֓֡֡֡֝֡֡֡֡֓֓֡֡֝֡֡֡֡֡֡	110147	13050 2050	2.5	° .	
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	X CA	10	Ϋ́	1 X L	PZE	7 C	7 2	t ×	۲ <del>-</del> -	X X	CLA	TCX	CLA	X - 1	Z :	× .	Y Z		X X	CLA	X.	CLA	X L	4 7 Y	Y - U	1°X	CLA	1°X	4 2 3 4 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5	γ <del>Υ</del>	XVL	CLA	XS.	۲ کا ا	۲ <del>۱</del>	7 X	CL A	TCX	CLA	۲ م ۱ - ر	Z X	CLA	TCX	15X	ر. ا	APD	0 - X	17.4
	03245	03247	n3250 49A	n3251	03252	0.3253	13234	0.305	03257	n326n	0.3261	n3262	03263	113264	03265	13264	0350	0.3271	0.3272	03273	0.5274	0.3275	03276	0.5277	03301	03302	03303	N3304	20500	03307	03310	03311	n3312	0.5514	03315	03316	03317	n332n	03321	0.5324	n3324	03325	<b>n332</b> 6	Ţ,	N333N 50A	03331	0.3334 51A	
	TITLE	1.4.5 1.1.1.0.4.	F.E.C.	*+#*	3411 K.UP	• UNCS	10°Z*	F 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	; • •	Y0+5	Y0+5		#+0\ #+0\	#+O+	[+4]	5+0*	Z-+1	•	YOSUP	¥0+0	C • 14	окорет-	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	#00AR74	39**LK*UR	RARG	₽•3	RARG	NFOWER O N	4.5A	46A		ا ا	NEL25	Y0+10	x . 1	EXP,4	7	47.1LK.DR	• •	FINU	РКОРТ		N.	· ·	AL0610•4	the Hand	10. U. 1
	PZE	15.E	ΤςΣ	TXT	PZE.	77.	177	Υ <u>-</u>	S L	3	A J	STO	30.0	E P	o :	<b>3</b> 0	100	A M	STO	CLA	FID	STW	NOLL	¥ ? 1	PZE		FMD	STO	- L	300 17E	TRA	NULL	\$T2	212	4 - C	STO	ISX	1×1	PZE	770	200	FMP	XCA	٦. ٤. ا	STO	YS1	2 7	4
ASSEMBLY LISIING	0.5157	0.3160	0.5162 34A	0.5163	0.104	0,5165	0.1167	0.100 0.170 35A		0.5172 36A		0.5174	0.175	1,5176	0.517	0.5200	0.500	0.50 0.3	0,2204	0.52US 37A		- 1	0.2210 38A		0.5212	03213 4UA			03216 41A	0.3220	05221 42A	03222 43A	0.5222 44A	0.5223	0.3254 454		0.5227 47A	0.22.50	0.5231	0.52.53	0.55.4	0.5235	0,22,36	0.52.57		0.241 48A	0.00	
ASS	11A	40%	z	6•3	1 t A	00160141	-	֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	3 -		χo	XX-1,1	THEIA	11-11	֓֞֜֞֜֜֜֜֜֜֞֜֜֜֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֜֜֜֜֜֜֜֜	ر. د. اد	7114		2214	7.0	JUMP + 4	BUArtens	# I	A97		6.0	25A	29A	:	<b>;</b>	Z	C.3	ָרָר װ	%	THETAU	¥ ¥	32A	_ '	2.15	3.64		. FWKD 4	7111+*	3211LK.UR	.0N06.	100/•	*+4**	
OUIPO	12E	¥ 5	CLA	SUB	ZNI	A I	200	֓֞֞֓֓֓֓֓֟֓֓֓֓֟֟֓֓֓֓֟֓֓֓֟֟֓֓֓֓֟֓֓֓֓֟֓֓֓	2012	L (	CLA	STO	۲ د د	2 :	בי בי	905	184		AXI	XX	LAC	IXL	XEC	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	¥ 5	SUB	12E	I KA	102 202	7 G	STG	CLA	STC	S CLA	0 0	STO	IRA	CLA	SUB	18t	102	15.	TXI	PZE.	P.Z.E.	PZE	Y X	1
	03074	3075 10A		5077		05101.15A		•	\$10.00 \$1	03105 16A		03107 17A		٦.	1112 19A	03113		03116 21A	03116 22A		03120	03121	03122	0.5123	03125 23A			5130 24A	US151 25A		03133	05134	į	03136 27A	0.5140	141	03142 28A	05143 29A	0.5144			03147 32A		03151	03152	3	03155 538	777

	OUTPU	2	ASSEMBLY LIS	ING			69/90/20			PAGE 57
_ [	1757J LAC		0.34.25		210	- Jump	03512	AXI	サーチャ	
02220	TXL SEC		03426	04P	¥ ;	15A	F1650	2	2+*	
02220	100	704	7740	PCO	¥ .	*******	0.5514	4 1	##	
03341	401	-	00100		120	65.11 8.00	03516	1	-	
0 4 3 4 2	AGT		02.02.0		200	INOC	04517	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	SYSI OC.4	
03343	TRA		0.000		D7F	2046	03520	Y X	LK-DR-4	
03344	TRA		03434		A C	ΛO	n3521	A X	#-7.4	
03345	TRA		0.5435		TSX	•FCNV • •	03522	SXA	*-9,1	
03346	TRA		03436		TSX	PFIL . *	03523	S S	さらの	
03347	TR		0.3437		CLA	THETA	03524	STA	<b>V6</b>	
03350	TRA	}	0440		FSB	C•16	03525	STA	1757J	
03351	TRA		0.3441		STO	N•	03526	TPA	1A	
03352	TRA		03442		CLA	ž				
	52A IS	X .FWRD. 4	0.5443		SS					
	TXI		44450		SUB	C.17				
03355	Zd	52.1LK UR	0.5445		12E	68A				
03356	Zd		9446		ם	68A				
03357	PZE	2040.	7447	66A	NULL					
03360	TST		74450	67A	TRA	15A				
	53A TRA	_	03450	68A	S C	NYD1				
			0.5451	ı	ADO O	D. 3				
			03452		STO	NYD1				
03364	PZE		03453	A98	TRA	15A				
03365	PZE		03454	70A	CLA	NPLOT				
03366	PZE	E 2041.	03455		SUB	6.0				
03367	TSX		0.3456		INZ	72A				
		6.3A	03457		TRA	OUTPIIT+1				
03371 56	56A TSX		03460	72A	NULL					
		_	03460	73A	TSX	CALCOUP				
03373	ρZd		03461	,	X	*+5,,3				
03374	PZE	.90NO.	0.3462		PZE	73**LK.DR				
03375	PZE		03463		PZE	18				7,
03376	<b>S1</b>		103464		PZE	00				
	57A TRA	_	03465		PZE.	SOA				
	58A TSX	X .FWRD.,4	03466	74A	N D L					
03401	TXI	1 *+4112	03466		TSX	CALCOSIA				
03402	PZE	E 5811LK, UR	03467		ΪXΙ	#+2·13				
03403	<b>2</b> d		0.3470		PZE	75* 1, K . DR				
03404	PZE	-	03471		PZE	₽.				
03405		X .FFIL.,4	03472	!	PZE	××				
		_	03473		PZE	**				
03407 60	60A 15X	X .FWKD.,4	0.3474	76A	CLA	C•3				
			03475		STO	JUMP				
03411	976		0.3476	77A	512	- 1				
03412	PZE	ļ	0.3477	7AA	ST2	187				
03413	320		0.450.0	4 5 5	18	OUTPIT+1				
03414	TCX	}	0.5501	RIIA	CTA	*+3				
_	137 A14	630	0.4500		ž Ž	FXEM				
- 1			20000		70.	OF ALMOND				
٠.	62A 15X		0.000		7 t	144744				
03417	IXI	-1	03504		17	BUTTEROUR				
03420	PZE	-	03505		PZE	C.18				
03421	PZE		03206	LKein	PZE	**				
03422	PZE	2045	03507		9C1	1.OUTPU				
03423	Y0.		0 4510			44.4				
	\chi	A	0.00		YY	****				

THE FIRST LOCATION NOT USED BY THIS PROGRAM IS 03527.

ASSEMBLY LISTING

6каРНи 6каРНи

470			TOW YOU				
		SUBKOUTINE PRAM	PRAM				
			ENTRY	ENTRY POINTS			
PRAM SECTION	2						
SYSLOC SECTION	3		SUBROU'	SUBROUTINES CALLED			
		EFN	IFN	EFN IFN CORRESPONDENCE			
IFN LOCATION	TION	N.F.	IFN	LOCATION	FFN	1 FN	LOCATION

			NO.					
			ָלָבּי (בּילָבּיים) בּילָבּיים בּילָבּיים בּילָבּיים בּילָבּיים בּילָבּיים בּילָבּיים בּילָבּיים בּילְבּיים בּי	COMMON VAKIAMLES	ง			
	MOO	COMMON BLUCK	бкаРН <sub>О</sub>	ORIGIN	00001	LENGTH	00023	
SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
YMINO	00003	œ	PLT	90000	2 &	MAAO	70000	ĸ
XMAX1	COMMC	COMMON BLOCK	GRAPH1 XMTM1	ORIGIN	00024	LENGTH	00011	0
YMIN1	00003	×	DATE	00000	<b>X</b>	TVUL	3000	
			WIG	DIMENSIONED PROGRAM VARIABLES	RAM VARIABLES			
SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE	CVMBO	MOTATION	TYDE
PLDAT	00035	×					104	
			MIGNO	UNDIMENSIONED PROGRAM VARIABLES	RAM VARIABLES			
SYMBOL	LOCATION	TYPE	CHMAC	1 OCATION	TYPE	Can	MOTTAGE	TVBE
MODE	00005	<b></b>	LVAL	90900	1	KVAL	00607	1
PHI	00613	×	AR	00611	~	2	00612	-
				ENTRY POINTS	TS			
CA	CALCO4 SECTION	ION 4	CAL			CALC01	CO1 SECTION	NO NO
5	CALCO2 SECTI		CAL		ION 8			
				SUBROUTINES CALLED	5 CALLED			
PR			AXIS			SYMBOL		0N 11
NIS NIS	NUMBER SECTION SIN SECTION	10N 10N 15	LINE	E SECTION SECTION		PLOT PLOTS	SECTION	
23	CC.1 SECTION		CC+2 SYSLOC	g	TON 19 ION 22	E•30		
			EFN	IFN	CORRESPONDENCE			
EFN 12	IFN 70A	1 OCATION 01427	EFN 10	1FN 65A	LOCATION	M 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	IFN	LOCATION
4 م	ETHST 1 OCATION NOT 1.SET) HY THIS OBJECT	01475 SED RY T.	300		01626			01410

	DENS				STUNAGE MAP				
				SUBHOUTINE	DENSF				
		Ī		COMMON	10N VARTABLES	ËS			
	COMMON BLUCK	BLOCK	RECT		ORIGIN	10000	LENGTH	13565	
SYMBOL	LOCATION	TYPE		SYMBOL SQA	LUCATION 05672	TYPE R	SYMBOL	LOCATION 13564	TYPE I
RMAX	COMMON BLUCK	aLock R R R	DATA	7 2 2 1	0KIGIN 00023 00026	13566 R R	LENGTH ONDR EMU	00054 00024 00027	αα
MORUER	COMMON 00000 00035	표	HBANK	۲٥	ORIGIN U0007	13642 R	LENGTH	00441 00022	<b>cc</b>
STZM5 AMBUL	COMMON 00000 00000	BLOCK K	RbLK1	HPR I ME HU	OKIGIN UOUN1 UOOO4	14303 R R	LENGTH	00005 00002	<b>«</b>
		:		MIGNO	UNDIMENSIONED PROGRAM	RAM VARIABLES			
SYMBOL	LOCATION	TYPE		SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE R
RPEHDR	14310	x x		RAD.	14314	x x x	AMPDA	14315	cc cc
SNL AM1	14316	* * *		SNTHP	14322	   ∝ a	STEAM	14323	α α
CSTH1 STSL	14324	YY		ZM1	14330	4 02 0	7.W.Z	14331	ac ac
ZM3	14332	; **:		DIFF	14336	       	1 K L	14337	α α
DIHEIA	14340	ĽĽ		W1	14344	ac a	T17	14345	α α
ENF	14346	r r		ENXK OFN CO.	14352	c 0c 0c	F NX F ACTOR	14353	oc oc
PKFKAC	14357	e ne t		FRACIN	14360	. ∝ a	AY2	14361	α α
T31 COAM ST	14562 14365 14370	xxx		SIAMS	14366	æ	٦٥	14367	Œ
					ENTRY POINTS	TS			
DENSE	SE SECTION	9							
					SUBROUTINES CALLED	S CALLED			
SIN	SECTION 1 SECTION	7 10		COS	SECTION	TON 8 TON 11	TAN AL06	SECTION SECTION	ION 9

	DENS			STORAGE MAP	02/06/69 MAP			PAGE 63	
			FFR	IFN CO	EEN IEN CORRESPONDENCE				
EFN	IFN	OCATION	FEN	IFN	LOCATION	N	TEN	LOCATION	
04	21A	15117	14	23A	19151	118	2AA	15315	-
יטו	FORMAT	14437	12	46A	15452				
THE FIRS	ST LOCATION NO	THE FIRST LOCATION NOT HISED BY THIS PROGE	PROGRAM IS 1547						

COMMON BLUCK EXFLD COMMON BLUCK FAFLD COMMON BLUCK DATA RAIGH FOR PLUS COMMON BLUCK HBANK1 COMMON BLUCK GAUSS COMMON BLUCK GAUS	COMMON BLUCK FAFLD  COMMON BLUCK DATA  COUNDS  COMMON BLUCK DATA  COUNTY  COUNTY  COUNTY  COUNTY  COUNTY  COMMON BLUCK  COMMON B	BLES.	T	
COMMON BLUCK   FAELD	COMMON BLUCK FAFLD  COMMON BLUCK DATA  BMIL  UDU01  UDU02  UDU03  UDU22  UDU033  H  UDU22  UDU33  H  COMMON BLUCK GAUSS  COMMON BLUCK GAUSS  COMMON BLUCK GAUSS  COMMON BLUCK GAUSS  H  FITEN  COMMON BLUCK GAUSS  COMMON BLUCK GAUSS  H  TERM  TERM  TERM  TERM  TERM  TERM  TERM  TERM  TERM  TERM  TOWN		T 925 T 88 T 81 T	
COMMON BLOCK   CHAIN   TYPE   CYMPOL   LOCATION   TYPE   CYMPOL   LOCATION   CONTROL	COMMON BLOCK DATA BAIL  00000  COMMON BLOCK DATA BAIL  00011  00012  00013  COMMON BLOCK HEANK1  00041  00041  COMMON BLOCK HEANK1  00000  COMMON BLOCK GAUSS  COMMON BLOCK GASK  COMMON		T 42 II 85 H	
COMMON BLOCK   NATA   NOTICITY	COMMON BLOCK DATA PMAK 1 00000	00007 200007 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	76 E 88 11 21 E	
COMMON BLUCK   NATA   NATGIN   UNDOT   LEFGTH   ON054	COMMON BLOCK DATA RAIL  00003  00011  00012  00013  00041  00041  00041  00041  00041  00041  00041  00041  00041  00041  00042  00041  00041  00041  00041  00041  00041  00041  00041  00041  00003	00007 R R R R L 1 R R R R R R R R R R R R R R R R R R R	T 22 II 86 H	
U0000	00000 000000 00000000000 0000000000000	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	T	
00000b         K         FPLER         U00007         K         NOTE           00014         K         FPLS         U0015         K         THF7AO         00016           00014         K         FLUS         U0015         K         FPLS         00016           00012         I         U0020         I         U0016         K         FPL           00020         K         FL         U0020         K         FPL         00016           00033         K         FL         U0034         K         FL         00034           00041         K         FL         U0034         K         FL         00035           00041         K         FL         U0034         K         FL         00035           00041         K         FL         U0045         K         FL         00045           00044         K         FL         U0046         K         FL         00045           00044         K         K         FL         U0046         K         FL           00044         K         K         M         K         K         K           00040         L         K	00000 00011 00012 00013 00013 00013 00013 00013 00013 00014 00013 00014 00014 00014 00015 00015 00015 00015 00016 00016 00017	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	T 472	
000111 K PUS 00015 K PUS 00011	00011	x x + x x x x x x x + + + 5	T 22 H	
U0017   1	00017 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	H X X X X X X X H H	11 27 H	
DOUGUES   Fig.   DOUGUES   Fig.   DOUGUES	DOUGES   LOUGH   DOUGES   LOUGES   LO	x x x x x x x + + + 5	1	
COMMON BLOCK	COMMON BLOCK CKSK RCT  COMMON BLOCK CKSK RCT	. x x x x x x x x x x x x x x x x x x x	25.1 N.7.2 N.1.1 N	
0.00.33         κ         FH         0.00.34         R         COSPST         0.00.35           0.00.35         K         FH         0.00.37         R         R         COSPST         0.00.43           0.00.41         K         COOUNT         0.00.42         R         R         CCDV7         0.00.43           0.00.42         K         K         0.00.42         R         K         CONO.41         0.00.42           0.00.47         K         K         K         0.00.42         K         EMILIAT         0.00.43           0.00.47         K         K         K         K         K         K         M           0.00.47         K         K         K         C         0.00.43         LEMSTH         0.00.44           0.00.02         L         K         K         V         0.00.44         K         V         0.00.52           0.00.03         L         K         Y         0.00.04         R         Y         0.00.22         C           0.00.05         L         K         Y         0.00.04         R         Y         0.00.22         C           0.00.05         K         K         K <td>  DOUGO</td> <td>~ ~ ~ ~ H</td> <td>1 21 1</td> <td></td>	DOUGO	~ ~ ~ ~ H	1 21 1	
1000435	COMMON BLOCK GAUSS  COMMON BLOCK GAUSS	× × × × × × ×	2H #	
U00041	10041	× 22 == 1		
OUUUS	COMMON BLOCK HBANK1  000020	1		
COMMON BLOCK	COMMON BLOCK HBANK1  00000  1			1
COMMON BLOCK HBANK1 ORIGIN 00063 LENGTH 00441  00000  1 NUMALF U0001 I NOFWH 00002  00003 H YO U0007 R YO U0002  000035 I NOFWH 00002  000035 I NOFWH 00002  00000 H YO U0001 R ORDOR  00000 H RITH 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO ELT 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO ELT 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO ELT 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO ELT 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO ELT 00001 R ORIGIN 000533 I ENGTH 000013  00000 H YO TERM 00001 R F FM 000015  00001 H YO ELT 00001 R F FM 00005  00001 H YO FM INDIMENSIONED PROGRAM VARIABLES  LOCATION TYPE SYMBOL LOCATION 1 YPE SYMBOL 10CATION 00550  00550	COMMON BLOCK HBANK1 000003	2 7000		-
OUGDOU   I NUMALE OUGOT   I NUMBER OUGOS	00000	Canon		
U00005         H         YO         U0007         R         YD         00022           U00055         J         COMMON BLUCK         GAUISS         ORIGIN         ORIGIN         OR524         LENGTH         00007           U00000         H         FIT         U0001         R         NCPDP         00007           U00003         H         RCT         U0001         R         FM         00015           U00004         H         TERM2         00007         R         R         PMO           U0001         H         YO6         00012         R         RMO         00010           LOCATION         TYPE         SYMBOL         LOCATION         LOCATION         LOCATION           LOCATION         H         R RTF1T         U0552         R         YO4S         00550	00005 H YO 00035 I DCPL 00000 H H FIT 00000 H H FIT 00005 H H CKSH 00003 H H TERV 00003 H YOO	<b>4</b> }		
CUMMON BLUCK         GAUSS         ORIGIN         OR524         LENGTH         OR007           U0000         K         DCPUP         U0001         R         00002           U0000         K         F1T         U0004         R         00005           U0000         K         CKSK         Q0001         R         FM         00013           U0000         K         Z         U0004         R         FM         00015           U001         K         Z         Q0007         R         R         FM         00016           U001         K         Z         Q0007         R         R         FM         00016           U001         K         TERM2         Q0007         R         R         FM         00016           U001         K         TYPE         SYMBOL         LOCATION         TYPE         SYMBOL         LOCATION           U0546         K         R         R         R         TOCATION         TYPE         SYMBOL         LOCATION           U0545         K         R         R         R         R         TOCATION         TYPE         SYMBOL         LOCATION           U0550         <	COMMON BLUCK GAUSS 00000  COMMON BLUCK 00003  H 000003  H 1 ERW 1 ETT 1 ETT 1	~		
00000         κ         FIT         00001         R         ncpdp         00005           00003         κ         FIT         00004         R         nownTR         00005           00000         κ         R         S         nc0013         nc0013           00000         κ         TERM2         00007         R         FM         00016           00011         κ         TERM2         00012         R         RMD         00016           LOCATION         TYPE         SYMBOL         LOCATION         TYPE         SYMBOL         LOCATION           LOCATION         TYPE         SYMBOL         LOCATION         TYPE         SYMBOL         LOCATION           R         R         R         R         R         R         NO45         00550	00000	00524		<b>L</b>
COMMON BLUCK CKSK   CONTIGIN ON533   ENGTH ON013	00003 R CKSK CKSK COMMON BLUCK CKSK RCT C00003 R C C CMSK CCT C00003 R C CMSK CCT C00003 R C CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CCT CMSK CMSK CMSK CMSK CMSK CMSK CMSK CMSK	oc o		
COMMON BLUCK CRSR RCT 00001 R S S 00002  00003 R Z 00004 R FM 00005  00000 R TERM2 00007 R FM 00005  00011 R TERM2 00012 R FM 00010  1.INDIMENSIONED PROGRAM VARIABLES  1.INDIMENSIONED PROGRAM VARIABLES  0.0051 R FF1T 00550  0.0051 R FF1T 00552  0.00550	COMMON BLUCK CASK RCT R L L L L L L L L L L L L L L L L L L	×		
10000	TERV YOR	00533		
00010         H         TERM2         00007         R         RMCD         00010           00011         H         Y06         00012         R         R         RMCD         00010           01         LOCATION         TYPE         SYMBOL         LOCATION         LOCATION         LOCATION           01         LOCATION         TYPE         SYMBOL         LOCATION           01         LOCATION         TYPE         SYMBOL         LOCATION           00550         H         R RTF1T         00550         R         Y045         00550	R TERW	d ac		
0L LOCATION TYPE SYMBOL LOCATION TYPE SYMBOL LOCATION 0.00546 R RTF1T 00547 R YOUS 0.0551 R F1P	2	22 2		
OL         LOCATION         TYPE         SYMBOL         LOCATION           0.0546         R         RTF1T         0.0547         R         YO4S         0.0550           0.0551         R         F1P         0.0552         R         YO4S         0.0550	UNDIMENSIONED PRO	R ROGRAM VARIABLES		
00546 R RTF1T 00547 R Y04S 00550 00551 R F1P 00552 R	LOCATION TYPE SYMBOL L			
	00546 R RTF1T 00551 R F1P			

			COM	COMMON VARIABLES	£S				
	COMMON BLOCK	BLOCK	DATA	ORIGIN	0000	I ENGTH	00053		:
SYMBOL	LOCATION	TYPE	SYMDOL	LUCATION	TYPE	CYMBOL	LOCATION	TYPE	
TMT.	00000	נצ	RMI	10000	×	TMAX	00005	œ	
PRNI	00000	2 Y	A ≥ 00	00004	ox s	Z L Z d	0000	œ	
D G	00011	Ľ	ROFE	00012	χæ	40	00000	œ. c	
PHIO		<b>1</b>	P.U.S	00015	: 04	NFOWER	00016	۲ ا	
- CJ-1	7,000	<b>-</b> -	ת ת	02000	⊷ :	MUAR	00021	-	
DNDT	00025	· ~	7 C 3 C	00025	<b>x</b> a	UNDR	00024	œ i	
RIYSOH	00030	r	<u> </u>	0000	¥ a	E C	0.0027	oc o	
<b>1</b> 5	00033	r	I	00034	e a	130302	20000	z c	
SINPSI	00036	r	DEHUR	00037	<b>:</b> 2:	10400	04000	× o	
DCPUT	00041	r	DCPDY1	00042	2	DCDDX2	04000 4 0000	× •	
DCPUY3	44000	×	SP2	00045	: ac	FMITNI	0.00	ĸα	
EMUS	74000	r	Z	0000		- INC	00051	i 2 02	
MUFLAG	25000	-	1					: : !	
	NOMMON	HI OCK	HANK	2100		1	,		
MURDER		<b>-</b>	F IAHOM	10001	+cmn	LENGTH	000441		
HBANK		¥	NOEW	#U000	<b>.</b>	FINADO	20000	<b>→</b> a	
FINVPI	90000	r	γo	70000	· œ		22000	د <b>۵</b>	!
МА		7	ΥΡ	20000	ac			1	
	CUMMON BLOC	HLUCK	POWLOS	NTSINO	2021	n Const			
SA	00000	r	>	0000	200	באפום	0000		
DMDT	0000	¥	OMO	7:000	c a	X ( )	20000	ac c	
DMDY2	0000	r	DMD Y 3	20000	· œ	TSUMO	0000	2 0	
DWDDS1	00011	r	DMULR .	00012	æ	TOUMO	00013	: 02	
DMUDP DMUDP	00014	¥:	DMUDY1	00015	œ	DMI IDY2	00016	· œ	
FMCDIS	00000	ב	DMUDSI	00000	Я	FMD	00021	œ	
1	3200	•							
	COMMON BLUCK	BLOCK	CASK	OKIGIN	00540	HENGIH	¥1000		
	00000	¥	RCT	0000	æ		0000	œ	
TERM	50000	¥:	2	1000n	¥	Σ	0000	~	
RADI-	00000	נ	LEKM2	2000	2	DOMA	01000	œ	
2	77000	£	406	0.0012	œ				
V.Coulde	COMMON BLUCK	BLUCK	GAUSS	ORIGIN	00553	( ENGTH	0000		
W. B	00000	בן	DCPuR	00001	32	DCPDP	0000	~	
DEL 2S	00000	x x	F1T	#U000	œ	NWNTR	00005	œ	
	COMMON HLUCK	H, UCK	EXFLD	ORIGIN	00562	Hono	70000		
D2CY1R	00000	¥	D2SY1K	0000	œ	DSCYST	20000	0	
D2SY2I	00003	3	01:00		: :		1000	ť	

PAGE

69/90/20

SYMHOL	LOCATION	•						
	00570	R	SYMHOL	LOCATION 00601	TYPE R	SYMBOL	LOCATION	TYPE
			WIGNN	UNDIMENSIONED PROGRAM VARIABLES	AM VARIABLES			
SYMBOL	LOCATION	TYPE	SYMHOL	LOCATION	TYPE	CYMBOL	NOTTATOL	TYPE
AA2	00612	xχ	TERMC1	00613	œ	COSPS2	00614	æ
ENDASC	00620	2	XTFOM	00621	2 0	AA2C1	00617	œ (
FHCSP2	00623	æ	F2C	12900	ĸα	FINADA	00622	× a
P0	00626	x:	SIPo	26900	~	0000	00630	2 02
0110	00631	×	COTO	00632	2	402	00633	oc.
COPMP	00034	z a	SIP	00635	oc I	dWdIS	00636	æ
COTP	00642	2	SITU	04000	*	d	00641	œ
DRPUR	00045	×	DRPot	00646	د ۵	4000	0000	oz (
DRDRP	00900	×	OTORD	00651	2	00000	14010	* 0
DZMY1R	00653	×	DZMYZT	00654	: 02	dr. Amou	2000	K 0
DZAYIR	00656	Œ i	NZAYZI	00657	œ	n2AY3P	0000	2 02
DADIT	0000	<b>x</b>	DADY2	00662	R	DAPYS	00663	œ
<b>5</b> 2	10000	<b>x</b> a	DADI	00665	œ	DANP	99900	œ
DROCT	00000	<u></u>	DBDT	0.00	<b>B</b>	UBNP	00671	œ
DZMUSP	00675	< 32	DZMUSK	00673	oc a	N2MDST	900	œ
D2UUSP	00200	×	A STINGE	0000	2 0	Delinost	00677	<b>a</b>
DZUY3P	00703	r	YPEMOU	00704	r oc	VPSMOU	20700	× 0
YP3MOU	00200	æ	XTEM2	20200	œ	XTFM	00710	c oc
DIVORD	41700	2 2	DUDSRP	00712	R	DUYIRP	0n713	R
1	1100	<	DOTSRP	00715	œ	RDOTP	00716	œ
				ENTRY POINTS	.0			
POWERL	ERL SECTION	ION A						
				SUBROUTINES CALLED	CALLED			
NIS		6 101	503			1000		
MIN	/ SECTION	10hi 12	SYSLOC	OC SECTION	N 13	NAC:	SECTION	11
			EFN	IFN CORRES	CORRESPONDENCE			
EFN	IFN	OCATION	FFN	IFN	LOCATION	FFN	IFN	LOCATION
	118	00/37	501	2A	01002	502	3.4	01006
504	16A	01101	<b>2</b> 0	5A 17A	01010	503	10A	01045
	21A	01153	506	22A	01167	507	LYA	01141
508	24A	01235	509	25A	01323	510	2 6 A	01330
110	29A	01542	512	30A	01344	513	31A	01442
	35A	01000	515	33A	01640	516	34A	01720
520	38A	02044	521 521	39A	02030	519	37A	02041
	* * * *				O + 1 4 5	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	9	

PAGE		02653		
		47A		
		52P		
69/90/20		02650	03010	:
	STORAGE MAP	464	46 A	2.
		527	530	S PROGRAM. IS 03032
		02603	02671	THE FIRST LOCATION NOT USED BY THIS PROP
	POWER	444	48A	SI LOCATION N
		5. 526	529	THE FIRS

CO SYMBOL LOCATION RMAX 000003 TMIN 00003 TMIN 00011 PHIO 00011 PHIO 00017 TMIN 00022 DNOT 00017 TMIN 00025 DCPDT 00041 DCPDT 000009 HBANK 000003 DCDT DCPDT 000009 DCDT DCPDT 000009 DCDT DCPDT 000009 DCDT DCPDT DCPDT DCPDT DCDT DCDT DCDT D	COMMON BLOCK ON TYPE AR AR AR AR AR AR AR AR AR AR AR AR AR A	SUBMOUTINE  COMMON  DATA  SYMBOL  RMIN  PMAX  RELERR  RO	FORCE				
LOCATI 00000 00011 00011 00012 00025 00025 00041 00041 00041 00041 00041 00041 00041	NOWW	SYMBOL RMIN PMAX RELERB RO					
LOCATI 00000 000014 00014 000176	7		10N VARIABLES	Ş			
00001 00001 00001 00011 00011 00012 00012 00013 00014 00014 00014 00014 00014 00000		SYMBOL RMIN PMAX RELERR RO	ORIGIN	00001	LENGTH	00053	
00001 00011 00012 00012 00012 00013 00014 00014 00014 00000 000003		PMAX PMAX RELERR RO	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
00011 00011 00011 00012 00025 00025 00041 00041 00041 00065 00065		RELERR RO	10000	œ (	TMAX	00005	œ
00011 00014 00017 00025 00035 00041 00044 00044 00065 00000		RO	0000	ox o	Z Z	00000	o <b>∠</b> o
00014 00025 00025 00025 00035 00047 00044 00000 00000			00012	2 02	THETAO	00013	2 02
000022 00022 00022 00023 00023 00044 00044 00000 00000		PLUS	00015	œ	NPOWER	00016	۲ 🛏
00025 00044 00044 00044 00044 00000 00000		ئ آ	00020	<b>⊢</b> (	NUAR	00021	⊷ (
00030 00033 00044 00044 00044 00044 00000 00000 00000		OND	00000	20	HOND	00024	~
00033 00041 00044 00044 00064 00000 00000		1011	00031	< 0°	2 C	72000	× 0
00000 000041 00044 00044 00000 000000 00000000	x x x -	Æ	00034	~	COSPSI	00035	ac
00000 00000 00000 00000 00000	x	DFHUR	00037	R	DEHDT	00000	œ
000000	x -	DCPDY1	00042	œ	DCPDY2	00043	œς
00000	۲ -	245	00045	æ	FMUINT	94000	œ
00000 00000 90000 90000		z	00020	1	GNT.	00051	œ
	COMMON BLOCK	HBANK1	ORIGIN	00054	FNGTH	00441	
	⊶ oc	NOHALF	10000	м	NOTON	00005	
	æ H	۲٥	20000	α	AD VD	00022	× «
		UNDIME	UNDIMENSIONED PROGRAM VARIABLES	AM VARIABLES			
SYMBOL LOCATION YNRMLZ 00515	N TYPE	SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
			ENTRY POINTS				
FORCE	SECTION 4						
			SUBROUTINES CALLED	CALLED			
SYSLOC SE	SECTION 5					-	
			ł				
		EFN	IFN CORKES	CORRESPONDENCE			
EFN IFN 100 1A	L OCATION 00522	EFN 101	IFN 2A	LOCATION 00525	FFN 102	IFN	LOCATION

			SUBROUTINE COL	כסרר				
i i			DIME	DIMENSIONED PROGRAM VARIABLES	AM VARIABLES			
SYMBOL A D	LOCATION 00001 00020	TYPE R R	SYMHOL	LOCATION 00007	TYPE R	ZY#BnL	LOCATION DOD15	TYPE R
	-		LINDIME	UNDIMENSIONED PROGRAM_VARIABLES	AM VARIABLES			
SYMBOL X S	LOCATION UOU23 UOU26	TYPE K K	SYMAOL COEFF E	LOCATION 00024 00027	TYPE R R	SYMBOL	LOCATION 00025	TYPE
	:			ENTRY POINTS	5			
COLL	SECTION	2						
			!	SUBROUTINES CALLED	CALLED			
SYSLOC	SECTION SECTION	<b>6</b> 3	503	SECTION		SIN	SECTION	ON N
			EFN	IEN	CORKESPONDENCE			
Ž	JEN	OCATION	FFN	IFN	LOCATION	FFN	IFN	LOCATION
		00056	5	4 4	00062	<b>د</b> ۲	7.A 11.A	00076 00131
!		70007	50 42	40	00151	45	17A	00226

SYMBOL LOCATION TYPE  A6 00015 R  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  SYMBOL LOCATION TYPE  R  SYMBOL LOCATION TYPE  SYMBOL TYPE  R  SYMBOL LOCATION TYPE  R  SYMBOL LOCATION TYPE  R  SYMBOL TYPE  R  SYMBOL LOCATION TYPE  R  SYMBOL TYPE  R  SYMBOL LOCATION TYPE  R  SYMBOL TYPE  R  SYMBOL LOCATION TYPE  R  SYMBOL TYPE  R	SUBMOUTINE DIMER SYMBOL A2 OP OP SYMBOL NN CN CN CN CN CN CN CN CN CC CC CC CC	DIMENSIONED PROGRAM VARIABLES OLOGATION TYPE OLOGATION TYPE OLOGOS R OLOCATION TYPE OLOGOS I OLOGOS I OLOGOS R	AM VARIABLES TYPE R R TYPE I I R R R R R R R R R R R R CALLED	SYMBOL AM SOLD FRROR NNN P P A XSO SS	LOCATION 00011 00027 00035 00035 00043 00043 00046 000946	7 PE
HOL   LOCATION   TYPE	Bot Lun	ISTONED PROGRA  LOCATION  00021  LOCATION  00024  00034  00037  00042  00045  00050  00055  SUBROUTINES	AM VARIABLES TYPE R R TYPE TYPE TYPE TYPE R R R R R R R R R R R CALLED	SYMBOL MM POLD FRROR NNN P 0 A XSA SS	LOCATION 00032 00032 00035 00040 00040 00043 00046	14 PE
BOL   LOCATION   TYPE		LOCATION 00021 00021 LOCATION 00026 00034 00037 00042 00045 00045 00050 00050 00050	TYPE R R TYPE I R R R R R R R R R R R R R R R R R R	SYMBOL SYMBOL MM POLD FRROR NINN P A XSA SS	LOCATION 00011 00032 00032 00035 00040 00043 00043 00043	1
CSINT   SECTION   COATION   TYPE   COUNTY   CO	1   1201 34   157	LOCATION PROGRA LOCATION LOCATION 00034 00042 00045 00045 00045 00053 ENTRY POINTS	M VARIABLES  TYPE  I R R R R R R R R CALLED	SYMBOL MM POLD FRROR NNN P P P P SS	LOCATION 00022 00032 00035 00040 00043 00046 00051 00051	x
CSINT   SECTION   TYPE   COATION   TYPE   COUGH   R   COUGH   R   COUGH   R   COUGH   R   COG		ISTONED PROGRE  LOCATION  00026  00034  00037  00045  00045  00050  00050  SUBROUTINES	M VARIABLES  TYPE I R R R R R R R R CALLED	SYMBOL MM POLD FRROR NNN P XSA XSA	LOCATION 00027 00032 00035 00043 00043 00046 00051 00054	} 
DL LOCATION TYPE 00025	SYMBOL M BOEX SGN NN CN PPP TERM	LOCATION 00026 00034 00034 00032 00045 00045 00050 00050 00053 SUBROUTINES	TYPE I R R R R R R CALLED	SYMBOL MM POLD FRROR NNN P A XSA XSA	LOCATION 00027 00032 00035 00043 00043 00046 00051 00054	<u>γ</u> π α α μ α α α α
CSINT SECTION  TOR SECTION  SIN SECTION  F, 3 SECTION  F, 3 SECTION  F, 3 SECTION  F, 3 SECTION  F, 44 00354  H 00354	M SOOFX SOON NN NN CN PPP TERM	00026 00034 00034 00042 00042 00045 00053 00053 SUBROUTINES	R R R R R R R CALLED	POLD FRROR NNN P D XSS	00027 00035 00035 00040 00043 00043 00051 00051	<b>→</b> α α <b>α</b> α α α α
CSINT SECTION  CSINT SECTION  CC.2  SYSLOC  SYSLOC  SECTION  FONV.  SECTION  SECTION  SECTION  SECTION  SECTION  SECTION  A 44 00354  344 00354  345 00354  374 00351	SGN NN CN CN PPP TERM	00034 00034 00042 00042 00045 00050 00053 ENTRY POINTS	CALLED	FRODE NNN P P S S X S S S S S S S S S S S S S S S	00052 00035 00040 00046 000951 00051	<b>x</b> α ≈ α α α
CSINT SECTION  100030 100044 1000047 1000047 1000047 1000047 1000047 1000047 100047 100044 1000041 100044 1000041 100044 1000034 100044 100034 100034 100044 100034 100034 100044 100034	ON CN CN CC TERM	00037 00042 00045 00050 00053 ENTRY POINTS	R R R R CALLED	S S S S S S S S S S S S S S S S S S S	00000 00046 00046 00051 00051	c ⊶ αc αc αc αc
CSINT SECTION  TOR SECTION  SIN SECTION  SIN SECTION  SIN SECTION  SA 00358  34A 00358  34A 00358  34A 00358  34A 00358  34A 00358  34A 00358  34A 00358  37A 00351	CC TERM	00042 00045 00045 00053 00053 ENTRY POINTS	R R R R CALLED	e S X S S S S	00043 00046 00051 00051	αα α α
CSINT SECTION  TOR SECTION  SIN SECTION  F.3 SECTION  F.3 SECTION  F.3 SECTION  CC.2 SECTION  CC.2 SECTION  CC.2 SECTION  A44 00359  444 00354  344 00354  344 00354  348 00173  528 00123  28 00173  537 00351	TERM	00050 00053 ENTRY POINTS	R R R	S X	00054 00054	- α α
CSINT SECTION  TOR SECTION  ALOG SECTION  F.3 SECTION  F.3 SECTION  CC.2 SECTION  CC.2 SECTION  CC.2 SECTION  TFN 1 OCATI  A44 003554  A44	3	00053 ENTRY POINTS SUBROUTINES	CALLED	SS	45000	œ
SECTION SECTIO		SUBROUTINES	CALLED			
F SECTION  SAA  003505  28A  00253  28A  00251		SUBROUTINES	CALLED			
SECTION SECTION SECTION SECTION SECTION SECTION SECTION SECTION SECTION 444 00359 344 00350 344 00350 354 00331 284 00331						
7. SECTION SECTION SECTION SECTION SECTION SECTION SECTION 1 00120 444 00354 344 00373 284 00231 374 00311	*KP3*		3	802		2
1. SECTION SECTION SECTION SECTION 2. SECTION 2. 00120 444 00354 444 00355 344 00355 224 00173 28 00233 28 00233	- FWRD.	SECTION		EXIT	SECTION	
SECTION  SECTION  SECTION  15N 1 00120  44A 00354  34A 00354  34A 00354  34A 00354  34A 00354  34A 00354  34A 00354  34A 00354  34A 00351	onno•			6-3	•	
SYSLOC SECTION SYSLOC SECTION SYSLOC SECTION TO TO TO TO TO TO TO TO TO TO TO TO TO T	i di		10 10	1.00		12 N
1FN 1 2A 44A 344A 32A 22A 378	ۥ30			7.00		
1FN 2A 444 344 344 228 284 378 378 378 378 378 378 378 378 378 378	EFN	IFN CORRES	CORRESPONDENCE			
	EFN	IFN 44	LOCATION	FFN	IFN	LOCATION
	<b>t</b>	6A	00130	50	7A	00140
	21	13A	00170	30	23A	00235
	1 15 11 15	18A	00214	- 22 - 22 - 4	20A	00230
	34	30A	00275	3.6	33A	00303
	42	40A	00333	500	80A	00664
401 46A 00357 1000 FORMAT 00107	405 407	¥ 60 4	00370	604	51A	00374
53A	5002	V + P	00672	404	544A	00420
	420	57A	94400	Uth	77A	00662
61A	430	68A	00564	422	63A	00472
	777	74.5	00000	405	Ac.	00057

PAGE	00672 00716 00762
	85A 98A 103A
	5005 5008 5011
69/90/c0 b	00671 00701 00742
STORAGE MAP	83A 90A 102A
	5u3 5007 5u1u
	00700 00700 00730
150	82A 86A 99A
	501 5006 5009

THE FIRST LOCATION NOT USED BY THIS PROGRAM IS 01024.

				STORAGE MAP				
			SUBROUTINE	E POLAR				
			COM	COMMON VARIABLES				
-	COMMON BLOCK	LOCK	DATA	ORIGIN	10000	I_ENGTH	9000	
	LOCATION	TYPE	SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
	00003	×	PMAX	0000	× α	DMTN	00005	2 02
	90000	×	RELERR	20000	: œ	Φ	00010	œ
	00011	rχ	R0 P1 15	00012	oc 0	THETAO	00013	α-
	00017	_	7	00000	1	NUAR	00021	-
	00022	-	EN	00023	R .	DNDR	00024	œ
	00025	×∝	doNo u	00026	oc oc	E ou	00027	OC OX
	00033	×	ī	95000	~	COSPSI	00035	. ~
	00036	<b>x</b> 3	DEHOR	00037	2	DEHDT	00000	œ
	15000	<b>x</b> x	SP2	00045	ox ox	FILTINE	00043	or or
	100047	œ ~	2 4	00050		ONC)	00051	œ
	COMMON BLOCK	LOCK	HBANKI	ORIGIN	00055	LENGTH	00441	
	00000	⊶ x	NOHALF NOE	00001		MODOUB	00002	⊷ œ
	00000	r	۲٥	20000	~	V.	00022	00
	00035	1						
	COMMON BLOCK	LOCK	CRSR	ORIGIN	00516	LENGTH	00013	
	00000	××	RCT 7	10000	oc o	v į	00002	oc o
	00006	×α	TERMS	00007	oc 0	PMOD	00000	ac ac
				21000	¥			
			MIGNO	UNDIMENSIONEN PROGRAM VARIABLES	VARIABLES			
SYMBOL L	Z	TYPE	SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	TYPE
	00536 00541	× ×	7.1 Y.1 Y.14	00537	<i>ع</i> مر	۸۲۶	00290	׿
				ENTRY POINTS				
POLAR	SECTION	ro.						
				SUBROUTINES CALLED	ALLED			
CSORT	SECTION	9	. CFDP		^	. CFMP.		a 2
CABS	SECTION	6.	ATANZ	42 SECTION		1.1	SECTION	
2751 00	SECTION	15.	E.3			F.	SECTIO	

	POLA			STORAGE MAP	02/06/69 MAP.		:	PAGE
			EFN	IFN CO	EFN IFN CORRESPONDENCE			
EFN	EFN	NO	EFN	IFN	LOCATION	FFN	IFN	LOCATION
101	2 A	00016	102	<b>4</b> †	00717	103	٧9	00724
THE FIR	THE FIRST LOCATION NOT USED	THE FIRST LOCATION NOT USED BY THIS PRUGRAM IS 00753.	PROGRAM IS 0075					

LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   TYPE   TY		THE RESERVE AND VALUE OF THE PERSON OF THE P		ST	STORAGE MAP	d.					
LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   TYPE   SYMBOL   LOCATION   SECTION		FUNCT		OR	TYPE	2					
LOCATION   TYPE   SYMBOL   LOCATION   R	A TANK OF THE PROPERTY OF THE		5	DIMENSIC	ONEN PRO	RAM VAR	IABLES	1		;	
SECTION   2   SUBRAUTINES CALLED   SUBRAUTINES CALLED   SUBRAUTINES CALLED   SUBRAUTINES CALLED   SECTION   4   SQRT   SECTION   5   E.3   SECTI	LOCATION	TYPE	SYMBOL X	:	OCATION 00002	TYP		SYMBO	:	ATION 003	TYPE R
SECTION   2   SUBRAUTINES CALLED   SUBRAUTINES CALLED   SUBRAUTINES CALLED   SGRT   SECTION	#0000	_									
SECTION 2   SUBROUTINES CALLED   SUBROUTINES CALLED   SECTION 4   SORT   SECTION 5   SECTION 10   SECTION 10   SECTION 10   SECTION 10   SECTION 10   SECTION 10   SECTION 10   SECTION 13   SECTION 13   SYSLOC   SECTION 14   SECTION 15				Ē	NTRY POIN	CTS					
SUBRAUTINES CALLED	SECTION										
SECTION         4         SQRT         SECTION           SECTION         6         6.2         SECTION         7         6.3         SECTION           SECTION         10         CC.2         SECTION         10         CC.2         SECTION           SECTION         12         CC.4         SECTION         13         SYSLOC         SECTION           FFN         10CATION         FFN         FFN         FFN         FFN         FFN				35	JBROUTINE	S CALLF	0				
SECTION         10         CC.2         SECTION           SECTION         13         CC.4         SECTION           SECTION         13         SYSLOC         SECTIO           FFN         IFN         CORRESPONDENCE           IFN         LOCATION         FFN         IFN				EXP E.2	SECT	TON	7		S@RT E.3	SECTION	r co
EFN TOPRESPONDENCE 10CATION FFN IFN				CC • 1 CC • 4	SECT SECT	10N 10N	10 13		CC.2 SYSLOC	SECTION SECTION	11 14
OCATION EFN IFN LOCATION FFN IFN					i	FSPONDE	CE	-			and the second s
		OCATION	EFN	11	z	LOCAT	NC.	N d d	IFA		CATION

			SUBROUTINE MINY	ANTW							
			DIME	NSIONEN	DIMENSIONEN PROGRAM VARIABLES	RIABLES					
SYMBOL IPIV	LOCATION	TYPE	SYMIOL	LOCATION		TYPE	SYMBOL	LOCA	LOCATION	TYPE	
		:	HINDIME	NSIONEN	HINDIMENSIONEN PROGRAM VARIABLES	RIABLES		# # # # # # # # # # # # # # # # # # #			
SYMBOL	LOCATION	TYPE	SYMBOL	LOCATION	t	TYPE	SYMBOL	LOCATI	OCATION	TYPE	:
I d I	20000	-		00010			TPU	00011	11		
IFMAX IPN ICOPI	00012 00015 00020		TEMP ICOMP	00013	<b>K H</b>		TPTVI	00014	14 17	<b>.</b>	
				ENTRY POINTS	POTNTS						
NIN	SECTION	α				:		:			
				Subkou	SUBROUTINES CALLED	ED					
E-1	SECTION		E . 2	•	SECTION	<b>‡</b>	tu.	F.3	SECTION	ď	
E.4	SECTION SECTION	<b>1</b> 00	1.00 00.1	<b>-</b> -	SECTION SECTION	10	Σ (vi	CC.2 SYSLOC	SECTION		
			E E	HEN	CORRESPONDENCE	ENCE					
EFN	IFN	1 OCATION	E FN	IFN 524	LOCA	LOCATION	11 L	TFN		LOCATION	
		00136		50A	002	55	α	444		00245	
	H0A	10551	10	78A	003	7,5	11	72A		00337	
	114A	27400	13	1064	00420	50	14	91A		00412	
	104A	9440	1º	98A	00436	36	17	109		10464	

AG		K20000
2/17/69 P		S SM
02/11/69		02/11/69
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02/17/69		RUNGE-KUTTA, ADAMS-MOULTON INTEGRATOR PACKAGE SEQUENCE MANK, PROS DERI, PHI, DER2 ETUKN BJJ, YJ L L L L L L L L L L L L L L L L L L L	YDUT Y (2) Y 0 (2) E UBAR HMAXT HMINT YCL OW KGERR 50	14:4 AEOS;4 AEOS;4 AEOS;4 14:1 0:2 0:2 0:2 0:2 1:4;1 1:4 1:4 1:4 1:1:5 1:4 1:1:5 1:1:1:5 1:1:1:1	L(12),1 U) STORF ( L(M) IN MARK M) 1 *+1:1,-1
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.02/11/69	M+2 TN ADD N IN DECRE N IN DECRE	N IN DECRE SHOULD BF ASSEMBLED AS AND AFLAG PZE FLAG'4 ASET NOW CONTAINS NOP	FIND MARK END OF TRIGGFRS
	## = 3,2,1 ## 2 ## 1,2 ## 1,1,2 ## 1,1,4 ## 1,2,1 ## 1,2,1 ## 1,2,1 ## 1,1,4 ## 1,1,4 ## 6,2,1 ## 6,2,1 ## 1,1,4 ## 6,2,1 ## 1,1,4 ## 6,2,1 ## 1,1,4	*+1'2'1  **1  DELZ+1'2'  *+1'1'*  *-3'2'1  2'2  **1  YNZ+1'2  *+1'1'*  *+1'1'*  *+1'1'*  *HOD'?  HAOD'?  HAOD'?  HAOD'?  HAOD'?  ASET PZE SET'4  ASET PZE SET'4  ASET PZE SET'4  ASET PZE SET'4  ASET PZE SET'4  ASET PZE SET'4  ASET PZE SET'4	BMIN TRIGO+1 HA11 **1 **1 TMIN2 TRIGO+1 IM:1 IM:1 HA10
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02/17/69	SKIP NEGATIVE TRIGGERS SET DEP. VAR. FLAG IF INDEPENDENT VARIABLE. JUMP ASET NOW CONTAINS TSX AFLAG NOW CONTAINS TSX	71(1)	T2(1)  T1(1)  T1(1)-TMIN=+*CONTTHUE SFARCH  T1(1)-TMIN=0.CHFCK IMIN2 IF P=1  T1(1)-TMINN=-*RFPLACE TMIN AND TMIN2	P=0, CONTINUE SEARCH	NEW TMIN TMIN2. CONTINIE SFARCH P=0.CONTINUE SFARCH T2(1)	T2(1)-TMIN2=+, CONTINUE SFARCH T2(1)-TMIN2=-, RFPLACE TMIN2 CONTINUE SEARCH FIND MARK	PHI IN T(TEMD)
	151 **2 1X1 HAU4.12 PDX 1.2 1XL **5.2.0 CLA HAI3 STD AFLAG 1X1 HAU4.12		PA		STO TMINE IXI HAU4.11-2 NZI P TXI HAU4.11-2 CLA* HAU6.		STZ
	н,11	HA05	n	3	¥ −	- v > v > v -	ηναν σναν
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	SET C(AEOS)=NOP			EOSTA (AEOS)	C(AEOS)=TSX ***4	A(AEOS)=NEW FOS		PHI TN A(TEMP)		PHI UNCHANGED	PHI AND RESTART	DICK LED N. (N.)		(N) DIGGED, DECTABL	(N) UNCHANGED, CONTINIE		DELA ADIRESSES FOR NEW		Ž	P													O L	F			
HA12	AEOS	AFOS.2	*+17.5.**	TACO. VAL	AEOS	AEOS	AFOS FEED	15 TEMP	• • • • • • • • • • • • • • • • • • •	FH1 HA16	RSTRT	(¥)	1.8	(N)	*+9	(N)	ADDK:4	(E)	I.	(E)	Į.	I œ		(E)	*+1,1,1,-1	È C	Q Q	18	(¥)	t 0.4 # #	***1	Z = 1	<b>-</b> a	UELU	# OF	50	7***
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PAGE	MARK1517 MADVOES	MARK 1519	MARK1520	MARK 15/01 MARK 15/01	MARK 1523	MARK 1524	MARK1525	MARK 1527	MARK 1528	MARK 1529	MARK 1531	MARK1532		MARK1533	MARK 1554 MARK 1515	MARK 1536	MARK 1537	MARK 1538 MADV 6 5 3 0	MARK 1540	MARK1541	MARK 1542	SANCE MARKED THE STATE OF THE S	MARKJS45	MARK 1546	MARKING	MARK1549	MARKISSO MARKISSI		2 A B B B B B B B B B B B B B B B B B B	MARK1553	MARK1554	MADY AND	MARK 1557	MARK 1558	MARK1559	MADK 1560	MARX 1560	MARK 1563	MARK 1564	MARK JUDU	MARK 1567
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02/17/69			EDOM DIFFERENCES									R1=(N)															
02/1	(N)*1 DELY*2 YDOT KUP1,1*1 UPDAT*4	KUP2,2,1 KUP0,2,0 **,4 **,1	***2	יר	KIKS+1,1	RIRS+2.2	12.2	MP1 RSUM1	RSUM2-1	KSUM3	RADUS-112 RSUM4	्र इ	D.2 RSUM6,2	Appears of the second of the s	0.4	1,5 DELX-1,2	DELXIO	KSUM6.2.1	RSUM3.2.**	X:00=0.K	KSUM6,2	RSUM1.1.1	<b>#**</b>	***************************************	1.4	N. O.	KSUM2-1
:	RUPO LXA RUPI CLA* STO* ITX ISX	RUPZ TXL RUP3 AXT AXT	AXI AXI URI A	TSX NORMAL	RSUM SXA	NZT	IRA	CLA STA	STA RECHICLA		i	STA RS	KSUMI AXT		AXI		KSOM4 FAB*	!	KSUMo TXL	TXD	nxs	11A	RIRS AXI	AXA		KEU CLA	S S T S
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	03401 03402 03403 03403 03404	03406 03407 03410 03411	BINARY CARD U3412 U3413		03414	03416	03421	03423	03429	03426	また	03431 03432	03433 03434	BINARY CARD	03435	03430	034¢C	03442	03443	03445	03446	03450	03451	03452	#S#£0	03455	03457

BINARY CARD (NOT PUNCHED)

MARK1669 MARK1671 MARK1671 MARK1672 MARK1673 MARK1673

MARS
ASSEMBLFU IEXT.
U346U 0774 UN 2 0000N
U3461 0020 UN 0 0 03425
U3462 0 0000N 0 00274
U3463 0 0000N 0 00273
U3464 0 0000N 0 00273

259

NAKY CAKD	BINARY CAKE (FIOT PUNCHED) 00346500000		PKEFAUF	SYART=0,LENGTH=1845,TYPE=7094,CMPLY=6
	00000400000 442151626060	MAKS	DECK	
	003465000000 442151426060	MAKK	REAL	SECT. 21LOC=0.LENGTH=0
	00000000000 302560606060	Ę.	REAL	SECT 31.00=165/LENGTH=0
	00000000000000000000000000000000000000	r Z	R <sub>E.</sub> AL	SECT - 4, LOC=166, LENGTH=0
	000000000166	0	R. A.	SFCT - 5,1.0C=173,LENGTH=0
	000000000000000000000000000000000000000	2		
	7060606060	<b>&gt;</b> -	REAL	SECT: A,LOC=223,LENGTH=0
	702446636060	YDOT	REAL	SECT 7.LOC=224.LENGTH=0
	0000000000224 700102016060	Y121	REAL	SECT. R.LOC=225,LENGTH=0
	000000000025	,	R. A.	SFC1 - 0, LOC=226, LENGTH=0
	000000000000000000000000000000000000000	2	<b>j</b>	
	700001020160 000000000227	10121	REAL	SECT. 10.LOC=227.LFNGTH=n
NARY CARD	BINARY CARD (NOT PUNCHED)			
	256422215160	LIBAR	REAL	SEC1 - 11.LOC=326.LENGTH=0
	000000000326 25432215160	ELBAR	REAL	SECT. 12.LOC=327.LENGTH=0
	000000000327			
	304421676360	HMAX	REAL	SECT - 13, LOC=330, LENGTH=0
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	00000000331		i .	
	702343466660	YCLOW	PLAL	SECT. 15.LOC=332.LFNGTHEN
!	512725515160	RGERH	REAL	SECT. 16.LOC=1671.LENGTH=0

NO MESSAGES FOR THIS ASSEMBLY

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MARSOND3

HEFERENCES TO DEFINED SYMBOLS.

00414 160,637,703,731,776,1114,126,7,1540			00216 2.5524,530,532,533,655,664,1043,1533,2550			015/6 14/2/12/4/12/5/10/14/5/			00255		00273 301:1312:1405:1510:1571:1572:1623:1705:2526:2534:2714:3061:3161:3264:3354:3437:3440:344:	00307 371•3062•3124•3125•3160•3328•3402	_	_	-	•		_	00251 53,61,74,107,112,136,374,1262,1306,1315,1350,1413,2667,2673,244,3030,3064,3120,3141,3145,			• •	_	01667 1532:1376:1600:1704	-			_		•	:		-						•	_	11046 1125511033	_		_	<b>3.5023 1.5647.25467.30167.30167.30</b>	7	0.0572 415	
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| 0,71,644,646,66,106,1134,1152,1273,1453,1454,1470,1500,1552,1631,1725,2450,2773,3035,3102,
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126+765+1451+15,5+3u55+3101+3166
1062+2426+2434
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437,445,461,467,4/2,4/4,500,504
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HA11
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     110 U4
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SYMBOL REFERENCE DATA

MAXS

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2455*2460*2462
3242*3244*3246*3250*3251*3252*3253*3255*3257*3272*3274*3274*3374*3303*3306
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2454-2461-2461-2510-2513
2442-2443-2444
                                            3402+3204+3411+3212+3213+3214+3216+3260+3271+3305
2456+2464+2465+2474
1326+1476+3332
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3201,3267
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1335,1440
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101115,1441,1443,1445,1463
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2447;2457;2472;2473;2536
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3424, 3237, 3326, 3330
3337, 3343
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3414,3415,3416
3155
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2452,2503
2475,2500,2501
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1530,3105,3167
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MARS SYMBOL REFERENCE DATA

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0/1142/1210/1235/1321/1544/1367/1407/1525/1556/2542/2777/3011
0/354/1205/1216/121//1225/1226/1231/1323/1346/1370/1406/1410/1411/1530/1570/2540/3000/3013
0/1422/1425
                                                                                                                                                                                                                   0+1141-1211-1230+1343+1420+1526+1560+1561+1632+1637+2543+2775,3012
0+1234+1237+1340+1251+1557+1562+1635+1640+2544+2776+3014
34+334+545+550+1140+1145+1310+1342+1366+1403+1417+1512+1551+1567+1616+2522+2665+2774+3010+
3457+3110+3220+3401+3432
60+677215+1537+276+2771+3050+3051+3106+3170
65+422+424+431+3053
2555+2423
                                                1337,2760,3405
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MARS SYMBOL REFERENCE DATA

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		(CFD)	03563 17405	/(03561) /(17416)	(03566) 26606	31012	/(21505)	(98880)/	(03566)				37752	40372 *	42040	4717 * 44274 *	44323	44360 *	44422 *	,	47145 *	47415 *	
		*=NOT PEFERENCFD)	/EPSTN / /Rnots /	/NFW /(03561 /GPAPH1/(17416	/GAUSS /(03566) OUTPUT 26606	CALCO1	/RALK1 /	/CRSR /	/6AUSS /(03566)				140	<b>&gt;</b>	RGERR	-1 XCA!	. PFAD	. I AREA	L UNBI	; >	-I. XMOP	OVFLOW	;
		OVFD+ *EN	03561 03620	21470 * (17407) (17426)	/(n4546) /(174A5)	30734	(83105)	7(03566)	7(03546)		36541		37745		40376 *	43714	44305	44347 *	44414	) !	* 50127	47176 47351 *	
		. "LOC" = MOVFD.	/NFW /	/CONST /(17407) /GRAPHn/(17426)	/CRSR / /Rnots /	CALCOS	/HRANK1/(03105	/6AUSS /	/CPSR /		POLAR		TRA24	160	YO121 YCLOW	LXFR9	PPFN-	PELES	. AREA1	1111	IVOX 1.	.t.TCH /.COUNT/	1
		(/NAME/=NON D LENGTH, (LOC)=DELETED,	03546 03575	17426 (03546) 21505	/(03105) /(03620) /(17407)	30656	7 (03031)	(03105)	(03525)	34774	(03546)	ı	37740	_	40375 *	43705 44101 *	44304		44411 *	c † †	47043 *	47175 *	-
		6TH+ (LOC	/CRSR / /POWLOS/	/GPAPHO/ /CRSR / /KRLK1 /	/HRANK1/(U3105) /KECT /(03620) /CONST /(17407)	CALCO4	/UAIA /	/HRAMK1/(03105)	/POWLOS/(03575)	FORCE	/cPSR /		TRA14	NT IN	YO	·LXOUT	-LUNB	. PEAUR	.RLHLD	•	.LXTST	LXFLG FPARG	) [ 1
02717	65771	MOM O LEN	<b>U3105</b> <b>U356</b> b	1/ 17416 1/(03105) /(03565)	/(03031) /(03031) //(21512) //(17416)	(17416)	31020 (17426)	/(03031)	(03105)	(03105)	(03105)	•	(37535)		40374 *	43637 43717 *	44505 *		44401 *	44460	47040	47174 *	1
HAU	[HKI]	(/NAME/=	/INBANK1/		INF(1) 23676 /UA1A /(U3U31) /GRAPH2/(21512) /GRAPH1/(17416)	/oRAPH1/(17416)	CALCOS 31020 /GRAPHO/(17426)	/DAIA /	/HBANK1/(03105)	/HBANK1/(03105)	/HBANK17(03105)		SMARK	₽ J	Y121 HMAX i	LASIP IREXIT	·LFBL	. BUR	•L15X	. F X 34	.1.8511	Frouts	- 201
ამიმა ა2 <i>1</i> 2ა	U2764 U2772 U3U20 U3U3U	SFCTIONS	U3031 U3565		(13565) (13575) (17426)	26652 (17426)	2 31015 /(03620)	32205 3222 3223	7/ 62/05/) / (TEDED) /	/(03031) /55/53	36271	36661	57434 57535	(37752) 40147	40375 *	43634 *	4430	44325	44370	44420	47037	47171 *	
a.	o b AT10w	CONTROL	/DAIA /	/COMS1 / /DATA / /KECT /	/GKAPHZ/ Z1512 /EPSTN /(U3563) /POWLOS/(U3575) /GRAPHD/(17420)	PRAM 26652 /GRAPHO/(17426)	CALCO2 /RECT /	DENSE /EXFLD /	/UAIA /		CSINI	10H	MINV	S C A A K	YDOT	LXSIR	CLSE.	WKIIE	· LTRLK	• FELTRY	.LASEL	·LAIND	- 11.
2161N (WI105	2. UNITOD 3. UNITOD 3. UNITOD PHE-EXECUTION INITIALIZATION CALL ON OBJECT PROGRAM OBJECT PROGRAM	ORIGIN	იპსპი	21504	23712	26625 26720	51025	32222	32504	34747 3500b	35304	36553	3667 <i>1</i> 37535	40147		43634	•	11044			44535.	101.1	17.75
SYSTEM FILE BLOCK ORIGI FILES 1.	2. 3. PILE LIST ORIGIN PRE-EXECUTION IN CALL ON OBJECT P	DECK	MAIN	UANT	outPu		DENS	r IEL	FOWER	FOKC	CSI	10	MIN SMK2	MAKS		•LXC019		• IOUEF			. IUCSF	1	ביי
SYST FILE FILE	FILE PKE- CALL OBJE		1:	<sup>2</sup>	ω <del>1</del>	တ် ထိ	7.	ဆ်	ŝ	10.	12.	14.	9	17.		18.		19.			21.		c

25. XII							!			;		
	47430	CC+1	47430	CC.2 FXTI.	47431	£.53	47432	4.00	47433			
	47435	FMTLOC	47435 *	EOFCL	47436	·RULD•	47437	· FXEM.	0144	.FXOUT	47776	
	50071	. FOUT.	50071		2000							
28. FCNV.	20465	. FCON.	20465	.FCNV.	50510	. ENDES		*CNNS#	50524	FDX1	50530	1
		FUX2	50531	.08C	50533	. DEC10	50671	• DBC2n	50717	WSQU.	50735	
		100	75500	FOX - C	20/16			1000	27.5	1010	10210	
		LNT.	51477	A011	51546	. TERRY	51564	- N	51377	Z X W	52010	
	:	FXD	52011	HOLL	52146	INTO	52216	TUOL	52300	. OOUT	52317	
		• XCF	52350	TEST.	53073	-KOUNT	53076	LIST	53101	DONE	53112	
		-OUTBF	53156	-BUF	53205	.asTo	53206	WIDIM.	53207	NI AG.	53210	:
		. GAIN1	53211	FUDDE	53221	. DUDFL	53245	• DOFLG	53246	OOM.	53247	
		• PEX	53250	.FEXP	53251	•DIG	53252					
29. F105	53267	•E105.	53267	FSEL	53437	.FILR.	53443	.FRTB.	53452 *	.FRTD.	53457	
		•F1LL.	53462	FCLS	53464 ×	NGOF.	53470 *	REOF	53474 *	.T0UT.	53642	
1010	. 1757	1000	0.0000	NTOS	50501	) i	20006	- 15.02Z	2000			
10.00	54772		53704	• 17 1	04046	2 4.	040.4					
	55016	-FRDU	55016									
	55044	-FRDU	55044									
1	55105	.UN05.	55105									
35, UNU6	55106	• 0M06•	55106	BUFSZ	22107	:	:	!		:		
	55112	.F100.	55112	CTOTO.	55610	.NMLST	55633	.NAME.	56737	. TNTAP	56740	
	57363	AL.0610	57363	AL06	57364	:	:			1	:	
	57567	EXE	57567	•								
4	5//10	203	5771U	NIZ	2//11							
	10109	- X97	\$010¢									
	20700	ZNY X	72700	ALAN	natna			:	:	:		
47. FXP1	50411 5055	X77.	11+00									
44. FXP3	60043	XP3.	60643	:				: : : : : : : : : : : : : : : : : : : :				1
	07709	.FSLI.	61000	.FSDI	61014 *							
	61025	.SLI.		.SL11.	61032	·sor.	61040	.co11.	61046			
47. FSLDO	61061	.FSLO.	61077	.FSD0.	61105 *	:					;	:
	61116	·S-0.		.SL02.	61124	.500.	61131	.5005.	61140			
	61152	CABS		:			:					
	61212	CFMP.	61212	.CFDP.	61213							
51. FCS0	61337	CSURT					. !					
	61413	COLAN		ZAL	61414	CRIT	61557 *					
53. FASC	61636	ARCOS	61630	ARSIN	61637 *				:		,	
	61767	OFFSET	61770 *	WHERE	62006	FACTOR	62023 *	PL.OTS	62030	P. OT	62113	
	63304	SYMBOL				:		:			:	
56. AXISZ	64110	AXIS										
LINEZ	94/49	LINE	•				***************************************					
58. NUMBRZ	65361	NUMBER	65732									

77100 THRU 77211

UNUSED CORF

						!						:				•		
		(OEO)	03563 17405	/(03561) /(17416)	/(03566) 24606	31012	32171 7(03546)	(99580)/			37735	40355 *	42023	44257 *	443000 44343 * 44405 *			* 001/1
		*Loc*=MoveD* *=NOT REFERENCED)	/EPSTN / /RnOTS /	/NFW /(03561 /GRAPH1/(17416	/GAUSS / OHTPUT	CALCOI	DFNSE /CrSR /	/ 85Nv9/	E		NO.	Y EIIBAR	RGEPR •LXCAI	.1.0	LAREA LANEA I UNBL		COMX 1.	OVFL.OW
		ved• *=N	03561 03620	21470 * /(17407) 1/(17426)	/(03546) /(17405)	30734	/(21505) /(03566)	(93246)/		36524	37730	40325 *	47677	44270	44332 *_ 44377 44377		47066 * 47161	47334 *
			/NEW /	21470 /CONST /(17407) /GRAPHO/(17426)	/CPSR //	CALCOS	/RBLK1 / ( /GAUSS / (	/CPSR //		POLAR	TRA24	TGL0 Yn121	YCLOW •LXERP	. DFOUT	OPEN RELES AREA1	1	.1 x0VI	/.COUNT/ E.4
		O LENGTH, (LOC)=DELETED,	03546 03575	/ 17426 /(03546) / 21505	/(03105) /(03620) /(17407)	30050	.03105) 03105)	(3252)	34757	/(03546)	37723	40360 *	40463 43670	* 44044	44602 446330 * 444374 *		47026 *	47372 47411
		TH, (LOC)		/GRAPHO/ /CRSP /( /KBLK1 /	/HBANK1/(031NS) /KFCT /(03620) /CONST /(174N7)	CALCO	/HBANK1/(03105) /HPANK1/(03105)	ZPOWLOSZ (03575	FONCE	/CPSP /(	1RA14		HMINT -L. AOUT	· LUNB	.PEADR .PEADR .RLHLD	<b>X</b>	LXTST	. FPAKG E. Š
- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	65754	ON O LENG	03105 03566	/ 17416 /(u3105) /(u3565)_		17416)	51020 /(U3031) /(U3U31)	03105)	34 /20 03105)	03105)	37520)	40317 *			# ## ## ## ## ## ## ## ## ## ## ## ## #	44513	47023	47324
	H.	(ZNAME/=NON	/HRANIK1/	/GRAPH1/ 17416 /HRANK1/(U3105) /KSu /(U3565)	INFILI 23676 /UAIA /(U3U31 /GRAPHP/(21512 /GRAPH1/(17416	/GRAPH1/(17416	CALCO3 /UAIA /( /UAIA /(	/HRANK17 (U3105)	POWFKL 34/20 /HRANK1/(03105)	/HBANK1/(03105	SMARK	, 52.	HMAYI LXAID	IRCXIT Lrab	BSR BSR LISK	.Fx34	1.49L1	Fr.nuT
08780	u2764 u2772 u3025 u3030	SECTIONS	03031 03565	/ 17407 /(U3U31) /(U3b2U)	21512 03565) 03575) 17426)	26652 17426)	31015 (03620) 3220c	32455 (13031)	/(32205) /(u3u31) 35235	36644 36644	3741/ 3752u	40132		43702	44310 44310 44361	44411	47022	
	N071	CONTROL	/ BIAI/	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	\$ .	PRAM 26652 /GRAPHO/(17426)	~ ` `	-		_ <	> <del>*</del>	NA S	ELBAR LXSIR	.LXPIN .CLSE	.OEFIN .WKITE .LFBLK	. COMXI	·LXSEL	. FFP1.
ORIGIN UNITOS 2. UNITOS	FILE LIST ON THING PRE-EXECUTION INTITION CALL ON OBJECT PROGRAM OBJECT PROGRAM	ORIGIN.	ივივი	21504	23712	26625 26720	31023 32205	32467	34732 34771	35267 36313 36530	36662 37520	40132	11 Sp. 1 7		47244		4452 <u>0</u> 47022	47167
ar ock	FILE LIST ONIGIN PRE-EXECUTION INITICAL ON OBJECT PROG	DECK OF	MAIN	N-M	outbo s	20,	OENS FIEL	POWER	FORC	a	MIN	MAKS	3		• I UDE F		.10CSF	FFTKP
SYSTEM FILE B FILES	FILE PRE-E CALL OBJEC		1.	<b>.</b> ≪	ю д		7. 8.	6			15.	17.		0	61		20.	22.

CONVSW CONVSW CONVSW FELT ANDTH NIDTH NIDTH NIDTH NIDTH SEOF FECKSZ SCOZ.
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SAMPLE CASE GENERATED FOR DOCUMENTATION

ECTION				. VALUES 0.707 0.050 1.176 60.549	
INITIAL RAY DIRECTION	AO 65,99 BO 0.00 DELAO 0.00	FIELD LINE LAMBDA 53.94 L-VALUE 1.53	INTFRVALS PPINI 200.0 PLOT 100.0 STEP 20.0	SCALE SIZE 0.707 PKFRAC 0.050 HPKIME 1.176 PKDFLN 60.549	
INITIAL KAY POSITION	9295,4u 77,44 90.0u	KAY CHARACTERISTICS FREG 1.00 MODE -1	STOP CONDITIONS MAX MIN 11000.0 6370.0 180.0 0.0	PROGRAM OPTIONS NPUMER 0 NPLOT 1 NOVEK 0 NAUTU 0 ATEST 2	о ми.
TVILIDI	HETAC PHIO	RAY CLAI	KADIUS IHETA PHI	NPOWER C NPLOT NPLOT O NAUTO C LEST 2	UNDKFLOW AT 20504 IN MG UNDKFLOW AT 20520 IN AC AND MG. UNDKFLOW AT 20520 IN AC AND MG.

POWER LOSS EPSTEIN Ch GROUP DELAY	0.0000000E-39	8.01052498-02	0.000000E-39	1.8393076E-13	7.9732613E-01	0.000000E-39	1.0242290E-13 1.5872814E 00	0 # 1 1 1 0 0 0 0 0 0	4.05274A7E-14	2.3712085£ 00	0.000000E-39	3.8245256E-14	3.1502037E 00	0.000000E-39	2.5948592E-14	3.9251668E 00	0.000000E-39	1.A751383E-14	4.6968806E 00	0.000000E-39	1.4453184E-14	5.4660469E 00	0.000000E-39	1.2002435E-14	0.63361136	0.000000E-39	1.0686431E-14	2014///	0.00000005-39	1.01416456-14	7.7641417E 00	0.0000000E-39	1.0141433E-14
DOPPLER SP Y**2 NU	0.0000000E=39	8.6929314E-06	-0.0000000E-39	R.6454015E-01	5.1706413E-06	-0.000000E-39	8.6975416E-01 3.0565067E-06	01-200000000000000000000000000000000000	0 74 157645-01	1.90243205-06	-0.000000E-39	8.7781718E-01	1,2563415E-06	-0.0000000E-39	8.8080528E-01	8.8431544E-07	-0.0000000E-39	8.8324544E-01	6.5878622E-07	-0.0000000F-39	A.851A245F-01	5.2030317E-07	-0.0000000E-39	8.8660225E-01	4.398789RE=U/	-0.000000E-39	8.8756102E-01	3+40220415-01	-0.000000E-39	R.8811182E-01	3.7861936E-07	-0.000000E-39	A. AA11520F-01
ABSORPTION MU**2 N	9.999999E=01	1.2074153E 03	9.9999995-01	8.6454017E-01	1.1775214E 03	9.9999999E=01	8.6975418E-01		9.9999996	1.1237326E 03	9.9999999E=01	8.7781720F=01	1.1025245E 07	9-9999996-01	A.8080530E-01	1.0848494E 07	0.99999995-01	A.8324545E-01	1.0700A84E 03	0.00000000000	B 8518948F=01	1.0580794E 03	9.9999999E-01	8.8660226E-01	1.0490262E 04	9.999999E-01	8.8756100E-01	1.0426132E UT	9.999999E-01	A.8811183E-01	1.0385536E 01	9.999999E-01	TOWN TOWN TOWN
LONGITUDE Y3 DFL MU	8.9999987E 01	-0.00000006-39 2.1791243E-05	8.9999947F 01	0.000000F-39	1.2532970E-05	8.999987E 01	0.0000000E-39		8, 9999987E UI	1.6612134E-05	8.9999987F 01	0.00000000	2,1914030E-05	8 00000075 01	0.000000F-39	9.8592200E-06	10 25000000 8	0.0000000F=39	1.0791444E-05	0 0000000	0.999999000	2.3180092E-05	8.999987E 01		1.5447359E-05	8.9999987E 01	0.0000000E-39	9.0264119E-06	8.9999987E 01	0.000000E-39	1,7753554E-05	8.9999987E 01	01-1000000
COLATITUDE Y2 MOD AND ARG		8.4940216E-01	10 2782520 7	0 6040035F=01	-9.0000000E 01	7.9ABSE71F 01	8.7869874E-01		8.1110764E 01	8.9420238E-01 -9.0000000E 01	10.331000160.01	0 0:20:00	9.03/2163E-01 -9.0000000E 01	10 1001 1146 0	0 1"570665-01	-9.0000000E 01	10 LC 11 C 1	0 25504465-01	-9.0000000E 01		8.6054828E U1	9.3235042E-01	8.7294759F 01	9.3677850E-01	-9.0000000E 01	A.8544160F 01		-9.0000000E 01	8,9790206E 01	9.4239470E-01	-9.0000000E 01	A. 9HOKKBUF 01	
RADIUS Y1 POLAKIZATION =	9.3041084E 03	3.7083140E-01 1.0000023E 00	#20.0000 P		1	0.4540106F 04	'	3	0.5233201E 03	2.7305632E-01 1.0000071E 00	#0 20101E03	9.5051916E US	2.4/19298E-01		9.5558551E US	1.0000034E 00		9,6/63511E 03	1.6283832-01		9.7104039E 03	1.2511563E-01 1.0000010E 00	#0 377#34#7	0.5122531F=02	1.0000070E 00	0.7494779E 03	4.7070662E-02	1.0000001E 00	0.7562792E 03	C. 1455051F=04	1.0000062E 00	FO 30000347	
PHASE PATH GROUP PATH RAY PATH	2.00000000 01	2.4031575E U1 2.1583306E U1			2,1547645E 02	60 10000000	4.7618443E 02	4.3024053E UZ	6.0000000E 02	7.1136256E 02 6.4441360E 02	,		9.4506111E 02			1.1775500E 03 1.0713754E 03		- 1	1.4090642E US	i	- 1	1.6398141E 03 1.4970117E 03	!	1 p690p34F 03	- 1		2.0997386E 03	- 1	2.0000000000 03		2.1340939E 03		Z.0025441E 03

PHASE PATH	RADIUS.	COLATITUDE LONGITUD Y2 Y3 - MUD AND ARG DEL MU	LONGITUDE	ABSORPTION	DOPPLER SP	POWER LOSS
GROUP PATH	Y1		Y3	MU**2	Y**2	EPSTEIN CO
RAY PATH	POLARIZATION		DEL MU	N	NU	GROUP DELAY
2.2000000E 03	0.7533718E 03	9.1036575E 01	8.9999987E 01	9.9999999E=01	#0.0000000E-39	0.0000000E-39
2.5587009E 03	-3.0006336E-02	9.4176053E-01	0.0000000E-39	8.8781328E=01	R.8781327E-01	1.0383982E-14
2.3463297E 03	1.0000025E 00	-9.0000000E 01	2.1992870E-05	1.0408437E_03	3.8631913E-07	8.5290028E_00
2,40000000E 03	9.7405720E 03	9.2282115E 01	8.9999987E 01	9.9999999E=01	-0.0000000E-39	0.0000000E=39
2,7883552E 03	-7.0091676E-02	9.3911A11E-01	0.0000000E-39	R.8696R46E=01	R.8696845E-01	1.1466033E=14
2,5586364E 03	1.0000024E 00	-9.0000000E 01	1.0138950E-05	1.0466211E_03	4.2215269E-07	9.2945173E_00
2.6000000E 03 3.0183646E 03 2.7710679E 03	-1.2064937E-01 -1.0000049E-00	9.3526370E 01 9.3534941E-01 -9.0000000E 01	8.9999947E 01 0.000000E-39 1.1550780E-05	9.9999999E=01 8.8569740E=01 1.0548366E 03	-0.0000000E-39 R.8569738E-01 4.8951262E-07	0.000000006-39 1.3509765E-14 1.0061215E 01
2.8000000E u3	9.6491510E 03	9.476.933E 01	8.9999987E 01	-9.9999999E=01	-0.0000000E-39	0.00000000E-39
3.2488991E 03	-1.505663E-01	9.270.798E-01	0.000000E=39	R.8396815E=01	R.8396A14E-01	1.7003786E-14
2.9836814E 03	1.0000005E 00	-9.000,000E 01	2.3382330E=05	1.0656361E 03	6.0283022E-07	1.0829664E 01
3.0000000E U3	9.6493534E U3	9.6007885E 01	8.9999947E 01	9.9999999E=01	-0.00000000=39	0.0000000E-39
3.4801365E U3	-1.8710618E-01	9.2015684E-01	0.0000000E-39	8.8169734E=01	8.8169732E-01	2.3049394E-14
3.1965358E U3	1.0000068E 00	-9.000,000E 01	1.4377438E-05	1.0794885E 03	7.9426515E-07	1.1600455E 01
3.2000000E 03	0.6008059E u3	9.7243106E 01	8.9999987E 01	9.9999999E-01	-0.000000000-39	0.00000000E-39
3.7122717E 03	-p.3219256E-u1	9.0827195E-01	0.000000E-39	A.78A7131E-01	A.7887131E-01	3.3414795E-14
3.4096949E 03	1.0000003E 00	-9.0000000E 01	8.4454776E-06	1.0963403E 03	1.1119204E-06	1.2374239E 01
3.4000000E 03	9.5443655E 03	9.8475507E u1.8.9483298E-019.0000000E.01.	8.9999947E 01	9.9999999E-01	-0.0000000E-39	0.00000000E-39
3.9455325E 03	-2.7338235E-01		0.000000E=39	A.7546400E-01	A.7546396E-01	5.1496354E-14
3.6232323E 03	-1.0000072E.00		1.6913921E=05	1.1162171E 03	1.6441106E-06	1.3151775E 01
3.6000000E 03	9.4792747E U3	9.9703398E 01	8.9999947E 01	9.9999999E-01	-0.0000000E-39	0.0000000E-39
4.1801808E 03	-2.9854333E-U1	8.8443135E-01	0.000000E-39	8.7134694E-01	R.7134697E-01	8.4905355E-14
3.8372307E 03	1.0000025E U0	-9.000un00E 01	2.1458650E-05	1.1397123E 03	2.5813040E-06	1.3933936E 01
3.8000000E 03	9.4054098E 03	1.0092554E 02	8.9999947E 01	9.9999999E=01	-0.0000000E-39	0.0000000E-39
4.4165199E 03	-3.3120860E-01	8.6988204E-01	0.000000E=39	8.6639392E=01	R.6639389E-01	1.5002362E-13
4.0517841E 03	1.0000035E 00	-9.000000E 01	9.2783632E=06	1.1673512E 03	4.3070709E-06	1.4721733E 01
4.00000000E 03	9.3240365E 03	1.0214426E U2	8.9999987E 01	9.999999E-01	-0.0000000E-39	0.0000000E-39
4.6549209E 03	-3.7075416E-01	8.5U32947E-01	0.0000000E-39	8.6051887E-01	R.6051A86E-01	2.A165519E-13
4.2670051E 03	1.0000038E 00	-9.0U0UNUE U1	8.7714449E-06	1.1993057E 0x	7.5706798E-06	1.5516403E 01
4.2000000E 03	0.2053370E u3	1.033mg8E u2	8.9999987E 01	9.9999099E-01	-0.0000000E-39	0.0000000E-39
4.8958493E 03	-u.0079329E-u1	8.324u772E-01	0.0000000E-39	A.5353786E-01	R.5353786E-01	5.6172143E-13
4.4830317E 03	1.0000049E u0	-9.0u0u0u0E 01	1.9825234E-05	i.2362420E 01	1.4000840E-05	1.6319498E 01
4.40000000 03	9.1386191E u3	1.0457172E 02	8.9999987E 01	9.9999999E-01	-0.0000000E-39	0.0000000E-39
5.1398913E 03	-u.1943090E-u1	8.1805645E=01	0.000000E-39	8.4513867E-01	A.4513A67E-01	1.1982238E-12
4.7000334E 03	1.0000060E u0	-9.000un00E 01	1.8242112E-05	1.2794121E 03	2.7374596E-05	1.7132971E 01

71 71 72 71 72 71 72 72 71 72 72 74 71 72 74 74100 74,0453949E 74 74,0453949E 74 74,0453949E 74 74,0453949E 74 74,0453949E 74 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453949E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999B 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999E 74,0453999B 75,0453999B 75,0453999B 75,045399B 75,045399B 75,045399B 75,0453B 75,0453B

POWER LOSS EPSTEIN CP GROUP DELAY	0,000000005-39 1,81358335-08 4,034465E 01	n.ngng0gnE-39 x.u927727F-09 u.1672571E 01			0/4 (						11 3.6805543F-13 16 4.9854250F 01 (9 0.000000F-39	
UNPPLFR SP Y**? NII	_n.nononone_3° 5.6977797E_01 6.6140081E-02	_0.0000000E-39 6.5640711E-01 2.0200305E-02	_n.0000000E=39 7.1185146E=01 6.8261424E=03	_0.0000000E=39 7.5036307E=01 2.4826449E=03	_n.00000000E=39 7.7857A86E=01 9.5962344E=04	_n.0000000E-39 A.0005737E-01 3.9179A97E-04	_n.nonononE-39 A.16A7A4nE-01 1.6853182E-04	_0,0000000E=39 A,3034059E=01 7,6312902E=05	_n.nononong-39 A.4130255E-01 x.6354116E-05	•	A.5778911E-01 A.5778911E-01 A.6116026E-06	i
ARS-ARPTTON MU**2 N	a.q229129E=01 5.6977799E=01 2.3380222E 03	0.9227326E-01 6.564071xE-01 2.0527903E 03	a,9226a43E=01 7,1185149E=01 1,8522921E=03	0.422644E=01 7.5025110E 01 1.7025110E 01	9.9226815E-01 7.7857887E-01 1.5860124E 03	a,9226au5E-01 a,n0n574nE-01 1,4926772E 03	a.q22bAQ2E-U1 a.16A7A41E-01 1.416218AE 07	o.9226800E=U1 8.30%4061E=01 1.3525142E 03	a.9226AUNE-01 A.411U257E-01 1.29A7N91E 01	0.9226A00E-01 A.50x4970E-01 1.2527917E 07	0.92268UNE=01 8.5788217E=01 1.21x3721E 0x	9.92268U0E-U1 8.6418176E-01 1.1794698E_03
DOCUMENTATION LONGITUDE YA DEL M <sup>II</sup>	8.ayayab7E 01 0.n000nunE-39 2.7363?b8E-05	8,9999987E 01 0.nunununE-39 1.8864516E-05	8,999987E 01 0,0000000E-39 1,46688U3E-05	8.999987E 01 0.n00ununE-39 1.2373409E-05	8.9999947E 01 0.0000000E-39 1.1996634E-05	8.9999987E 01 0.n00ununE-39 1.345u1.1E-05	8,9999947E U1 0,0000000E-39 1,4730776E-05	8,agagad7E_01 0,n000n0nE_39 1,*54 <sub>0</sub> 3enE_05	8.q999qq7E 01 0.n000nunE=39 1.2090531E=05	8.a999987E 01 0.nu00n0nE-39 1.a019496E-05	8, <u>9999</u> 987E_01 0,000000E=39 1,5211265E=05	8.a999987E 01 0.n000000E-39 1.u742595E-05
GENERATED FOR DOCU COLATITUDE 12 MOD ALD AKG	1.149/A56E 02 -5.5164032E-01 9.0004000E 01	1.1364109E 02 -6.0857538E-01 9.000.000E 01		1.1112141E 02 -6.8495159E-01 9.000HOUDE 01	1.0989641E u2 -7.1505410E-01 9.000mn0E u1	1.0860143E U2 -7.4147620E-U1 9.0UUNOUE U1	1.0747157E 02 -7.647595E-01 9.000un00E 01	1.1	1.0505471E U2 -8.0745341E-U1 9.000000E U1	1.0384443E U2 -8.2749397E-01 9.000_000E_01	1,026,5119E_02 -8,4534718E-01 9,01001010E_01	1.0141391E U2 -8.6154041E-01 9.000000E_01
SAMPLE CASE RADIUS Y1	0.0155108E U3 c.1525870E-U1		201 101	A.4080642E U3 <.3027412E-U1 1.0000002E U0	A.625¤927E U3 <.1701558E-U1 1.000000E U0	A.7548459E U3 S.0U27055E-U1 1.0U00002E U0	A.8/64929E U3 4.816555E-U1		0.0977012E 03 0.3011170E-01 1.000001E 00	0.1975750E 03 n.0094400E-01 1.0000001E 00	9.2896003E03 7.7851059E-01 1.0000000E.00	9.3740654E 03 3.4918459E-01
	6.8000000E U3 1.2105340E U4 7.0857478E U3		8.14059455E U3 7.2000000E U3 1.2839439E U4 8.3821237E U3	7.40000000 u3 1.3144621c u4 8.6158774c u3	7.600u0u0b u3. 1.34298u6c u4 8.8445264c u3	7.80000000 03 1.3701579c 04 9.0595828c 03	8.000u0u0c u3 1.3963811c u4	9.2919/43E 03 8.2000000E 03 1.4218965E 04 9.4127836E 03		8.5000000E u3 1.4714182E U4 9.9485109E u3	8.8000000E U3 1.4956275E U4 1.0164904E U4	9.00000000 u3. 1.5195626E U4
			: !		: !			!	:			

II	RAUIUS Y1	COLATITUDE 72	LONGITUDE	ABSORPTION MU**2	DOPPLER SP Y**2	POWER LOSS EPSTEIN CD
RAY PATH	POLARIZATION	- MOD AND ARG	DEL MU	2	NN N	GROUP DELAY
0.3	0.4506141£ 03	1.0019236E 02	8,9999947E 01	9.9226800E-01	-0.00000005-39	0.000000E-39
すっ	3.1603229E-01	-8.7726200E-01	0.0000000E-39	8.6946503E-01	A.6946501E-01	
90	1.0000000 00	9.0000000E U1	1.32054565-05	1.15029475 01	3.1485539E-06	5.1442470F 01
03	9.5191812F 03	9.8966667E U1	8,9999947E 01	9.9226800F-01	-0.000000E-39	0.0000000E-39
70	2.8045148E-01	-8.9176531E-01	0.000000E=39	8.73A9A39E-01	R.7389839E-01	6.2476631E-14
70	1.00000016 00	9.0000000E 01	1.4332095E-05	1.1252157E 07	1.9576336E-06	5.2226745E 01
03	9.5794746E 03	9.773n665E 01	8,9999987E 01	9.9226A00E-01	-0.000000E-39	0.0000000E-39
ħ0	2,4564439E-01	-9.0402183E-01	0.000000E-39	8.7759665E-01	A.7759664E-01	3.9345983E-14
10	0.999999E-01	9.0000000E 01	1.6199269E=05	1.1038191E 0*	1.2890357E-05	5.3006017E 01
03	9.6311339E 03	9.6502371E 01	8,9999987E 01	9.9226A00E-01	-0.0000000E-39	0.0000000E-39
40		-9.1469123E-01	0.0000000E-39		A.8064346E-01	2.6495707E-14
100	1.0000002E 00	9,000unue 01	1.4973576E-05	1.085809AE 04	9.0114630E-07	5.3781209E 01
7	9.6740923E 03	9.5264431E 01	8,9999987E 01	9.9226800E-01	-0.000000E-39	0.0000000E-39
70	1.70145556-01	-9.2421018E-01	0.0000000E-39	8.831139RE-01	A.8311397E-01	1.9077606E-14
40	9.999999E-01	9.0000000E 01	1,40740U1E-05	1.0708A69E 03	A.6914065E-07	5.4553111E 01
7	0.7082855F 03	9.4023u62F 01	8.9999987E 01	9.9226800E-01	-0.000000E-39	0.0000000E-39
ŧ		-9.3172966E-01	0.000000E-39	8.8506474E-01	8.8506474E-01	1.46882425-14
10	1.0000001E 00	9.0000000E 01	1.5889954E-05	1.0588217E 03	5.2798227E-07	5.5322417E 01
71	0.7334000F 03	9.2774930F 01	8.9999987E 01	9.9226800E-01	-0.0000000E-39	0.0000000E-39
70	9.1694817E-U2		0.0000000E-39		A.8652664E-01	1.2117002E-14
04	1.0000001E 00	9.000un00E 01	1.6450377E-05	1.0495130E 07	4.436549RE-07	5.6089748F 01
40	9.7492821E 03	9.1534641E 01	8.9999987E 01	9.9226A00E-01	-0.0000000E-39	0.0000000E-39
40	F.1120044E-02	-9.4069759E-01	0.000000E-39	A.8752522E-01	P.8752520E-01	1.0720111E-14
10	1.0000001E UO	9.000000E 01	1.4713411E-05	1.0428664E 0%	4.9742639E-07	5.6855673E 01
7	9.7560507F 03	9.028H507F 01	8,9999987E 01	9.9226800E-01	-0.000000E-39	0.0000000E-39
40	P.6260205E-03	-9.4234359E-01	0.000000E-39	A.880858E-01	A. A808583E-01	
70	1.0000001E 00	9.0000n00E 01	1.5072413E-05	1.03A7583E 07	3.7922009E-07	5.7620725E 01
40	9.7562743F 03	A. 9990169F 01	8.99999875 01	9.9226A00F-01	-0.0000000F-39	0.0000000-39
	4.2585988E-07	18	0.000000E-39	8.881524RE-01	A.8815246E-01	1.0138060E-14
	a.9999999E-01	9.000unonE 01	1,4537934E-05	1.03A1770E 07	3.7863385E-07	5.7798265E 01
-0.107819E-09						
<b>\$</b> 0	0.75364235 03	8.9042212E 01	8.999987E 01	9.9226R00E-01	-0.000000E-39	0.0000000E-39
			0.000000E-39	A.8784222E-01	8.8784222E-01	1.0361183E-14
i	1.000000E 00	9.000unonE 01	1.47477335-05	1.0406271E 01	7.8560248E-07	5.A385561E 01
40	7418979F 03	A.77964.35F 01	8.9999987F 01	9.9226800F-01	-0.0000000-39	0.0000000000000000000000000000000000000
7		-9.3912849F-01	0.000000E-39	P.8704495E-01	A.8704494E-01	1.1350454E-14

POWER LOSS EPSTEIN CN GROUP DELAY	n.0000000E-39 1.3329988F-14 5.0917629E 01	0.0000000E-39 1.675685F-14 6.0685947E_01 0.0000000E-39 2.2557459F-14 6.1456567F_01	0,0000000005-39 7,2509142E-14 6,2230144E 01	0.0000000E-39 5.0049374E-14 6.3007420E 01	0.000000000-39 8.2231394F-14 6.3789254E 01	0.000000000-39 1.4422660E-13 6.4576659E 01	0.0000000E=39 2.6979289E=13 6.5370858E 01	0.000000000=39 5.3755009E-13 6.6173367E 01	0.000000005-39 1.1412095F-12 6.6986106F 01	0.0000000E-39 2.5853932E-12 6.7811584E 01	0.0000000E-39 6.260168RE-12 6.8653159E 01
DOPPLER SP Y**2 NU	-0,0000000E-39 8,8579675E-01 4,8360261E-07	-0.0000000E-39 8.8468101E-01 5.9492356E-07 -0.0000000E-39 8.84851E-01	-0.0000000E-39 R.7908039E-01 1.0845563E-06		-0.0000000E-39 8.7161939E-01 2.5080389E-06	-0.0000000E-39 8.6674499E-01 4.1572354E-06	-0.0000000E-39 8.6093254E-01 7.2849621E-06	-0.000000E-39 A.5400407E-01 1.3464957E-05	-0.0000000E=39 8.4570740E-01 2.6223182E-05	-0.0000000E-39 R.3568949E-01 5.3790262E-05	-0.000000E-39 A.234625AE-01 1.1611286E-04
ARSORPTION MU**2 N	9,9226800E=01 8,8579674E=01 1,0542007E 03	9,9226800E-01 1,0649434E 07 9,9226800E-01	1 1	9.9226800E=01 8.7569367E=01 1.1148888E 03	9.9226A00E-01 A.7161947E-01 1.1381775E 03	9.9226800E=01 8.6674502E=01 1.1654038E 0*	9,9226800E=01 8,6093255E=01 1,1970722E 03	9.9226799E-01 R.5400409E-01 1.23x8120E 0x	9.9226799E-01 R.4570742E-01 1.2765310E 03	9,9226799E-01 R.3568950E-01 1.3264917E 07	9,9226798E=01 A.2346261E=01 1,3853692E_03
DOCUMENTATION LONGITUDE. Y3 DEL MU	8.9999987E.01 0.0000000E=39 1.4286140E=05	8,999987E 01. 0,0000000E-39 1,5562217E-05 8,999987E 01 0,000000	8.9999987E 01 0.n000nunE-39 1.4323911E-05	8.99998AZE 01. 0.0000000E=39 1.3952774E=05	8.9999987E 01 0.0000006=39 1.5438533E=05	8.9999947E 01. 0.0000000E-39 1.4930436E-05	8.0999987E 01 0.000000E=39 1.3085780E=05	8.9999987E 01 0.000000E=39 1.3208324E=05	8.0999987E 01 0.0000000E-39 1.4492756E-05	8.9999987E 01 0.n000nunE=39 1.4017018E=05	8.999987E 01 0.000000E-39 1.2474426E-05
GENERATEN FOR DOCI COLATITUDE 12 MUD ALD ARG	8.6552052E 01 -9.3439713E-01 9.0000000E 01	8.5309726E 01 -9.2767429E-01 9.000000E 01 -8.4070248E 01	8.2834369E U1 -9.0945650E-U1 9.000,000E U1		8.0374426E 01 -A.8389356E-01 9.0004040E 01	7.9151016E 01 -8.6954740E-01 9.0000000E 01	7.7932055E 01 -8.532550E-01 9.000000E 01	7.671n922E U1 -8.352,550E-U1 9.000u00E 01	7.5505080E 01 -8.1658098E-01 9.000000E 01	7.4295930E 01 -7.9704476E-01 9.000000E 01	7.3u8an99E 01 -7.7555203E-01 9.000un00E 01
SAMPLE CASE GI HADIUS. Y1 POLAKIZATION -	0.7209622E U3 -1.1268877E-01 9.999999E-U1	9.6910646E u3 1.6030173E-01 1.6000002E u0 9.6921852E u3	1.00000000 uu a.6044097£ u3 ->.2796770E-U1 1.0000001E u0	0.5480913E 03 ->.6574545E-01 1.0000001E 00	0.4834436E 03 -x.0061479E-01 1.0000001E 00	0.4105314E 03 -3.3262481E-01 1.0200000E 00	0.3296013E U3 -3.6454452E-01 1.0000000E U0	0.2409858E 03 -3.9545574E-01 1.0000002E 00	0.1448372E 03 -u.2300777E-01 1.000001E 00	9.0412130E U3 -u.4/67079E-01 1.0000000E U0	A.9502416E U3 -u.7114927E-01 1.0000000E U0
PHASE PAIH GROUP PAIH HAY PAIH	1.140u0u0E 04 1.7975289E 04 1.293b186E 04	#10 #10 #10 #10	1.33616235 04 1.2000000E 04 1.8669043E 04 1.3574761E 04	1.22000000	1.2400000E U4 1.9136776E U4 1.4002238E U4	1.25000000c. 04 1.9372998E 04 1.4216753E 04	1.28000000 04 1.9611258c 04 1.431929E 04	1.3000000c 04 1.9852010c 04 1.4647900c 04	1.320u0u0E 04 2.0095832E 04 1.4864835E 04	1.340u0u0E 04 2.0343475E 04 1.5082941E 04	1.3600000E 04 2.0595948E 04 1.5302499E 04

POWER LOSS EPSTEIN CN GROUP DELAY	0.0000000E-39 1.6244030E-11 6.9515514E 01	0.0000000E-39 4.5419231E-11 7.0405443E 01	0.0000000E-39 1.3816030E-10 7.1333328E 01	0.0000000E-39 u.c449985E-10 7.2316142E 01	0.0000000E=39 1.7747449E=09 7.3384317E 01	0.0000000E=39 R.1507641E=09 7.4600591E 01	0.0000000E-39 5.1968114E-08 7.6130611E 01	0.000000 <u>6-39</u> 9.9657889E-07 7.8844307E 01	0.0000000E-39 2.1926464E 00 8.2760466E 01
DOPPLER SP Y**2 NU	-0.0000000E-39 8.0832472E-01 2.6358472E-04	-0.0000000E-39 7.8921354E-01 6.2969025E-04	-0.0000000E-39 7.6445710E-01 1.5868946E-03	-0.0000000E=39 7.3129321E-01 4.2381968E-03	-0.0000000E-39 6.8481303E-01 1.2101202E-02	-0.0000000E-39 6.1524897E-01 3.7627766E-02	-0.0000000E-39 u.9882069E-01 1.3343921E-01	-0.0000000E-39 2.3506874E-01 6.5767968E-01	0.0000000E-39 6.0598143E-08 1.4376653E 00
ARSORPTION MU**2 N	9.9226796E=01 8.0832474E=01 1.455674E 03	9,9226790F-01 7.8921355E-01 1.5403517E 07	9.9226773E-01 7.64u5711E-01 1.6451040E 03	9.9226717E-01 7.3129424E-01 1.7778818E 04	9.9226516E-01 6.8481304E-01 1.9520851E_03	9.9225663E-01 6.1524900E-01 2.1921001E-03	9.9220926E-01 4.98R2070E-01 2.5517022E_03	9.9166191E-01 2.3506A7E-01 3.2418612E 03	9.8841257E-01 -3.5762787E-07 3.7784719E 03
CUMENTATION LONGITUDE YA DEL MU	0.0000000E=39	8,9999987E 01 0,000000E=39 1,3231398E=05	8.9999987E 01 0.000000E=39 1.u497929E=05	8,999987E 01 0,0000000E-39 1,5111310E-05	8.9999947E 01 0.0000000E=39 1.6286408E=05	8,9999947E 01 0,0000000E-39 2,0763987E-05	8.999987E 01 0.0000000E-39 3.4778884E-05	8,999994E 01 0,0000000E-39 2,0589124E-04	8,9999987E 01 -0,0000000E-39 -1,9078991E 05
GENERATED FOR DOCUMENTATION COLATITUDE Y Y MUD AND ARG DEL MU	7.1879375E 01 -7.5191908E-01 9.0000000E 01	7.0666925E 01 -7.265661AE-01 9.000unu0E 01	6.9446842E 01 -6.9915A76E-01 9.0000000E 01	6.8212914E 01 -6.6807187E-01 9.0000000E 01	6,6954459E 01 -6,3053519E=01 9,0000000E 01	6.5651290E 01 -5.8162571E-01 9.0000000E 01	6.425p299E 01 -5.0417310E-01 9.000un00E 01	6.2571919E 01 -3.3667156E-01 9.000000E 01	6.176920E 01 -2.3048930E-04 9.0000010E 01
SAMPLE CASE OF HADIUS Y1 POLAKIZATION -			8.5532037£ 03 -c.2500870E-01 1.000001E 00	R.4115997E U3 -5.3382881E-01 1.0000000E U0	A.2003882E U3 -5.3594627E-01 1.0000000E U0	A.0969135E 03 -5.2627038E-01 0.999999E-01	7.9145271E 03 -4.9049036E-01 1.0000000E 00	7.6847656E 03 -3.4888537E-01 1.000003E 00 3E-06	7.5721335E 03 p.6445506E-05 p.4903268E 00
PHASE PATH GROUP PATH KAY PAIH	1.3800000E 04 2.0854655E 04 1.5523881E 04	1.4000000E 04 2.1121633E 04 1.5747610E 04	1.4200000E 04 2.1399999E 04 1.5974452E 04	1.4400000E 04 2.1694843E 04 1.6205602E 04	1.46000000 04 2.20152956 04 1.6443082E 04	1.4800000E U4 2.2380177E U4 1.6690746E U4	1.5000000E 04 2.2839184E 04 1.6957711E 04	1.52000006 U4 7.64 2.3653292E U4 -3.44 1.7282349E U4 1.0 EMUS = -0.33763E-U6	1.5252622E U4 2.4828140E U4 1.7437619E U4
								MAIN EMUS	

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8.0	INITIAL MAY POSITION.	INITIAL RAY DIRECTION	
	KO 9295.19 THETAC 77.44 PHIO 90.00	AO 65.49 BO 0.00 DELAO 0.00	
	HAY CHARACTFRISTICS	FIELD LINF	
	FREG 1.00 MOUE -1	I AWBDA 53.04 L-VALUF 1.53	
	STOP CONDITIONS	INTFRVALS	
	MAX. MIN RAUIUS, 20000.0 6376.0 FHETA 180.0 0.0 PHI 360.0 0.0	PPINI 200.0 PLOT 100.0 STEP 20.0	
	PROGHAM OPTIONS	OTHER INITIAL VALUES	
	NPOWED 0 NPLOT 1 NOVEK 0	SCALE SIZF 0.707 PKFPAC 0.050 HPRIME 1.176 PKDELN 60.553	
	NAU10 0		

a.3u3y232E u3 7.756x594E u1 8.9999947E n1 1.0u0u0u02E u0 -9.0u0u0uE u1 1.6469652E=05 1.0u0u0u02E u0 -9.0u0u0u0E u1 1.4469652E=05 1.4456922E=01 8.6207x60E=01 0.n000n0nE=39 1.0u0u0u2E u0 -9.0u0u0u0E u1 1.446624E=05 0.999992E=01 -9.0u0u0u0E u1 1.446673E=05 0.999999E=01 -9.0u0u0u0E u1 1.4466743E=05 0.999999E=01 -9.0u0u0u0E u1 1.4466743E=05 0.9999999E=01 -9.0u0u0u0E u1 1.4466743E=05 0.9999999E=01 -9.0u0u0u0E u1 1.4466743E=05 0.000n0nC=39 1.0u0u0u7E u0 -9.0u0u0u0E u1 1.447239E=01 0.n00n0nC=39 1.0u0u0u7E u0 -9.0u0u0u0E u1 1.447239E=05 0.001739E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.347239E=05 0.001739E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.347239E=05 0.001739E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.347239E=05 0.001739E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00TE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00EE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00EE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00EE u0 -9.0u0un0E u1 1.329939E=01 0.n000n0nC=39 1.0u0u00EE u0 -9.0u0un0E u1 1.323439E=05 0.n000n0C=39 1.0u0u00EE u0 -9.0u0un0E u1 1.3323439E=01 0.n000n0nC=39 1.0u0u00EE u0 -9.0u0un0E u1 1.3323439E=05 0.n000n00E=39 1.0u0u00E u1 1.3323439E=01 0.n000n00E=39 1.0u0u00E u1 1.3323439E=01 0.n000n00E=39 1.0u0u00E=01 0.n000n00E=39 1.0u0u000TE u0 -9.0u0un0E u1 1.3323439E=05 0.n000n00E=39 1.n00000TE u0 -9.0u0un0E u1 1.3323439E=05 0.n00000TE u1 1.3323439E=05 0.n00000TE u1 1.3319731E=03 0.n00000TE u1 1.3319731E=03 0.n00000TE u1 1.3319731E=03 0.n00000TE u1 1.319731E=03 0.n000	MU**2 Y**2		EPSTEIN CD GROUP DELAY
3.7294975E-01 8.4946694E-01 -0.000000E-39 1.0000002E 03 7.8662731E 01 8.999987E 01 3.493692E-01 8.620780E-01 1.4166274E-05 0.455102E 03 7.9884624E 01 0.000000E-39 1.0000012E 00 -9.000000E 01 1.4166274E-05 0.999999E-01 -9.000000E 01 1.4166274E-05 0.9999999E-01 -9.000000E 01 1.4166743E-05 0.5232367E 03 8.1110411E 01 0.000000E-39 1.0000007E 00 -9.000000E 01 1.1866743E-05 0.5830220E 03 8.234061E 01 8.999987E 01 2.4415679E-01 9.0454199E-01 0.000000E-39 1.0000001E 00 -9.000000E 01 1.747239E-05 0.6340448E 03 8.3575341E 01 8.999987E 01 2.6415679E-01 9.151375E-01 0.000000E-39 1.0000002E 00 -9.000000E 01 1.747239E-05 0.6566775E-01 9.151375E-01 0.000000E-39 1.0000002E 00 -9.000000E 01 1.3846945E-05 0.746810E 03 8.4813458E 01 0.000000E-39 1.0000002E 00 -9.000000E 01 1.3299947E 01 0.746810E 03 8.6054524E 01 8.999947E 01 0.746810E 03 8.7296237E 01 0.000000E-39 1.0000006E 00 -9.000000E 01 1.3323439E-05 0.7499128E 03 8.8543625E 01 8.999997E 01 0.7561775E 02 9.4085938E-01 0.000000E-39 1.0000006E 00 -9.000000E 01 1.3323439E-05 0.77936449E-03 9.4238310E-01 0.000000E-39 1.0000007E 00 -9.000000E 01 1.3323439E-05	İ	1	0.00000000=39
9.379u900E 03 7.8662731E 01 8.9999BJE 01 3.4436922E-01 8.6207AE0E-01 0.000000E-39 1.0000012E 00 -9.000000E 01 1.4166274E-05 9.99999BJE 01 -9.000000E 01 1.4166274E-05 9.99999BJE 01 -9.000000E 01 1.1865743E-05 9.99999BJE 01 -9.000000E 01 1.1865743E-05 1.000000TE 00 -9.0000000E 01 1.50250.2E-05 1.000000TE 00 -9.0000000E 01 1.50250.2E-05 1.000000TE 00 -9.0000000E 01 1.7477239E-05 1.000000TE 00 -9.0000000E 01 1.7477239E-05 1.000000TE 00 -9.000000E 01 1.7477239E-05 1.000000TE 00 -9.000000E 01 1.7477239E-05 1.000000TE 00 -9.0000000E 01 1.7477239E-05 1.000000TE 00 -9.000000E 01 1.7301845E-05 0.654625E 03 8.481345E 01 0.000000E-39 1.000000TE 00 -9.000000E 01 1.7301845E-05 0.710185IE 03 8.720477E-01 0.000000E-39 1.000000E 00 -9.000000E 01 1.7301845E-05 0.746810E 03 8.720477E-01 0.000000E-39 1.000000E 00 -9.000000E 01 1.7301845E-05 0.746810E 03 8.720436E-01 0.000000E-39 1.000000E 00 -9.000000E 01 1.7301845E-05 0.746810E 03 8.720436E-01 0.000000E-39 1.000000E 00 -9.000000E 01 1.7301845E-05 0.7469172E-02 9.408338E-01 0.000000E-39 1.000000E 00 -9.000000E 01 1.3323433E-05 0.7561775E 03 8.9789210E 01 0.000000E-39 1.000000TE 00 -9.000000E 01 1.3319731E-05	8.5898767E-01 8.5898 1.2074858E_03 8.7041	8.7041584E-06 8	3.2931667E-13 8.0106949E-02
3.4936922E-01 8.6207x60E-01 0.0000000E-39 1.40000012E 00 -9.0000000E 01 1.4166274E-05 0.4551005E 03 7.9884624E 01 0.000000E-39 0.999998E-01 -9.0000000E 01 1.1866743E-05 0.5232367E 03 8.1110411E 01 0.0000000E-39 1.0000007E 00 -9.0000000E 01 1.1866743E-05 0.5530220E 03 8.234061E 01 0.0000000E-39 1.0000001E 00 -9.0000000E 01 1.7477239E-05 0.6340448E 03 8.3575341E 01 0.0000000E-39 1.0000001E 00 -9.0000000E 01 1.7477239E-05 0.6566775E-01 9.1513752E-01 0.0000000E-39 1.0000002E 00 -9.0000000E 01 1.3846945E-05 0.6764625E 03 8.4813458E 01 0.0000000E-39 1.0000002E 00 -9.0000000E 01 1.3299366-05 0.7346810E 03 8.5220477E-01 0.0000000E-39 1.0000005E 00 -9.0000000E 01 1.3299987E 01 0.0000005E 00 -9.0000000E 01 1.3299987E 01 0.0000005E 00 -9.0000000E 01 1.3299987E 01 0.0000005E 00 -9.0000000E 01 1.3323439E-05 0.7499128E 03 8.8543625E 01 0.0000000E-39 1.0000005E 00 -9.0000000E 01 1.3323439E-05 0.7499128E 03 8.97834210E-01 0.0000000E-39 1.0000005E 00 -9.0000000E 01 1.3323439E-05 0.7795449E-03 9.4239210E-01 0.0000000E-39 1.0000007E 00 -9.0000000E 01 1.339731E-05	0,9999999F-010.000		0.000000E-39
0.4951005E 03 7.9884624E 01 8.999947E 01 0.4951005E 03 7.9884624E 01 0.000000E=39 0.9999995E=01 8.783471E=01 0.000000E=39 1.00000007E 03 8.1110411E 01 0.0000000E=39 1.00000007E 00 9.0000000E 01 1.5025012E=05 0.5830220E 03 8.2340601E 01 0.0000000E=39 1.00000001E 00 9.0000000E 01 1.747729E=05 0.6340448E 03 8.3575341E 01 0.0000000E=39 1.0000001E 00 9.1513752E=01 0.0000000E=39 1.0000002E 00 9.1513752E=01 0.0000000E=39 1.0000002E 00 9.220177E=01 0.0000000E=39 1.0000002E 00 9.3220177E=01 0.0000000E=39 1.0000003E 00 9.000000E 01 1.3323439E=05 0.7499128E 03 8.8543625E 01 8.9999947E 01 0.7561775E 03 8.8543625E 01 8.9999947E 01 0.7561775E 03 8.9789761E 01 0.0000000E=39 1.0000007F 00 9.0000000E 01 1.3323439E=05	A.6454064E-01 A.6454	R.6454062E-01 1	1.A389052E-13 7.0732478E-01
0.4951005E 03 7.9284624E 01 8.999997E 01 0.1347375E-01 8.7634971E-01 0.0000000E39 0.9999999E-01 -9.000000E 01 1.1866943E-05 0.5232367E 03 8.1114411E U1 8.999987E 01 0.7713870E-01 8.9294065E-01 0.0000000E39 1.0000000TE U0 -9.000000E 01 1.5025012E-05 0.5830220E 03 8.2240661E 01 8.999987E 01 0.0000001E 00 -9.000000E 01 1.747729E-05 0.6340448E U3 8.3575341E U1 8.999987E 01 0.0000001E U0 9.1513752E-01 0.0000000E-39 1.00000002E U0 9.1513752E-01 1.3406495E-05 0.6764625E U3 8.4813458E U1 8.999987E 01 1.6666775E-01 9.2491707E-01 0.0000000E-39 1.0000002E U0 9.220177E-01 0.0000000E-39 1.0000002E U0 9.3220177E-01 0.0000000E-39 1.0000002E U0 9.9280177E-01 0.0000000E-39 1.0000002E U0 9.9000000E U1 1.3209987E 01 0.746810E U3 8.8543625E U1 8.999987E 01 0.7499128E U3 8.8543625E U1 8.999987E 01 0.7561775E U2 9.4085938E-01 0.0000000E-39 1.0000000E U0 -9.0000000E U1 1.3323439E-05 0.7561775E U3 9.4085938E-01 0.0000000E-39 1.0000000E U0 -9.0000000E U1 1.3323439E-05	ļ		
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0.5232367E 03 8.1110411E 01 0.000000E-39 1.0000001E-01 0.0000000E-39 1.0000001E-01 0.9.0000000E 01 1.5025012E-05 2.4415679E-01 9.0454199E-01 1.5025012E-05 1.0000001E-00 -9.0000000E 01 1.7477239E-05 1.0000001E-00 -9.0000000E 01 1.7477239E-05 1.0000001E-00 9.1515752E-01 0.0000000E-39 1.0000002E-00 9.2491707E-01 1.3846845E-05 0.7246810E-03 9.2491707E-01 1.3846845E-05 0.7246810E-03 9.220177E-01 0.0000000E-39 1.0000003E-00 -9.0000000E-01 1.3299387E-01 0.7246810E-03 9.220177E-01 1.3299387E-01 0.7246810E-03 9.24926E-01 0.0000000E-39 1.0000005E-00 -9.0000000E-01 1.3299387E-01 0.7246810E-03 9.498585E-01 0.0000000E-39 1.0000006E-00 -9.0000000E-01 1.3323439E-05 1.00000006E-00 -9.0000000E-01 1.3323439E-05 1.0000000E-00 -9.0000000E-01 1.3323439E-05 1.0000000E-00 -9.0000000E-01 1.3323439E-05 1.0000000E-00 -9.0000000E-01 1.3323439E-05 1.0000000E-00 -9.0000000E-01 1.3323439E-05 1.0000000TE-00 -9.0000000E-01 1.3323439E-05 1.0000000TE-00 -9.0000000E-01 1.3323439E-05	8.69764UNE-U1 A.6976 1.1486229E O1 3.0524	3.0524584E-05 1	1.5872855E 00
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\$\text{0.0000007E} 0.0 \$-9.0000000E} 0.1 \$\text{1.5025012E} -0.5 \$\text{0.0000000E} 0.1 \$\text{1.5025012E} 0.5 \$\text{0.0000000E} 0.1 \$\text{1.50999937E} 0.1 \$\text{0.0000000E} 0.3 \$\text{0.0000000E} 0.1 \$\text{1.7477239E} 0.5 \$\text{1.60000000E} 0.1 \$\text{1.7477239E} 0.5 \$\text{1.60000000E} 0.0 \$\text{0.0000000E} 0.1 \$\text{1.7477239E} 0.5 \$\text{0.0017369E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.00000000E} 0.1 \$\text{0.000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0.1 \$\text{0.0000000E} 0			6.0566377E-14
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0.6340448E 03 8.3575341E 01 8.999947E 01 2.0817369E-01 9.1513752E-01 0.0000000E-39 1.00000007E 00 -9.0000000E 01 1.3845845E-05 0.00000007E 01 1.6666775E-01 9.2491707E-01 0.0000000E-39 1.00000002E 00 -9.0000000E 01 1.32999367E 01 1.2717220E-01 9.2491776E-01 0.0000000E-39 1.2717220E-01 9.3221777E-01 0.0000000E-39 1.2717220E-01 9.3221777E-01 0.0000000E-39 1.00000003E 00 -9.0000000E 01 1.7301343E-05 0.7546675E-02 9.3724246E-01 0.0000000E-39 1.0000000E 01 1.7301343E-05 0.7499128E 03 8.724245E-01 0.0000000E-39 1.0000000E 01 1.5301343E-05 0.7499128E 03 8.8543625E 01 8.9999947E 01 0.000000E 01 1.3323439E-05 0.7561775E 03 8.9789761E 01 1.3323439E-05 0.7561775E 03 9.4234210E-01 0.0000000E-39 1.0000007E 00 -9.0000000E 01 1.3319731E-05	1.1025771E 0x 1.2578		3-1502071E 00
2.0817369E-01 9.1515752E-01 0.0000000E-39 1.0000007E U0 -9.0000000E 01 1.3845845E-05 1.6666775E-01 9.2491707E-01 0.0000000E-39 1.0000002E U0 -9.0000000E 01 1.3299936F-05 0.7101851E U3 8.6654524E 01 8.9999947E 01 1.2717220E-01 9.3220177E-01 0.0000000E-39 1.0000003E U0 -9.0000000E 01 1.7299936E-05 0.7346810E U3 8.722424E-01 0.0000000E-39 1.0000003E U0 -9.0000000E 01 1.7301343E-05 0.7499128E U3 8.3724246E-01 0.0000000E-39 1.0000006E U0 -9.0000000E 01 1.5301343E-05 0.7561775E U3 8.9789761E 01 8.9999947E 01 0.0000006E U0 -9.0000000E 01 1.3323439E-05 0.7561775E U3 8.9789761E 01 8.999997E 05 0.7561775E U3 8.9789761E 01 8.999997E 05	9.99999995-01 -0.0000		0.0000000E-39
1.0000007E   10   -9.0000000E   11.3846645E-05     1.6666775E-01   9.2491707E-01   0.0000000E-39     1.6066775E-01   9.2491707E-01   0.0000000E-39     1.0000002E   00   -9.0000000E   01   1.3299936E-05     1.0000002E   00   -9.0000000E   01   1.3299336E-05     1.0000003E   00   -9.0000000E   01   0.0000000E-39     1.0000003E   00   -9.0000000E   01   0.0000000E-39     1.0000003E   00   -9.0000000E   01   0.0000000E-39     1.0000006E   00   -9.0000000E   01   0.0000000E-39     1.0000006E   00   -9.0000000E   01   0.0000000E-39     1.0000000E   00   -9.0000000E   01   0.0000000E-39     1.0000000E   00   -9.0000000E   01   0.0000000E-39     1.0000000E   00   -9.0000000E   01   0.0000000E-39     1.00000007E   00   -9.0000000E   01   0.0000000E-39     1.00000007E   00   -9.0000000E   01   0.0000000E-39     1.00000007E   00   -9.0000000E   01   0.0000000E-39     1.0000007E    00   -9.0000000E   01   0.0000000E-39     1.00000000E   00   -9.0000000E   01   0.0000000E-39     1.00000000E   00   -9.000000E   01   0.0000000E-39     1.0000000E   00   -9.0000000E   01   0.0000000E-39     1.00000000E   00   -9.0000000E   01   0.0000000E-39     1.0000000E   00   0.000000E-30   0.0000000E-30     1.0000000E   00   0.000000E-30   0.00000000E-30     1.0000000E   00   0.000000E-30   0.0000000E-30     1.0000000E   00   0.000000E-30   0.0000000E-30     1.000000E   00   0.000000E-30   0.0000000E-30   0.0000000E-30     1.000000E-3000E-300E-300E-30   0.0000000E-30   0.0000000E-30     1.000000E-300E-300E-300E-300E-30   0.0000000E-30   0.0000000E-30			. 4913750E-14
9.6764625E 03 8.4813458E 01 8.999987E 01 1.6666775E-01 9.249107E-01 0.000000E-39 1.0000002E 00 -9.0000000E 01 1.3299936E-05 1.0000002E 00 -9.0000000E 01 1.3299936E-05 1.0000003E 00 -9.0000000E 01 1.730138E-05 1.0000003E 00 -9.0000000E 01 1.730138E-05 0.0446675E-02 9.3724206E-01 0.000000E-39 1.0000006E 00 -9.0000000E 01 1.6676506E-05 0.7499128E 03 8.8543625E 01 8.9999947E 01 0.0000006E 00 -9.0000000E 01 1.322939E-05 1.0000006E 00 -9.0000000E 01 1.3323439E-05 1.0000000E 01 0.0000000E-39 1.0000000E 01 0.0000000E-39 1.0000000E 01 0.0000000E 01 0.3323439E-05 1.00000007E 00 -9.0000000E 01 1.5319731E-05 1.00000007E 00 -9.0000000E 01 1.5319731E-05		R. 8320764E-07 3	3.9251707E 00
1.6666775E-01 9.2491707E-01 0.0000000E-39 1.0000002E 00 -9.0000000E 01 1.3299956E-05 0.7101851E 03 8.6054524E 01 8.999997E 01 1.2717220E-01 9.3220177E-01 0.0000000E-39 1.0000003E 00 -9.0000000E 01 1.7301343E-05 0.7346810E 03 8.7294257E 01 8.999997E 01 0.046675E-02 9.3724246E-01 0.000000E-39 1.0000006E 00 -9.0000000E 01 1.5676506E-05 0.7499128E 03 8.8543625E 01 8.999997E 01 0.0000006E 00 -9.0000000E 01 1.3523439E-05 0.7561775E 03 8.9789761E 01 8.999997E 01 0.7561775E 03 8.9789761E 01 8.999997E 01 0.7561775E 03 8.9789761E 01 8.999997E 01			0.0000000E-39
1.0000002E 00 -9.0000000E 01 1.529935E 03 0.7101851E 03 8.6054524E 01 6.999997E 01 1.2717220E-01 9.3220177E-01 0.0000000E-39 1.0000003E 00 -9.0000000E 01 1.7301343E-05 0.7346810E 03 8.7242426E-01 0.0000000E-39 0.0000006E 00 -9.0000000E 01 1.6676506E-05 0.7499128E 03 8.8243625E 01 8.999997E 01 0.0000006E 00 -9.0000000E 01 1.6676506E-05 0.7499128E 03 8.82436E-01 0.0000000E-39 0.0000000E 01 1.3323439E-05 0.7261775E 03 8.9789781E 01 8.999997E 01 0.7261775E 03 8.9789781E 01 8.999997E 01 0.7261775E 03 8.9789781E 01 1.3323439E-05 1.0000007E 00 -9.0000000E 01 1.5319731E-05	8.8324974E=01 8.8324		1.8735864E-14
0.7101851E 03 8.6054524E 01 8.999947E 01 1.2717220E-01 9.3220177E-01 0.000000E-39 1.0000003E 00 -9.0000000E 01 1.7301383E-05 0.7346810E 03 8.7224246E-01 0.000000E-39 0.0446675E-02 9.3724206E-01 1.667520E-05 0.7499128E 03 8.8543625E 01 8.999987E 01 0.7499128E 03 8.8543625E 01 0.0000000E-39 0.7499128E 03 8.978936E-01 0.70000000E-39 0.7499128E 03 9.40838310E-01 1.3323439E-05 0.7561775E 03 8.9789761E 01 8.999987E 01 0.7561775E 03 9.4238210E-01 1.5319731E-05	Ì	*	3/0000¢u•
1.2717220E-01 9.3220177E-01 0.000000E-39 1.0000003E U0 -9.000000E U1 1.7301383E-05 1.0000003E U3 8.7296237E U1 8.999987E 01 0.0446675E-02 9.3724206E-01 0.000000E-39 1.000006E U0 -9.000000E U1 1.6676506E-05 1.000006E U3 8.8543625E U1 8.999987E 01 0.799128E U3 8.8543625E U1 0.000000E-39 1.000000E U0 -9.000000E U1 1.3323439E-05 0.7561775E U3 8.9789761E U1 8.999987E 01 0.756449E-U3 9.4238210E-01 0.0000000E-39 1.0000007E U0 -9.000000E U1 1.5319731E-05	10-3666666		0.00000005-39
1.0000003E U0 -9.000000E U1 1.7301383E-U5 0.7346810E U3 6.7294237E U1 8.9999987E 01 0.0446675E-U2 9.3724206E-U1 0.000000E-39 1.0000006E U0 -9.000000E U1 1.6676506E-05 0.7499128E U3 8.8543625E U1 8.9999987E 01 0.000000E U0 -9.4085938E-U1 0.0000000E-39 1.0000000E U0 -9.000000E U1 1.3323439E-05 0.7561775E U3 8.9789761E U1 8.999987E 01 0.7936449E-U3 9.4238210E-U1 0.0000000E-39 1.0000007E U0 -9.000000E U1 1.5319731E-05		A.8517290E-01 1	1.4476953E-14
0.7346810E 03 8.7296237E 01 8.999987E 01 0.0046675E-02 9.3724206E-01 0.000000E-39 1.0000006E 00 -9.000000E 01 1.6676506E-05 1.0000006E 03 8.8543625E 01 8.999987E 01 0.799128E 03 8.8543625E 01 0.000000E-39 1.0000000E 00 -9.000000E 01 1.3323439E-05 0.7561775E 03 8.9789761E 01 8.999987E 01 0.793449E-03 9.4238210E-01 0.0000000E-39 1.0000007E 00 -9.000000E 01 1.5319731E-05	1.0581417E 01 7.2109		00 400000000000000000000000000000000000
a.0446675E-U2 9.37242U6E-U1 0.000000E-39 1.0000006E U0 -9.000u00E U1 1.6676506E-05 1.0000006E U0 -9.000u00E U1 0.0000000E-39 1.0000000E U0 -9.000000E U1 1.323439E-05 0.7561775E U3 8.9789761E U1 8.999987E 01 4.7936449E-U3 9.4238210E-U1 0.000000E-39 1.0000007E U0 -9.000000E U1 1.5319731E-05	9,999999E-01 -0.0000		0.000000E-39
1.0000006E U0 -9.000000E U1 1.6676506E-05 0.7499128E U3 8.8543625E U1 8.999947E 01 4.8520172E-02 9.4085938E-01 0.000000E-39 1.0000000E U0 -9.000000E U1 1.3323439E-05 0.7561775E U3 8.9789761E U1 8.999947E 01 0.7936449E-U3 9.4238210E-01 0.000000E-39 1.0000007E U0 -9.000000E U1 1.5319731E-05			
0.7499128E 03	1.0490151E 01 4.3974	4.3974591E-07 6	6.2332812E 00
4.8520172E-02 9.4085938E-01 0.000000E-39 1.0000006E 00 -9.000000E 01 1.3323439E-05 0.7561775E 03 8.9789761E 01 8.999987E 01 4.7936449E-03 9.4238210E-01 0.000000E-39 1.0000007E 00 -9.000000E 01 1.5319731E-05			0.00000005-39
1.0000000E U0 -9.000000E U1 1.3323439E-05 0.7561775E U3 8.9789761E U1 8.9999947E 01 4.7936449E-U3 9.4238210E-01 0.000000E-39 1.0000007E U0 -9.0000000E U1 1.5319731E-05			1.0667616E-14
0.7561775E U3 8.9789761E U1 8.999987E 01 4.7936449E-U3 9.4238210E-01 0.000000E-39 1.0000007E U0 -9.0000000E U1 1.5319731E-05	1.0425515E 03 3.9570	3.957001AE-07 6	6.991349E 00
4.7936449E-U3 9.4238210E-01 0.000000E-39 1.0000007E U0 -9.000000E U1 1.5319731E-05	-		0.00000000-39
1.0000007E U0 -9.000000E U1 1.5319731E-05 1			1.n149667E-14
•	• 0385822E 07 7.7888	3.7888778E-07 7	7641487F 00
0.7562467F 03 8.9952406F 01 8.9999947E 01			0.0000000E-39
	3814222E-01		1.0141084E-14

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POWER LOSS EPSTEIN CN GROUP DELAY	Ი.ᲘᲘᲘᲘᲘᲘᲘ 1.Ი394681E-14 A.5290051E 00	0.n0 <u>0000006</u> -39 1.1445093F-14 9.2945191F 00	0.00000000F-39 1.3500052F-14 1.0051220E 01	0.00000000E-39 1.7031583E-14 1.0829664E 01	0.0000000E-39 2.3030040E-14 1.1600450E 01	0.000000000005-39 3.3349983F-14 1.2374237E 0.1	n.nonooooe-39 5.15354376-14 1.3151772E 01	0.00000000005-39 A.u979735F-14 1.3933925E 01	n.ngn00000F-39 1.u972562F-13 1.u721719F 01	0.00000008-39 2.8128736E-13 1.5516391E 01	0.0000000E-39 F.6242231E-13 1.6319479E 01	1.1984651F-12 1.7132940E 01
DOPPLER SP	-0.0000000E-39	-0.0000000E=39	-0.0000000E-39	-0.00000000E-39	-0.0000000E-39.	-0.0000000E-39	-0.0000000E-39	-0.0000005=39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-n,0000000E-39
Y**?	8.8780747E-01	8.869785uE=01	8.8570115E-01	A.A395A85E-01	8.8170195E-01	8.7888357E-01	8.7545863E-01	A.7134090E-01	8.6640869E-01	A.6052927E-01	R.5352689E-01	R,4513656E-01
N'!	3.8668870E-07	4.2143457E=07	4.8918262E-07	A.0374732E-07	7.9364087E-07	1.1099250E-06	1.6452545E-06	2.5833914E-06	4.2992075E-06	7.5616214E-06	1.4016773E-05	2,7379573E-05
ARSORPTION	a.9999999E=01	9,9999999E=01	a,99999996=01	a,9999999E=01	9.99999998E-01	a.99a9a9ae=u1	a,999999qE-01	9.2999999E=01	0.9999999E-01	a.9999999e=01	9.99999996E-01	9.9999999E_01
MU**2	A.87AU75NE=01	A,8697A55E=01	A.857U116E=01	8.8395886E=01	8.8170196E-01	a.78A836NE=01	R.75u5R6uE-01	A.7134092E=01	A.664UA73E-01	a.6052931E=01	A.5352691E-01	R.451365RE_01
M	1.04NBRO3E 03	1,0465529E UR	1.054808ZE 0*	1.0656973E 03	1.0794545E 0x	1.0962617E 03	1.1162475E 03	1.1397493E 03	1.1672594E-03	1.1992414E 0*	1.2353054E 07	1.279422RE_03
LONGITUDE	8.ayayaa7E 01	8.9999987E U1	8.9999887E U1	8.9999987E 01	8.ayayayz U1	8.999987E 01	8.999987E 01	8.9999987E_01	8.999987E U1	8.999987E 01	8.9999987E_01	8,a999a87E 01
Ya	0.nu0ununE-39	0.nunununE-39	0.0000000E=39	0.nunununE-39	0.nunununE-3a	0.000000E=39	0.n000nnE-39	0.000000E=39	0.000000E=39	0.n000n0nE-39	0.0000000E=39	0,nunununE=39
DEL MU	1.p152613E-05	1.nal714nE-05	1.3307696E=05	1.68nu984E-U5	1.6751295E-05	1.292149E=105	1.3783289E-U5	1.6982257E=05	1.0573974E=05	1.1754524E-05	1.1437256E=05	1,59978U1E=05
COLATTIUDE	9.103c0b7E 01	9.2281754E U1	9.352cnule 01	9.4/6.252E U1	9.6u0/515E 01	9.724.5036E U1	9.8474867E U1	9.9702653E u1.	1.0092505E U2	1.0214423E Q2	1.0335929E U2	1.045/108E U2
72	9.416c404E-01	9.38976U1E-U1	9.3592753E-U1	9.270/8U7E-U1	9.191/433E-01	9.0882241E-U1	8.9511049E-U1	8.8302022E-u1	A.689.925E-01	8.5200294E-U1	8.336m97E-01	8.1544n24E-01
MUD Aun AKG	-9.000no00E 01	-9.0u0ununE U1	=9.000unu0E 01	-9.000unune U1	-9.0u0onu0E 01	-9.0000000E U1	-9.0000000E U1	-9.0000000E u1	-9.0000000E U1	-9.0000000E 01	-9.000m00E 01	-9.000a000E 01
KAUIUS	0.7532346E U3	0.7408184E U3.	0.7193019E U3	9.6489330E U3	0.64946b3E u3	0.5010556E 03	0.5442659£ U3		0.4056719E 03	0.32420b3E 03	0.2351743E U3	0.1385934E U3
Y1	-3.3936011E-U2	-7.2818894E-U2	-1.1910507E-01	-1.5647718E-U1	-1.91886b9E-u1	-9.3005522E-01	->.6915673E-U1		-3.3354193E-01	-3.60720b3E-01	-3.9829176E-01	-0.2449239E-U1
EQLAKIZAIION -	6.999999E-01	1.0000006E U0	1.0000001E U0	1.0UUUUU5E U0	1.0000004E u0	.1.000001E 00	1.0000007E U0		1.0000006E 00	0.999999E-01	1.0900009E 00	1.0000000E U0
C PHASE PAIH GROUP PAIH KAY. PAIH	2.5000000e u3 2.5587015e u3 2.3463297e u3	2.40000000 03 2.7883557E 03 2.5588364E 03	2.64000000 u3 3.0183659E u3 2.7714682E u3	2.800u0u0e u3 3.248b991e u3 2.983b812e u3	3.00000000 u3 3.4801351E u3 3.1965352E u3	3.20000000 u3 3.7122710E u3 3.4096945E u3	3.4000000E 03 3.9455315E 03 3.6232317E 03	3.60000000 u3 4.1801774E u3 3.8372293E u3	3.8000000 03 4.4165156E 03 4.0517824E 03	4.0000000 03 4.6549172E 03 4.2670035E 03	4.20000000 03 4.8958437E 03 4.4830295E 03	4.400u0u0e u3 5.1398819E u3 4.7000301E u3
282		:			1							

POWER LOSS	0.00000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.000000000000000000000000000000000000	0.0000000E-39
EPSTEIN CD	2.7273660E-12	6.6340648E-12	1.7287982F-11	4.8560328F-11	1.4855589E-10	5.0310463E-10	1.9409943E-09	9.0477102E-09	5.9504748E-08	1.4098117E-06		1.5544319E-07
GROUP DELAY	1.7959319E 01	1.8802044E 01	1.9665902E 01	2.0557860E 01	2.1488604E 01	2.2475686E 01	2.3550799E 01	2.4780022E 01	2.6341849E 01	2.9277749E 01		3.8499721E 01
DOPPLER SP	-0.0000000E-39	-0.000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0.000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39
Y**2	8.3499227E-01	8.2260203E-01	R.0725307E-01	7.8785077E-01	7.6266467E-01	7.288350AE-01	6.8125989E-01	6.0969082E-01	4.8869640E-01	2.0199115E-01	1.4230609E-06	4.1052A72E-01
NU	5.6363433E-05	1.2208703E-04	2.7797160E-04	6.6601317E-04	1.6842028E-03	4.5145364E-03	1.2958793E-02	4.0555973E-02	1.4547056E-01	7.5239098E-01	1.4374013E 00	2.6039533E-01
ABSORPTION	9.9999999E=01	9.999998E-01	9.9999996E-01	9.9999990E-01	9.9999971E=01	9.999911E-01	9.9999690E-01	9.9998741E-01	9.9993349E-01	9.9923335E=01	9.9611150E-01	9.9242402E=01
MU**2	8.3499229E=01	8.2260205E-01	8.0725309E-01	7.8785077E-01	7.6266468E=01	7.28A350RE-01	6.8125990E-01	6.0969087E-01	4.8869641E-01	2.0199116E=01	1.4210609E-06	4.1052877E=01
N	1.3299086E 0x	1.3894372E 01	1.4603705E 04	1.5462582E 01	1.6524843E 03	1.7874207E 03	1.9649102E 03	2.2103736E 01	2.5809750E 01	3.3205346E 03	3.7784882E 01	2.7982431E 01
LONGITUDE	8.9999947E 01	8.9999947E 01	8.9999987E 01	8.9999987E 01	8.9999947E 01	8.9999947E 01	8.999987E 01	8.9999947E 01	8.9999987E 01	8.9999987E 01	8.9999987E 01	8.9999987E 01
Y3	0.000000E-39	0.000000E-39	0.0000000E=39	0.0000000E=39	0.000000E-39	0.000000E-39	0.000000E-39	0.0000000E-39	0.000000E-39	0.000000E-39	0.n000nunE=39	0.0000000E-39
DEL MU	1.3783368E-05	1.1102887E-05	1.1611349E=05	1.4284647E=05	1.5901231E-05	1.5228258E-05	1.5642431E-05	2.0518218E-05	3.8403949E-05	2.7678541E-04	3.9348341E 04	5.9383944E-05
COLATITUDE	1.0577993E 02	1.0698758E 02	1.0819654E 02	1.094u955E 02	1,106,3033E U2	1.1186527E 02	1.1312562E 02	1.144.5262E 02	1.1583653E 02	1.1755643E 02	1.1823051E 02	1.1645444E 02
Y2	7.963∪570E-01	7.7418749E-01	7.4985154E-01	7.2449n33E-01	6,9759721E-01	6.665855E-01	6.2830439E-01	5.779930AE-01	5.0175183E-01	3.1156787E-01	1.0876130E-03	-4.5505125E-01
MUD AND ARG	-9.0000000E 01	-9.0000000E 01	-9.000000E 01	-9.0000n0E 01	-9,000,0000E 01	-9.000000E 01	-9.000000E 01	-9.0000000E 01	-9.000000E 01	-9.000000E 01	-8.9999988E 01	9.000000E 01
RADIUS Y1 POLARIZATION =	0.0344534E 03 -u.4820698E-01 1.0000006E 00	8.9229851E 03 -4.7247833E-01 1.0000000E 00	A.8043370E 03 -u.9495025E-01 1.0000007E 00	A.6783485E 03 -5.1280068E-01 1.0000010E 00	A.5445992E 03 -5.2537873E-01 9.999999E-01	8.4024056E 03 -5.3338426E-01 1.0000006E 00	A.2504941E 03 -4.3525086E-01 1.0000005E 00	A.0860879E 03 -5.2499031E-01 1.0000000E 00	7.9020624E 03 -4.8676638E-01 1.0000003E 00	7.6653594E 03 -3.2390833E-01 1.0000021E 00	7.5721304E 03 4.8961587E-04 2.9313798E 00	7.8181928E 03 4.5106217E-01
PHASE PATH	4.6000000E 03	4.8000000E 03	5.00000000 03	5,2000000E 03	5.4000000E 03	5,6000000E 03	5.8000000E 03	6,0000000E 03	6.2000000E 03	6.4000000E U3	6.4400566E 03	6.6000000E 03
GROUP PATH	5.3877957E 03	5.6406133E 03	5.8997706E 03	6,1673580E 03	6.4465814E 03	6,7427059E 03	7.0652397E 03	7,4340067E 03	7.9025547E 03	8.7833248E U3	9.8577780E 03	1.1549916E 04
RAY PATH	4.9182202E 03	5.1378809E 03	5.3593929E 03	5,5832910E 03	5.8103626E 03	6,0418395E 03	6.2798168E 03	6,5283325E 03	6.7971226E 03	7.1307551E U3	7.2591330E 03	7.6019037F 03
												RDOT =

					:							
POWER LOSS	0.0000000E-39	0.0000000E-39	0.0000000E-39	0,00000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.00000000E-39	0.0000000E-39
EPSTEIN CD	1.41A4772E-08	3.u926194E-09	A.46A0160E-10	2,3892542E-10	7.5342794F-11	2.5946676E-11	9.6403118E-12	3.8537134E-12	1.6552251E-12	7.5757118E-13	3.6803251E-13	1.0084091E-13
GROUP DELAY	4.0336654E 01	4.1664945F 01	4.2790603E 01	4,3807926E 01	4.4758558E 01	4.5664464E 01	4.6538579E_01	4.7389109E 01	4.8221563E_01	4.0039841F 01	4.9846818E 01	5.0644666E 01
DOPPLER SP	-0.0000000E-39 5.6963303E-01 6.6271536E-02	0.0000000E-39	-0.0000000E-39	-0.00000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	_0.0000000E=39	-0,0000000E-39	_n.ngngnnge_39	-0.00000000005-39	-0.0000000E-39
Y**2		6.5640996E-01	7.1190167E-01	7.5037320E-01	7.7854166E-01	8.0001958E-01	A.16A8013E-01	A.3035950E=01	A,4129438E-01	n.5032732E_01	R.5788337E-01	R.6419458E-01
N <sup>(1)</sup>		2.0199563E-02	6.8160733E-03	2.4819458E-03	9.6128929E-04	3.9263385E-04	1.6852501E-04	7.6199617E=05	3,6383688E-05	1.8256n42E_05	9.6111444E-06	5.3439853E-06
ABSORPTION	9.9229947E-01	9.9228141E=01	9.9227757E-01	9.922765RE-01	.9.9227629E-01	9,9227619E-01	9.9227616E-01	0.9227615E-01	9.9227614E-U1	9.9227614E-01	9.9227614E=01	9,9227614E-01
MU**2	5.6963304E-01	6.564099RE=01	7.1190169E-01	7.50*7321E-01	7.785416RE-01	8.0001961E-01	A.1688014E-01	R.30~5052E-01	8.4129439E-01	8.5072735E-01	8.5788339E=01	R.6419459E-01
N	2.3385556E 03	2.0527R54E 03	1.8520632E.03	1.7024764E 0*	1.5861974E 03	1,4928716E 03	1.4162165E 03	1.3524099E 03	1.2987617E 03	1.2529211E 07	1.2133702E=0×	1,1793927E 03
LONGITUDE	8.9999987E 01	8.9999947E_01	8.ayagak7E 01	8.9999947E 01	8.9999987E 01	8.9999987E 01	8.9999947E 01	8.999987E 01	8.0999987E 01	8.a999987E 01	8,9999987E 01	8.0999087E 01.
Ya	0.n00ununE-39	0.n000000E=39	0.n00ununE=39	0.nununnE-39	0.0000000E-39	0.000000E=39	0.0000006=39	0.000000E-39	0.0000000E=39	0.n000nunE-39	0,0000000E=39	0.n000nunE=39
UEL MU	2.3742982E-05	2.n575027E=05	2.7577250E=05	1.u429818E-05	7.6741700E-06	7.2116479E=06	1.5808574E=05	2.2830800E-05	9.6646328E=06	6.8744184E-06	1,5956494E=05	2.2390344E=05
COLATTIUDE	1.1497738E 02	1.1354226E 02	1.1230723E 02	1.1112236E U2	1.0989553E 02	1.086cn42E 02	1.0747194E U2	1.0620442E 02	1.0505457E UP	1.0384374E U2	1.0265151E 02	1.0141471E 02
12	-5.5545828E-01	-6.1377549E-01	-6.5077886E-01	-6.8U85596E-U1	-7.1241779E-01	-7.4275952E-01	-7.6635877E-U1	-7.8530670E-01	-8.0465754E-01	-8.2785741E-01	-8.4792549E-01	-8.6053364E-01
MUD. ALLD. ARG	9.000unonE 01	9.000HAUDE 01	9.0000000E.01	9.0U0UNUE U1	9.0000000E 01	9.000unu0E.u1	9.000ununE U1	9.000unu0E 01	9.000000E U1	9.0000000E 01	9.0000000E 01	9.0000000E 01
RAUIUS	R.0153340E 03	A.1465252E_03	A.343u8a0E u3	A.4887042E U3	A.6454446E_03	A-7545413E U3	n.8764985E u3	6.9909630E 03	0.0975846E U3	0.1970591E_03	0.2990071E u3	0.3742843E 03
Y1	F.1097861E-01	5.2485737E=01	5.3702185E-u1	F.355221E-U1	<.2057907E=01	A-943250RE-U1	n.7590920E-01	4.6209006E-01	0.4025101E-01	0.0017660E=01	x.7270744E-01	3.5167662E-01
POLAKIZATION -	1.0000138E 00	1.0000194E_00	1.0v0u0u5E u0	1.000U195E U0	1.0000049E_00	1-0000030E_U0	1.0000113E DD	1.0000026E 00.	1.000096E U0	1.0000006E_00	1.0000090E.00	1.0000029E 00
PHASE PATH GROUP PATH RAY PATH	6.8000000 03	7.000u0ube u3	7.2000000E U3	7.4000000E u3	7.6000000 03	7.8000000c u3	8.00000000 U3	8.20000000 03	8.400v0v0E u3	8.60000000 u3	8.800000E u3	9.0000000E u3
	1.2100996E 04	1.2499464E u4	1.2837181E U4	1.3142378E u4	1.3427567c 04	1.3699339c u4	1.3961574E U4	1.4216733E 04	1.4466469E u4	1.4711952E u4	1.4954046E u4	1.5193400E 04
	7.8857042E 03	8.1405644E u3	8.3820966E U3	8.6158564E u3	8.8445085c 03	9.0695627c u3	9.2919552E U3	9.5123059E 03	9.7310469E u3	9.9484939E u3	1.0164867E u4	1.0380414E u4

	FO 358540c4.0				, and	
# # # # # # # # # # # # # # # # # # #	7.2061915t-01		8.9999987E 01		-0.0000000E-39	11.1
500 000 000 000	1.0000054E 00	9.000unu0E 01	9.40494515-06	1.1503586E 03	3,1527372E-06	5.1435053E 01
# P # #	9.5189124E U3	9.8965430E 01 -8.9275735F-01	8,9999987E 01	9.9227614E-01 A.73A8499E-01	-0.0000000E-39	
5 4 4 0 5 7	1.0000032E UO	9.000000E 01	8,9807132E-06	1.1253020E UT	1.9613061E-06	5.2219324E 01
# # # # # # # # # # # # # # # # # # #		9,7737236E 01	8.9999987E 01	9.9227614E-01	-0.000000E-39	0.0000000000000000000000000000000000000
	2.4152758E-01 1.0000031E 00	-9.0513543E-01 9.000000E 01	0.0000000E=39 2.2039917E=05		1.2873662E-06	5.2998599E 01
9.8000000E 03		9.6502707E 01	8,999987E 01	9.9227614E-01	-n.000000E-39	0.0000000E-39
1.61321395 04	2.1531682E-01	-9.1339286E-01	0.0000000E-39		A.8064783E-01 9.0064015E-07	2.4479376E-14 5.3773798E 01
1			A 00000×7F 01		94-30000000-0-	0.0000000-39
1.63637106 04	1.7132190F=01	-9.2 19H523F-01	. 0000000E	A.A309991E-01	A.830998AE-01	1.0123235E-14
	1.0000002E 00	9.000unu0E_01	8.3066135E-06	1.0709788E 03	6.7062639E-07	5.4545699E 01
1.0200000E 04		9.4023710E 01	8.9999987E 01	i	-0.000000E-39	0.000000E-39
	5	-9.3254A48E-01	0.000000E-39	.8506378E-01	A.8506377E-01	1.4692298E-14 E.E.15002E 01
1.1662110E U4	1.0000077E 00	9.000000E U1	1.51.554 / 75-05	5	2016316316	+0 3200CTC++C
	9.7336588E U3	9.278u326E 01	8.999997E 01	9.9227614E-01	-0.000000E-39	0.000000E-39
	0.3664411E-02	-9.3689085E-01	0.0000000E-39	8.8653749E=01	4.865374AE=01	
	9.7490923E 03	9.1534812E 01	8.999987E 01	9.9227614E-01	8.8751777E-01	1.0735285F-14
1.20869595 04	5.3669649E=02	9.000000F 01	1.0955231E-05	1.0429188E 04	7.979525AE-07	5.6848267E 01
				11.000	00000000	01-10000000
1.0800000 04	0.7558131E 03	9.0288774E 01	8.999987E 01	9.922/614E-01	8. ABO7637E-01	1.01789645-14
1.2299215E 04	1.0000034E 00	9.0000000E 01	1.03A2043E-05	1.03A8236E 04	7.7984839E-07	5.7613314E 01
	F11 3847456 113	8.989ko46F 01	8.9999987E 01	9.9227614E-01	-0.000000E-39	0.000000E-39
1 745-1016 04	E. 24547626-05	1.5	0.00000000-39	P.8812046E-01	A. 8812044E-01	1.0162559E-14
1.2365933E U4	1.0000018E 00	9.000unonE 01	9.5427146E-06	1.03844256 01	3.7941475E-07	5.7853736E 01
= 0.304660E=09						
1,08628755 04	0.7559785F U3	8.9896946E 01	8,9999987E 01	9.9227614E-01	-0.000000E-39	0.000000E-39
			0.0000000E-39	A.8812046E-01	A.8812044E-01	7
	1.0000018E 00	9.000unu0E_01	9.5427146E-06	1.0384425E 03	3.7941475E-07	5.7853736E 01
= 0.112647E-10						
1.08628756.04	0.7559785E 03	8.9896946E 01	8,9999987E 01		-0.000000E-39	0.000000E-39
	5.2858488E-U5	-9.4240142E-01 9.000000E 01	0.0000000E-39 9.5427146E-06		A.8812044E-01	1.0162559E-14 5.7853736E 01

POWER LOSS	0.0000000E-39	0.00000000E-39	0.0000000E-39	0.0000000E-39	0.0000000E-39	0.00000006-39	0.0000000E-39.	0.00000000E-39	0.0000000000539	0.00000000E-39	0.0000000E-39	0.000000005-39
EPSTEIN CO	1.0343140F-14	1.1346602F-14	1.3560989F-14	1.6752208F-14	2.7516394F-14	3.25602435-14	5.0121591E-14	R.2083085E-14	1.4416212E-13	2.7034880E-13	5.3775775E-13	1.1389420E-12
GROUP DELAY	5.8378152E 01	5.9143615E 01	5.9910223E 01	6.0678538E 01	6.1449163E_01	6.2222742E 01	6.3000012E 01	6.3781848E 01	6.4569258E 01	6.5363454E 01	6.6165956E 01	6.6978700E 01
DOPPLER SP	_n.n000000E-39	0_0000000E#39	-0.000000006-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0.0000000E-39	-0,0000000E-39	-0.000000E=39	-0.0000000E-39	A. 5469925E-05	-0.1000000E-39
Y**2	A.R78500E-01	a.A704755E-01	R.R578374E-01	A.A408346E-01	A.8186967E-01	A.7907112E-01	8.7568486E-01	8,7163235E-01	R.6674935E-01	8.6091636E-01		8.4572698E-01
NU	3.R497R70E+07	4.1816919E-07	4.8464928E-07	5.9477699E-07	7.7756054E-07	1.0861438E-06	1.6044905E-06	2,5038825E-06	u.1555854E-06	7.2987399E-06		2.6176049E-05
ABSORPTION	9.9227614E-01	9.9227614E-01	9.9227614E-01	9.9227614E-01	9.9227514E-01	9.9227514E-01	9.9227613E-01	9.922/613E=01	9.9227613E-01	0.9227613E-01	9.9227613E-01	9.9227613E-01
MU**2	A.8785204E-01	R.8704756E-01	8.8578375E-01	8.8408347E-01	A.8186968E-01	8.7907117E-01	R.7568486E-01	8.7163236E=01	8.6674938E-01	A.609163RE-01	R.5400207E-01	8.4572700E-01
N	1.0405631E 03	1.0460998E 07	1.0542867E_03	1.0649328E 03	1.0784390E 03	1.0951607E.03	1.1149483E 03	1.1380990E 03	1.1653835E-03	1.1971709E 03	1.2338320E 03	1.2764207E 03
LONGITUDE	8.999987E 01	8.9999987E U1	8.9999987E 01	8,a999987E 01	8.9999987E 01	8,999987E 01	8.99999947E 01	8.9999987E 01	8.9999987E 01	8.0999987E 01	8,9999947E_01	8,9999987E 01
Y3	0.n000nune-39	0.nu0ununE-39	0.nu00nunE=39	0,nu0ununE-39	0.nu00nunE=39	0,000000E-39	0.nu000nunE-39	0.000000E-39	0.nu0nunE-39	0.0000000E-39	0,0000000E=39	0,0000000E=39
DEL MU	2.3012678E-05	1.6700121E-05	8.4944277E=06	1,62254U9E-05	2.29n8a39E=05	9,7715355E-06	9.6153893E-06	2.2372335E-05	1.6083744E-05	7.2461871E-06	1,1260225E=05	2,3405390E=05
COLAITIUDE	1424	8.779.0659E_01	8.6552547E ul	8.531unu0E 01	8.4u7u226E ul	8.2834958E 01	8.1503024E U1	_8.0574266E_01	7.9151181E 01	7.7935098E 01	7.6/17u56E 01	7.5504608E 01
72	1590	-9.395.0057E-01	-9.344,726E-01	-9.256H476E-01	-9.2u14293E-ul	-9.1044134E-01	-8.9602736E-01	-8.8283198E=01	-8.716681E-01	-8.5559492E-01	-8.327o558E-01	-8.152795E-01
Mun Ain AKG	1000	9.806.000E_01	9.0u0unu0E ul	9.000unu0E u1	9.0u0unu0E 01	9.0000000E.01	9.0000006 01	9.0000000E_01	9.00040E 01	9.000000E 01	9.000u000E 01	9.0000000E 01
KAUIUS	0.7534746E U3	C.7919417E.U3	9.7206520L U3	<pre>0.69110u0E u3 -1.5918176E-u1 1.0000079E u0</pre>	0.6324272E 03	9.6042000E U3	q.5478989E U3	0.463b815E 03.	0.4105884E 03	0.3293307E 03	0.2409331E 03	0.1450950E u3
Y1	-x.5245760E-U2	5370599E-U2	-1.1258842L-01		-1.8763440E-01	->.2398147E=01	-p.6985149E-U1	-x.0355927E-01	-x.2/02917E-01	-3.6371978E-01	-0.0062893E-01	-u.2357370E-01
POLAKIZAIION -	1.0000022E U0	1.0000074E.00	9.999999E-ul		1.0000019E 00	1.0000038E.00	;.0000045E U0	1.0000027E 00	1.0000082E 00	1.000002E 00	1.0000094E 00	1.0000004E 00
PHASE PATH GROUP PATH	г г г С С С Ф Ф Ф	40 40 40 40	1.140u0u0c u4 1.797s0e7c u4 1.293e172c u4	1.1600000E 04 1.8203562E 04 1.3148771E 04	1.1800000E 04 1.8434749E 04 1.3361609E 04	1.20000000 04 1.8666823E 04 1.3574747E 04		1.2400000c u4. 1.9134554c u4. 1.4002224c u9	1,2600000E 04 1,9370778E 04 1,4210740E 09	1.2800000E U4 1.9609036E U4 1.4431915E U4	1.30000000 04 1.9849767E 04 1.4647885E 04	1.3200000 04 2.0095610E 04 1.4864819E 04

POWER LOSS	EPSTEIN CH GROUP DELAY		6.7804183E 01		6.2723915E-12 6.8645753E 01			0.000000E=39	4.5345888E-11   7.0398026E 01			ĺ		0.0000000E-39	1.7785231E=09 7.3376900E 01					5.1992248E-08	0.0000000				Z.1138030E 00
DOPPLER SP	7**2 NU	-0.000000E-39	8.3569102E=01	-0.000000E-39	A.2343902E-01 1.1631613E-04	-0.000000E-39	8.0831569E-01 2.6376807E-04	-0.000000E-39	7.8924296E-01 6.2881361E-04	-0.0000000E-39	7.6448794E-01	-0.0000000E-39	7.312720nE-01 4.2416177E-03	-0.0000000E-39	6.8474312E-01 1.2122247E-02	-0.0000000E-39	6.1517477E-01	3.7678461E-02	•	4.9880040E-01	'	2.350008AE-01	6.5800690E-01	0.000000E-39	#•2433812E=01
ABSORPTION	MU**2	9.9227613E-01	1.3264922E 03	9.9227612F-01	A.2343904E=01 1.3854996E 03	9.9227610E-01	8.0831572E-01 1.4555654E 03	9.9227604E-01	7.8924296E-01 1.5402129E 03		7.6448797E-01	9.9227531E-01	7.3127202E-01 1.7779944E 03	9.9227331E-01	6.8474313E=01 1.9523911E 03	9.9226478F=01	6.151747AF-01	2.1924n89E 03	9.9221747E-01	4.98A0040E-01	0.91670765-01	2.3500089E-01	3.2421275E 03	9.8845857E-01	-2.98HZ3ZZE-U7
LONGITUDE	Y3 DEL MU	8.9999987E 01	1.3188527E-05	8,9999987E 01	0.0000000E-39 6.6921920E-06	8,9999947E 01	0.0000000E-39 8.9132457E-06	8,9999987E 01	0.0000000E-39 2.0426532E-05	8.9999987F 01	0.000000E-39	8.9999987E 01	0.0000000E-39 1,1226565E-05	8,9999987E 01	0.0000000E-39	8.9999987F 01	0.00000000	1, A152357E-05	8.9999987E 01	0.000000E-39	8 0999947F 01	0.000000E-39	2.n531902E-04	8.999987E 01	-0.000000E-39
COLATITUDE	Y2 MOD AND ARG	7.429628BE 01	-8.0004225E-01	7.3089460F 01	-7.7593203E-01 9.0000000E 01	7.1880236E 01	-7.4900517E-01 9.0000000E 01	7.0566442E 01	-7.2427469E-01		-7.0218415E-01	6.8213956F 01	-6.7144819E-01	6.695b388E 01	-6.3081A10E-01	6.565.061F 01	-5-790ha48r-01	9.0000000E 01	6.4257302E 01	-5.0412133E-01		1	9.000000E 01	6.177u928E 01	3.1147716E-04
RAUIUS	Y1 POLAKIZATION -	0.0412096E 03	-4.4629341E-01	8.9299915F 03	-4.7049816E-01	A.8119235F 03	-4.9729967E-01	8.6869577F 03	-5.1445442E-01	0.5533727F 01	-5.2098500E-01		-5.2955579E-01	8.2601404F 03	-4.3554799E-01	0.0967217F 113	-E.2901274F-01	1.0000072E 00	7.9144752E 03	-4.9463328E-01	1.0000270E 01		1.0000440E 00 E-06	7.5721128E 03	-4.0342019E-04
PHASE PATH	GROUP PATH		2.0341255E 04 1.5082927E 04	1.360000000.04	2.0593726E 04 1.5302485E 04	1.3800000E 04	2.0852429E 04	1.400000000 04	2.1119408£ 04	1.4200000E OF		1	2.1692623E U4 1.6205589E O4	1.4600000E 04	2.2013070E 04	1.080unne nu	2.23779356 114		1.5000000E 04	)	1.699/6695 04	3	2		2.4815457E U4

APPENDIX C

CHECKLIST OF ELEMENTS IN COMMON AND SUBROUTINE

IN WHICH USED

		O I		F :	P F		D :	C P <i>I</i>	\
	M A	N P	T P	I E	O R	W E	E N	o L	-
	I N	U T	U .T	L D	C E	R L	S E	A R	C O 4
/DATA/	X	x	X	X	х	х	х	х	· · · · ·
RMAX	x	x							
RMIN	x	X							
TMAX	x	x							
TMIN	x	X							
PMAX	X	X							
PMIN	X	X							
PRNT	x	X							
RELERR	P	resently	not us	ed					
AØ		x							
ВØ		x					•		
RØ		X	X			x			
THETAØ		X	X			X			
PHIØ		x	X			X			
PLUS	x	X						x	
NPØWER	x	X	$\mathbf{x}$			X			

	М	O I U			P	D		C A	-
	A I N	N P U T	P U T	E L D	R C E	A E R L	E ( N S E	D 1 L A R	C O 4
NPLØT		X	x						
J	X	X							
NUAR	X	X							
N1	x								
EN	X	X	X			X	X		
DNDR	X						X		
DNDT	X						X		
DNDP	X						X		
EMU	X	X	X		X				
RTYSQR	X			X	X				
F	X	X	X					X	
F2	X	X	X			X			
C1	X	X				X			
FH	X	X		X		X		X	
CØSPSI	X	X		X		X		X	
STNPSI	X	X		X		X		X	
DFHDR	X			X		X			
DCPDT	X			X		X			
DCPDY1	X			X		X			

M A	I N P	O U T P	F I E	F O R	P O W E	D E N	P O L	C A L C
		J (		r c				A O R 4
DCPDY2	x			x		x		
DCPDY3	x			X		x		
SP2	x			X				
EMUINT	x	X	X					
EMUS	x	x	X			x		
N	x		X					
GNU	x		X					
MUFLAG	x					x		
NTEST	Presei	ntly not	used					
/HBANK1/	x	x	X	x	X	x	X	x
MØRDER	Presei	ntly not	used					
NØHALF	Prese	ntly not	used					
NØDØUB	Prese	ntly not	used					
HBANK	x	x						
NØEQ	Prese	ntly not	used					
FINVP	Prese	ntly not	used					
FINVPI	Prese	ntly not	used					
ΥØ	X	X	x	x	X	X	X	x
YD	X		x			X		

		0	, ,		Р	C
	M A	I U N P	T :	F I O E R	W . E	D P A E O L N L C
	I N	U T	U <b>T</b>	L D	C R E L	S A O E R 4
MA	Pr	esently	not used	l		
/CSCR/	X	X	X	X	X	X
C	X	X		X	X	
RCT	X		X		X	
S	X	X		X	X	
RST	X				X	
Z	X					X
EM	X	X			X	
TERM	X	X			X	
TERM2	X	X			X	
RMØD			X			X
RARG			X			X
YØ6	Pı	resently	not used	d		
/CONST/	<b>X</b>	X				
ØRDER	X	X				
EUBAR	X	X				
ELBAR	X	X				
YCLØW	X	X				
нмахт	X	X				

1	<u>.</u>	I N		F I	F O		) E	P O	Δ
	A I N	P U T	P U T	E L D	R C E	E R L	N S E	L A R	L C O 4
HMINT	х	х						· · · · · · · · · · · · · · · · · · ·	
KD	X	x							
/NEW/	X	x							
PLØTØ	X	X							
RDØT	X	X							
/EPSTN/	X		x						
EPSTIN	X		X						
PRØPT	X		X						
/GAUSS/	X		X	x		X			
YSQUAR	X			X					
DCPDR	X			X		X			
DCPDP	X			X		X			
DFHDP	x			X		X			
F1T				X					
DNMNTR				X					
DEL2S			X			X			
/PØWLØS	s/ x		x			X			
CØSA	X					X			

	I M N	O U F T I	F O	O D W E	C P A O L
	A P	P F J U T T		E N R S L E	L C A O R 4
Y	X	<u> </u>	<u> </u>	X	1, 4
DMDR	X			X	
DMDT	X			X	
DMDP	X			X	
DMDY1	X			X	
DMDY2	X			X	
DMDY3	X			X	
DMDSI	X			X	
DMDDSI	X			X	
DMUDR	X	X		X	
DMUDT	X	X		X	
DMUDP	X	X		X	
DMUDY1	X			X	
DMUDY2	X			X	
DMUDY3	X			X	
DMUDSI	X			X	
EMD	X			X	
EMRAD	X			X	
/EXFLD	/		X	X	

	M A	O I N P		F I I E	P F O O W R I	D E	F N	C O L	A L C
	I N	์ บ <u>T</u>	U T	T D	C E	R L	S E	A R	0 4
D2CY1R				X		x			
D2SY1R				X		X			
D2CY2T				X		X			
D2SY2T				X		X			
D2CY3P				X		X		·	
D2SY3P				x		X			
/GRAPHC	)/ X	X							X
XMAXO	X	X							X
XMINO	x	X							X
YMAXO	x	X							x
YMINO	x	x							X
DATE	X	x							X
/GRAPH1	./ <b>x</b>	X							X
XMAX1	x	X							X
XMIN1	X	x							X
YMAX1	X	X							X
YMIN1	X	X							X
PLT	X	x							x
/RECT/	X		X				X		

		I	כ נ ט	F	F	) O	D	C	
	М	N	T	I	0	W	D E	0	A L
	A I	P U	P U	E L	R C	E R	N S	L A	C
	N	Т	T	D	E	L	E	R	4
DD	X		X				X		
SØA	X		X				X		
LB	X		X				X		
/RDØTS/	X		X						
JUMP	X		X						
NYD1	X		X						
/BLK1/		X					X		
STZM5		X					X		
HPRIME		X					X		
PKDELN		X					X		
AMBDL		X					X		
NO		X					X		